

STORMWATER MANAGEMENT REPORT

For

Mixed Use Development 128 Broad Street Stamford, Connecticut

Prepared For TR Broad II, LLC

October 28, 2022

21UT_DSR_01

Leonard C. D'Andrea, P.E. CT License No. 14869

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Project Summary

TR Broad II LLC, owners of property at #128 & #136 Broad Street in Stamford, Connecticut, are proposing to construct a thirteen-story mixed use building on the subject parcels. The parcels are located on the north side of Broad Street, approximately 350 feet east of the intersection with Bedford Street. The total combined area of the parcels is approximately 35,659 square feet, located in the C-G Zoning District. According to FEMA FIRM Map No. 09001C0516G, (revised July 8, 2013), the parcels do not lie within any Flood Hazard Zones. Refer to Exhibit "E" for a copy of the FEMA FIRM Map.

Parcel A (128 Broad Street) encompasses 20,865 square feet and is located to the west of Gay Street Extension. Currently, the southern portion of the parcel supports a lawn with an asphalt sidewalk along the eastern property line. The northern portion of the parcel supports a portion of the municipal parking lot between the Bedford Street Parking Garage and the buildings fronting Bedford Street. Under existing conditions, the total impervious coverage on Parcel A is approximately 13,000 square feet or 62% of the lot area. Historically, the parcel supported a commercial building with asphalt parking lot. The commercial building and a portion of the parking lot was previously removed circa 1996. Refer to Appendix "B" for an aerial photo of the subject parcel from 1985 depicting the previously removed commercial building.

Parcel B (136 Broad Street) encompasses 14,794 square feet and is located to the south of the Bedford Street Parking Garage. Currently, the parcel supports Gay Street Extension and a concrete sidewalk along the western property line. The remainder of the site supports a manicured lawn with ornamental trees. The total impervious coverage on Parcel B is approximately 2,800 square feet or 19% of the lot area. Historically, the parcel supported a parking lot prior to the construction of the Bedford Street Parking Garage. Refer to Appendix "A" for an aerial photo of the subject parcel from 1970 depicting the parking lot.

The proposed development will include the construction of a thirteen-story mixed use building, spanning over Gay Street Extension, which contains 196 residential units and approximately 4,284 square feet of retail space along the Broad Street frontage. An elevated garage structure will be constructed above both parcels, providing 156 parking spaces. An additional 17 parking spaces will be provided within the surface lot behind the first floor of the proposed building. Other improvements will include the construction of new concrete sidewalks and curbing along Broad Street and Gay Street Extension, installation of new storm drain conveyance systems and various underground utilities.

For a depiction of existing conditions and the proposed development, refer to a plan set prepared by D'Andrea Surveying & Engineering, PC entitled "Final Site Plan Review Set, Location 128 Broad Street Stamford, Connecticut, Prepared for TR Broad II, LLC", Sheets 1 through 6 of 6.

This report will summarize the effect of the proposed development on the surrounding watershed and downstream locations, and outline the proposed stormwater management plan designed to facilitate the proposed improvements.

Watershed Analysis

Drainage patterns for the site were analyzed using HydroCAD version 10, with runoff data generated for the 1, 2, 5, 10, 25, 50 and 100-year storm events.

In this analysis, three (3) "Points of Concern" were identified. Referring to the watershed maps in Exhibits A & B, the points of concern (POC) are designated as various drainage structures within Broad Street and Gay Street Extension.

According to the USDA soil delineation map presented in Exhibit C, the parcel lies within mapped area of Urban Land (HSG-D).

Existing Conditions

The subject parcels are part of a larger watershed, encompassing approximately 4.4 acres, tributary to the storm drainage systems within Broad Street. The watershed extends from Broad Street, north to Forest Street, and from Bedford Street, east to the Bedford Street Parking Garage (refer to Exhibit A). The above-mentioned watershed was delineated into four drainage basins under existing conditions.

Drainage Basin Ex. Area #2 encompasses the northern portion of Parcel A and Gay Street Extension, the municipal parking lot to the north of Parcel A and most buildings fronting Bedford Street from Broad Street to Forest Street. This drainage basin was delineated based on field observations, as the roof downspouts from the buildings fronting Bedford Street were observed discharging stormwater runoff at grade onto the municipal lot to the north of Parcel A. Stormwater runoff from the municipal lot to the north of Parcel A is collected by a series of catch basins and trench drains, directing all flow into an existing manhole (Ex. SDMH#1) at the southwest corner of the Bedford Street Parking Garage (POC A). Existing SDMH#1 also accepts flow from drains within the Bedford Street Parking Garage (Drainage Basin Ex. Area #3). Flows exiting SDMH#1 are routed through a 24-inch RCP sloped at 0.49% to the existing storm drain manhole at the intersection of Gay Street and Broad Street (Ex SDMH #2). Based on our analysis, the 24-inch RCP has adequate capacity to convey tributary flows up to the 5-year storm event.

Drainage basin Ex. Area #1 encompasses the southern portion of Parcel A and Gay Street Extension. Runoff from this drainage basin sheet flows to the south into the northern

gutter line of Broad Street, is collected by two existing catch basins and piped to a manhole located at the intersection of Broad Street and Gay Street Extension (Ex. SDMH#2). Flows exiting SDMH#2 are routed through a 18-inch RCP sloped at 3.9% to the existing 24" RCP storm drain within the center of Broad Street (POC B). Based on our analysis, the 18-inch RCP has adequate capacity to convey tributary flows up to the 10-year storm event.

Ultimately, all runoff from Ex. Area#1, Ex. Area #2 and Ex. Area #3 is tributary to the existing 24" RCP storm drain within Broad Street (POC B). The 24" RCP directs flows east within Broad Street and south on Greyrock Place. Based on City of Stamford Engineering Bureau records, the storm drain conveyance system within Broad Street, including the 24-inch RCP, was constructed in 1972 (Refer to Appendix "C"). Based on the records, this 24-inch RCP has a slope of 0.84% and an approximate capacity of 20.8 CFS. Based on our analysis, the 24-inch RCP does not have adequate capacity to convey tributary flows under existing conditions.

Runoff from Ex. Area #4, which encompasses the manicured lawn on Parcel B, sheet flows to the northeast and is collected by a catch basin in the northeast corner of Parcel B. Runoff entering the catch basin is piped to the south to a manhole located at the southeast corner of Parcel B (POC C). Ultimately, all runoff to POC C is tributary to an 18-inch RCP within the northern sidewalk of Broad Street, which directs flows east within Broad Street and north on Greyrock Place. Based on City of Stamford Engineering Bureau records, the 18-inch RCP was constructed in 1960 (Refer to Appendix "C") and later modified in 1972 during the abovementioned storm drain improvements. The 18-inch RCP has a slope of 0.4% and an approximate capacity of 6.7 CFS.

Base on our analysis, the existing storm drains conveying flows from POC A to POC B are undersized. Therefore, the municipal parking lot behind Parcel A will pond during large storm events. The extend of the ponding has been modeled in the HydroCAD analysis. During extreme rainfall events (50 or 100 year storms), the water surface elevation may overtop the concrete curb on the western face of the Bedford Street Parking Garage, resulting in stormwater flooding the lower level of the garage.

Refer to the Exhibit "A" for a depiction of existing conditions. Refer to Aooendix "J" for a summary of existing conditions peaks flows to each Point of Concern. Refer to Appendix "K" for the existing conditions HydroCAD watershed analysis model.

Proposed Conditions

The proposed development will increase the total onsite impervious coverage, resulting in each parcel having almost 100% of each lot area covered by the proposed building or hardscape. The increase in impervious coverage thereby increases the volume and peak rate of runoff generated during a storm event as compared to existing conditions. However, since Parcel A and Parcel B were historically developed with 100% impervious coverage as previously discussed, the proposed development will result in a net zero increase in volume and peak rates

of runoff as compared to historical conditions. This report compares volume and peak rates of runoff from existing conditions to the proposed development.

Five drainage basins were delineated under proposed conditions. The drainage management plan developed for the proposed development involves the construction of a storm drain conveyance system to collect and route runoff to the existing storm drainage system within Broad Street. Refer to Exhibit "B" and Sheet 2 of 6 in the site plan set for a depiction of proposed conditions.

Stormwater runoff from drainage basin Pr. Area #1, which encompass hardscapes to the south of the proposed building, will be collected by the existing catch basins within Broad Street and piped to POC B. Stormwater runoff from drainage basins Pr. Area #2 and Pr. Area #3, which encompasses offsite properties to the north of the subject property and the Bedford Street Parking Garage, will be collected and piped to a manhole at the southwest corner of the Bedford Street Parking Garage. Flows exiting the manhole will be piped south through Gay Street Extension, into the existing 24" RCP within Broad Street (POC B).

Stormwater runoff from drainage basin Pr. Area #4, which encompasses the new building, will be collected and piped to Retention System #1. Retention System #1 was sized to retain and infiltrate the Water Quality Volume for the parcel. Should the system reach capacity, additional flows will be piped to the proposed twin 18" PVC storm drain within Gay Street Extension. Stormwater runoff from drainage basin Pr. Area #5, which encompasses areas to the northeast and east of the proposed building, will be collected and piped to POC C.

Refer to the Exhibit "B" for a depiction of proposed conditions. Refer to Appendix "J" for a summary of proposed conditions peaks flows to each Point of Concern. Refer to Appendix "L" for the proposed conditions HydroCAD watershed analysis model.

During the construction phase of the project, pretreatment of stormwater runoff will be provided by the use of temporary soil and erosion controls as outlined on the "Sediment and Erosion Control Plan," prepared by D'Andrea Surveying & Engineering, PC. This includes the installation of silt fence, sit sacks and periodic on-site inspections to ensure that the development of the site remains "tight" and stable throughout the construction phase.

Summary of Compliance with Standard 1

The proposed retention system has been sized to retain and infiltrate the Water Quality Volume of the parcel.

Summary of Compliance with Standards 2, 3, and 4

All standards have been achieved to the maximum extend allowable based on onsite soil conditions and limitations of the proposed development and existing infrastructure.

Conclusion

Based on our analysis of the aforementioned watershed, the proposed development will result in a decrease in peak flows to POC B for the 1, 2, 5-, 10-, 25- and 50-year design storms. The proposed development will also result in a decrease in peak flows to POC C for the 1- and 2-year design storms. There will be an increase in peak flows to POC C during the 5, 10, 25, 50 and 100-year design storm due to the proposed 8" PVC that will convey flows from Pr. SDMH #1 to JB #3. The 8" PVC is intended to redirect flow tributary the 24" RCP system within Broad Street, helping to decrease the hydraulic grade line within the proposed twin 18" PVC pipes within Gay Street and the ponding level in the municipal parking lot behind the proposed development.

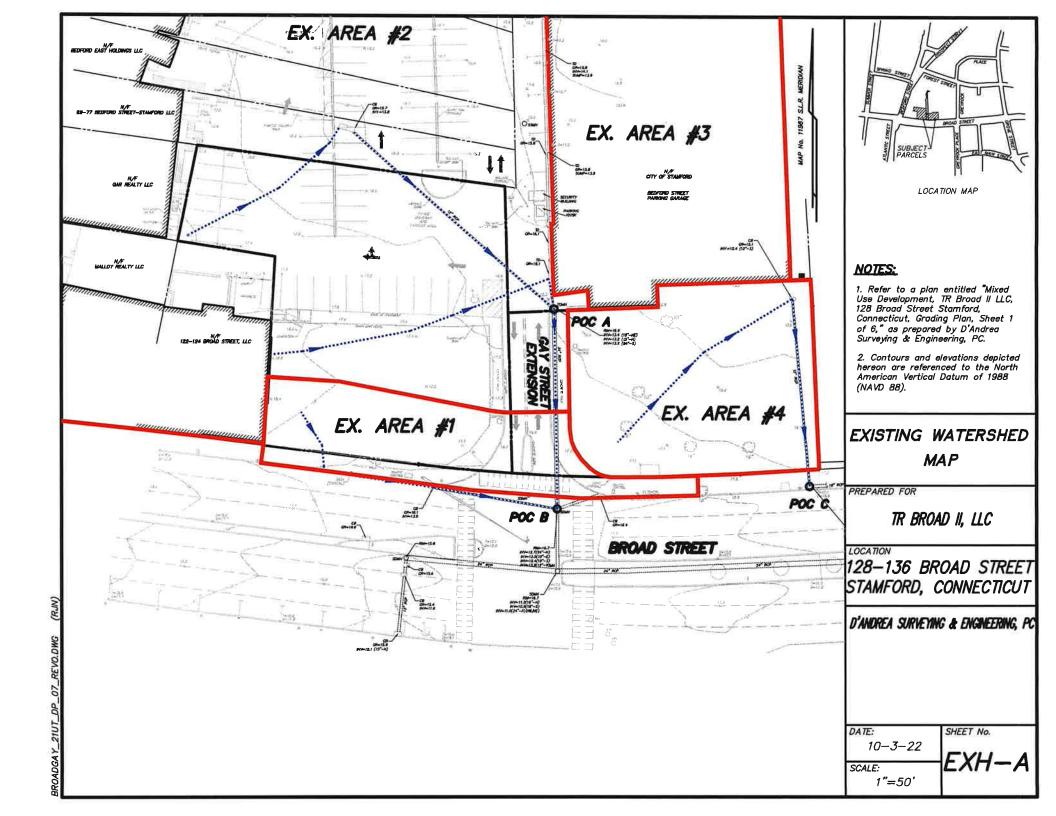
The increase in peak flows to POC C was directed to the existing 18-inch RCP within Broad Street. The 18-inch RCP conveys flows 250 feet east on Broad Street and 525 feet north on Greyrock Place. The 18-inch RCP within Greyrock Place ultimately discharges into a 60" RCP within Forest Street.

The alternative would be to direct the increase in peak flows into the existing 24-inch RCP within Broad Steet, which is currently undersized. The 24" RCP conveys flows 380 feet east on Broad Street and 1,375 feet south on Greyrock Place, where it discharges into a 84" RCP in the intersection of Tresser Boulevard and Greyrock Place.

The proposed design will maintain or reduce the water surface elevation of the ponded water in the municipal parking lot behind the proposed development for all storms excluding the 100-year storm event. The proposed design will also reduce the volume of water tributary to the Bedford Street Parking Garage for the 25- and 50-year design storms.

Based on the above information, the proposed improvements are designed in accordance with the City of Stamford Stormwater Drainage Manual and will not adversely impact adjacent or downstream properties or City-owned drainage facilities.

Exhibit A:
Existing Conditions
Watershed Map



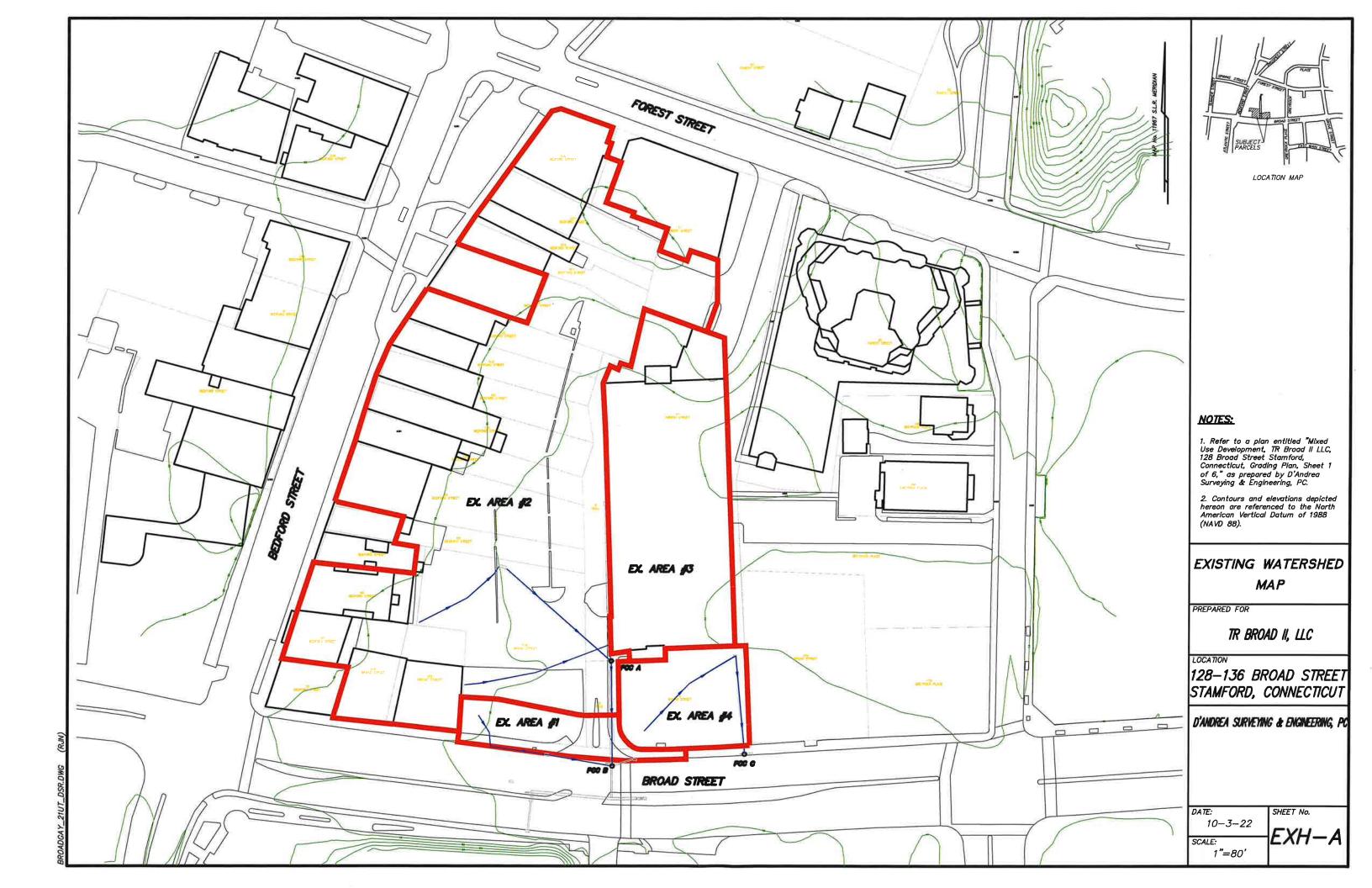
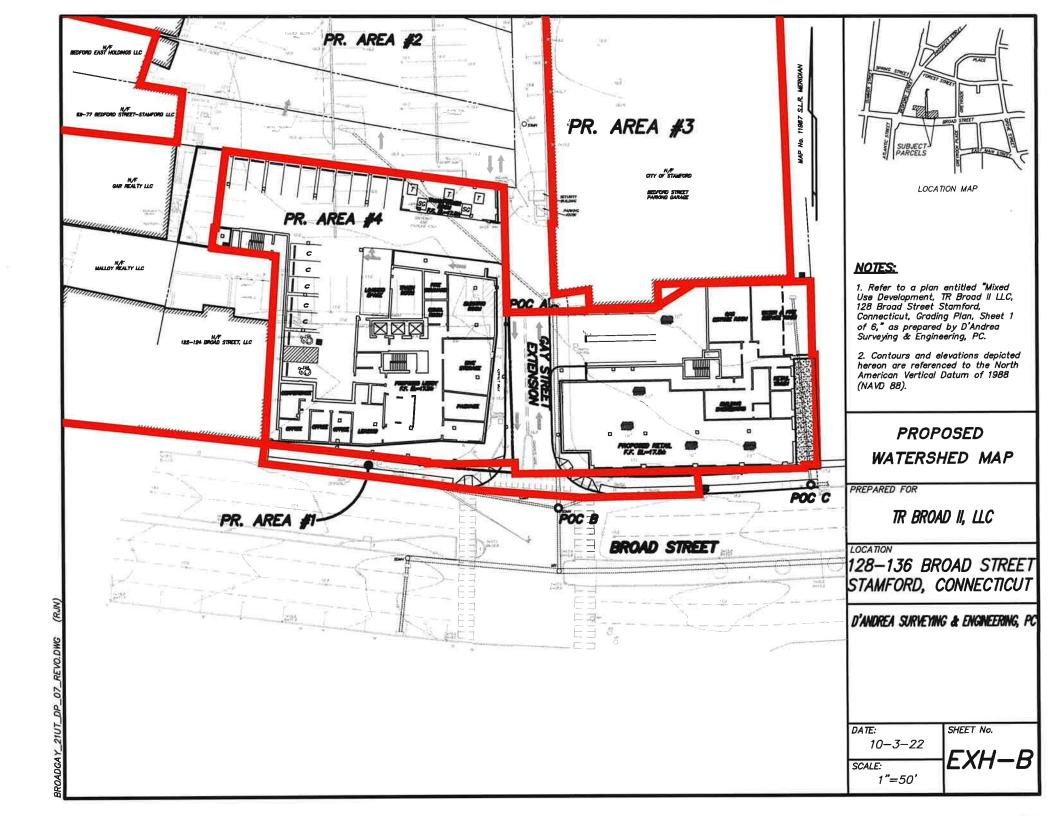
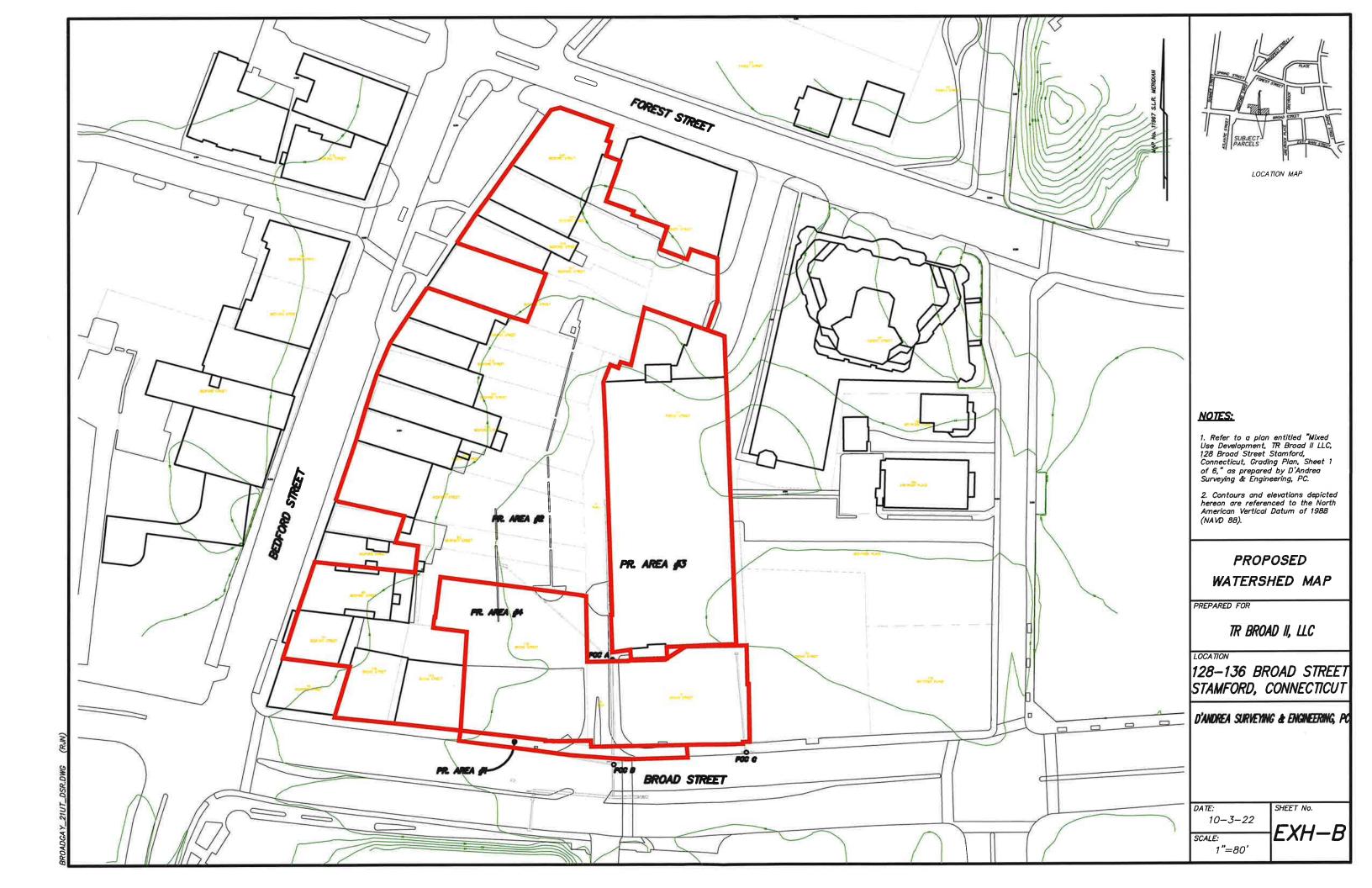
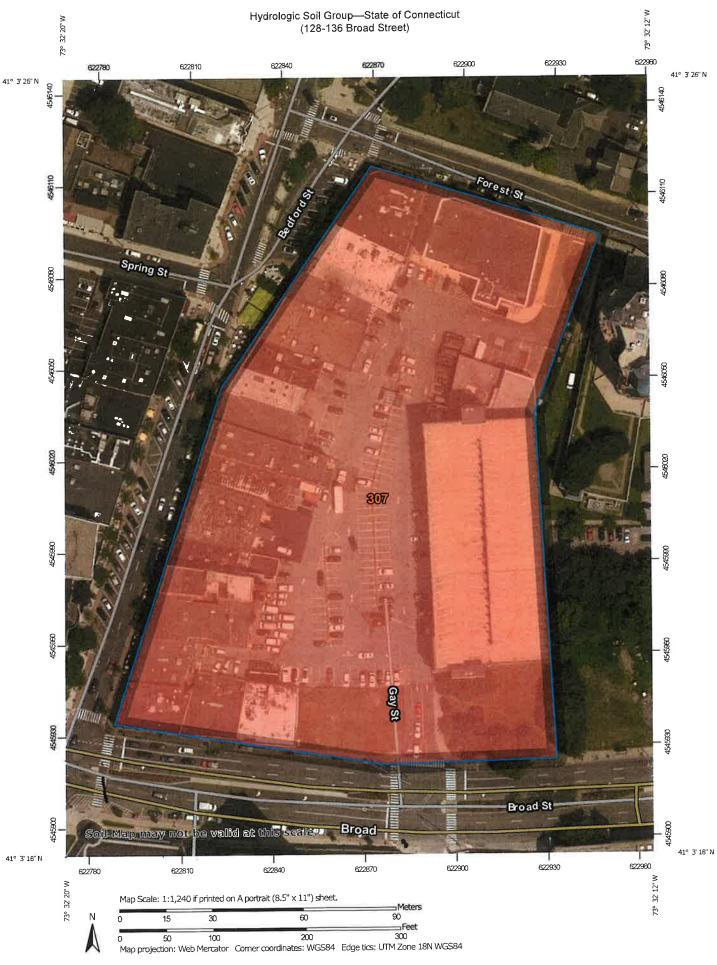


Exhibit B: Proposed Conditions Watershed Map









MAP LEGEND Area of Interest (AOI) Area of Interest (AOI) C/D Soils **Soil Rating Polygons** Not rated or not available Α **Water Features** A/D Streams and Canals Transportation B/D Rails Interstate Highways C/D US Routes Major Roads Not rated or not available Local Roads Soil Rating Lines **Background** Aerial Photography A/D B/D Not rated or not available **Soil Rating Points** Α A/D B/D

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: State of Connecticut
Survey Area Data: Version 15, Sep 28, 2016

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 21, 2014—Aug 27, 2014

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Hydrologic Soil Group— Summary by Map Unit — State of Connecticut (CT600)						
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI		
307	Urban land	D	5.1	100.0%		
Totals for Area of Inter	rest		5.1	100.0%		

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

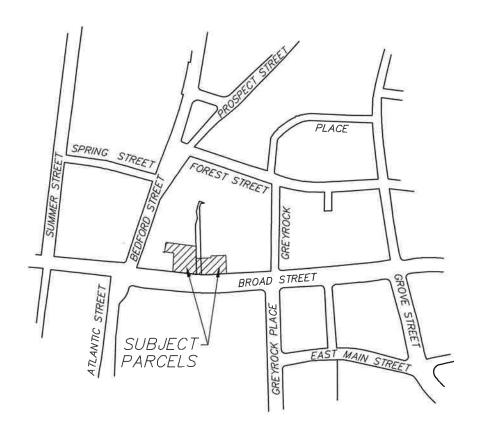
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

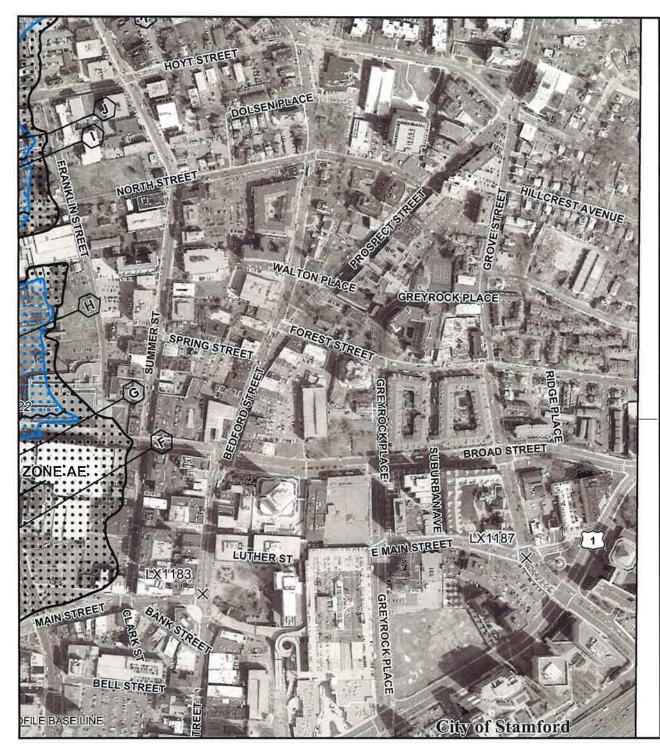
Tie-break Rule: Higher

Exhibit D: Site Vicinity Map



LOCATION MAP

Exhibit E: FEMA Firm Map





MAP SCALE 1" = 500'

1000

FEET

VFIP

w

FIRM

FLOOD INSURANCE RATE MAP FAIRFIELD COUNTY, CONNECTICUT (ALL JURISDICTIONS)

PANEL 0516G

PANEL 516 OF 626

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS:

COMMUNITY	NUMBER	PANEL	SUFFIX	
GREENWICH, TOWN OF	090008	0516	G	
STAMFORD, CITY OF	090015	0516	G	

Notice to User: The **Map Number** shown below should be used when placing map orders; the **Community Number** shown above should be used on insurance applications for the subject community.



MAP NUMBER 09001C0516G MAP REVISED JULY 8, 2013

Federal Emergency Management Agency

This is an official copy of a portion of the above referenced flood map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at www.msc.fema.gov

	ibit F: Precipitation Table	s	
	13		



NOAA Atlas 14, Volume 10, Version 3
Location name: Stamford, Connecticut, USA*
Latitude: 41.0554°, Longitude: -73.5376°
Elevation: 15.78 ft**

* source: ESRI Maps
** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

	Average recurrence interval (years)									
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.365 (0.281-0.465)	0.425 (0.327-0.542)	0.523 (0.401-0.669)	0.605 (0.461-0.777)	0.717 (0.530-0.952)	0.802 (0.581-1.08)	0.889 (0.626-1.24)	0.984 (0.661-1.40)	1.12 (0.724-1.64)	1.23 (0.775-1.82
10-min	0.517 (0.398-0.659)	0.602 (0.463-0.768)	0.741 (0.568-0.948)	0.856 (0.653-1.10)	1.01 (0.751-1.35)	1.14 (0.823-1.54)	1.26 (0.887-1.75)	1.40 (0.937-1.98)	1.58 (1.03-2.32)	1.74 (1.10-2.58)
15-min	0.609 (0.469-0.775)	0.709 (0.545-0.904)	0.872 (0.668-1.12)	1.01 (0.768-1.29)	1.19 (0.883-1.59)	1.34 (0.968-1.81)	1.48 (1.04-2.06)	1.64 (1.10-2.33)	1.86 (1.21-2.73)	2.04 (1.29-3.04
30-min	0.851 (0.655-1.08)	0.992 (0.763-1.26)	1.22 (0.937-1.56)	1.41 (1.08-1.82)	1.68 (1.24-2.23)	1.88 (1.36-2.53)	2.08 (1.46-2.89)	2.30 (1.55-3.27)	2.60 (1.68-3.80)	2.84 (1.80-4.22)
60-min	1.09 (0.842-1.39)	1.27 (0.981-1.63)	1.57 (1.21-2.01)	1.82 (1.39-2.34)	2.16 (1.59-2.86)	2.42 (1.75-3.26)	2.68 (1.88-3.72)	2.96 (1.99-4.20)	3.34 (2.16-4.88)	3.63 (2.30-5.40)
2-hr	1.42 (1.10-1.79)	1.67 (1.29-2.11)	2.07 (1.60-2.63)	2.41 (1.85-3.08)	2.88 (2.14-3.80)	3.23 (2.35-4.34)	3.60 (2.54-4.97)	3.99 (2.69-5.64)	4.55 (2.95-6.61)	4.99 (3.17-7.38)
3-hr	1.63 (1.27-2.06)	1.93 (1.50-2.44)	2.42 (1.87-3.06)	2.82 (2.17-3.58)	3.37 (2.52-4.44)	3.79 (2.77-5.08)	4.23 (3.00-5.84)	4.71 (3,18-6.62)	5.39 (3.51-7.80)	5.94 (3.78-8.74)
6-hr	2.06 (1.61-2.58)	2.45 (1.91-3.07)	3.08 (2.40-3.88)	3.61 (2.80-4.56)	4.34 (3.26-5.68)	4.89 (3.60-6.51)	5.46 (3.91-7.51)	6.11 (4.14-8.54)	7.04 (4.60-10.1)	7.80 (4.98-11.4)
12-hr	2.54 (2.00-3.16)	3.03 (2.39-3.78)	3.85 (3.02-4.80)	4.52 (3.52-5.67)	5.44 (4.12-7.09)	6.14 (4.55-8.14)	6.87 (4.95-9.42)	7.72 (5.25-10.7)	8.94 (5.86-12.8)	9.96 (6.37-14.5
24-hr	2.97 (2.36-3.67)	3.59 (2.85-4.45)	4.61 (3.64-5.72)	5.45 (4.28-6.80)	6.62 (5.03-8.58)	7.48 (5.58-9.89)	8.41 (6.11-11.5)	9.49 (6.49-13.1)	11.1 (7.30-15.8)	12.5 (8.01-18.0)
2-day	3.32 (2.65-4.08)	4.08 (3.26-5.02)	5.33 (4.23-6.57)	6.36 (5.03-7.88)	7.79 (5.97-10.1)	8.84 (6.65-11.6)	9.98 (7.31-13.6)	11.4 (7.78-15.6)	13.4 (8.86-19.0)	15.2 (9.81-21.8
3-day	3.59 (2.88-4.39)	4.42 (3.54-5.42)	5.79 (4.62-7.11)	6.92 (5.49-8.53)	8.48 (6.52-10.9)	9.63 (7.26-12.6)	10.9 (8.00-14.8)	12.4 (8.51-16.9)	14.7 (9.70-20.7)	16.7 (10.8-23.8)
4-day	3.84 (3.09-4.69)	4.72 (3.79-5.77)	6.16 (4.93-7.54)	7.35 (5.85-9.04)	8.99 (6.93-11.5)	10.2 (7.72-13.4)	11.5 (8.48-15.6)	13.1 (9.02-17.9)	15.5 (10.3-21.8)	17.6 (11.4-25.0)
7-day	4.58 (3.70-5.56)	5.54 (4.47-6.73)	7.10 (5.71-8.65)	8.39 (6.71-10.3)	10.2 (7.87-13.0)	11.5 (8.72-14.9)	12.9 (9.52-17.4)	14.6 (10.1-19.8)	17.1 (11.4-23.9)	19.3 (12.5-27.3
10-day	5.31 (4.30-6.42)	6.31 (5.11-7.64)	7.96 (6.42-9.65)	9.32 (7.47-11.4)	11.2 (8.68-14.2)	12.6 (9.56-16.2)	14.1 (10.4-18.8)	15.8 (11.0-21.3)	18.3 (12.2-25.4)	20.4 (13.2-28.8
20-day	7.48 (6.11-8.99)	8.61 (7.02-10.4)	10.5 (8.49-12.6)	12.0 (9.68-14.5)	14.1 (11.0-17.6)	15.7 (11.9-20.0)	17.4 (12.7-22.7)	19.1 (13.3-25.6)	21.6 (14.4-29.7)	23.5 (15.3-32.9
30-day	9.28 (7.61-11.1)	10.5 (8.59-12.6)	12.5 (10.2-15.0)	14.2 (11.5-17.1)	16.4 (12.8-20.4)	18.2 (13.8-22.9)	19.9 (14.6-25.8)	21.7 (15.2-28.9)	24.1 (16.2-33.1)	25.9 (16.9-36.2)
45-day	11.5 (9.46-13.7)	12.8 (10.5-15.3)	15.0 (12.3-17.9)	16.8 (13.7-20.2)	19.3 (15.1-23.8)	21.2 (16.2-26.6)	23.1 (16.9-29.6)	24.9 (17.5-33.0)	27.3 (18.3-37.2)	29.0 (18.9-40.3)
60-day	13.3 (11.0-15.8)	14.7 (12.2-17.5)	17.0 (14.0-20.3)	19.0 (15.5-22.7)	21.6 (16.9-26.6)	23.7 (18.1-29.5)	25.6 (18.8-32.7)	27.5 (19.4-36.4)	29.9 (20.1-40.6)	31.5 (20.6-43.7)

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

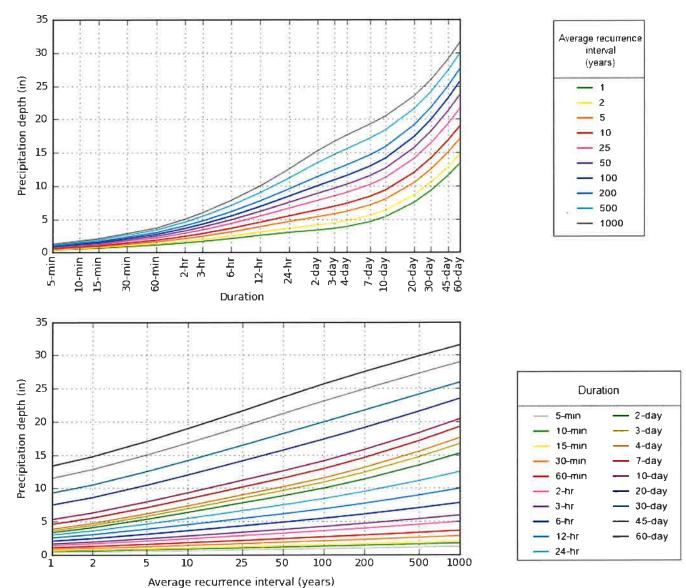
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top

PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 41.0554°, Longitude: -73.5376°



NOAA Atlas 14, Volume 10, Version 3

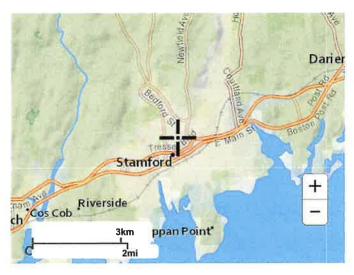
Created (GMT): Mon Apr 18 15:12:51 2022

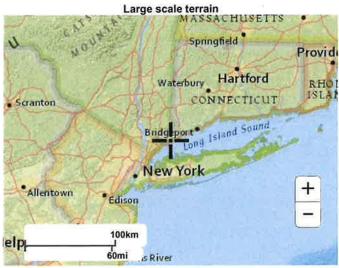
Back to Top

Maps & aerials

Small scale terrain

2 of 4 4/18/2022, 11:13 AM







Large scale aerial

3 of 4 4/18/2022, 11:13 AM



Back to Top

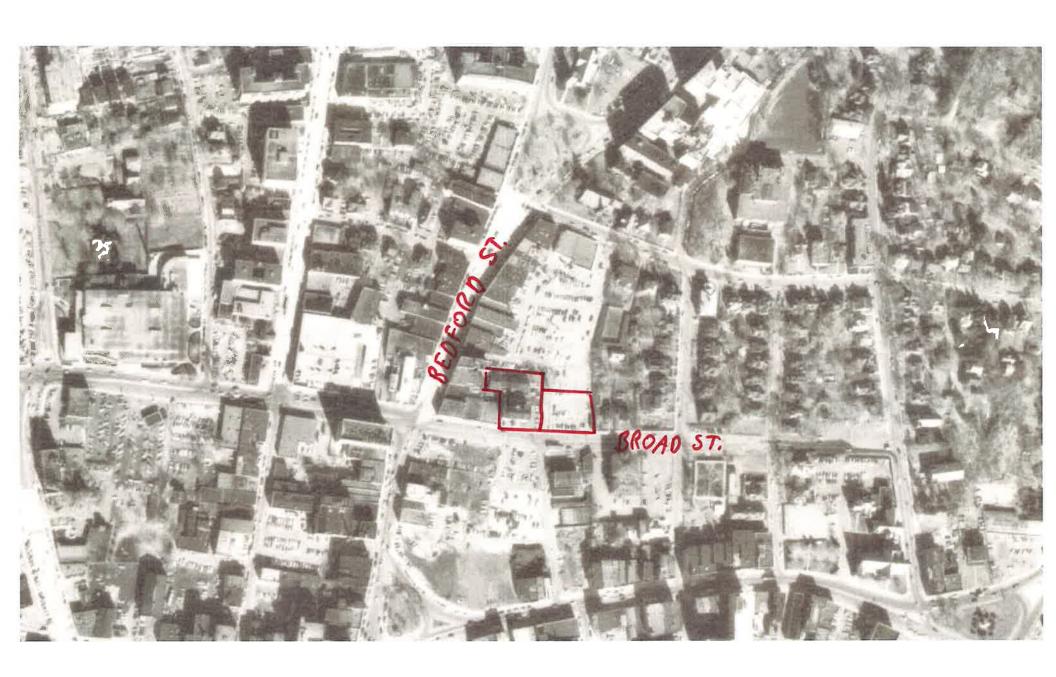
US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway

Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

Disclaimer

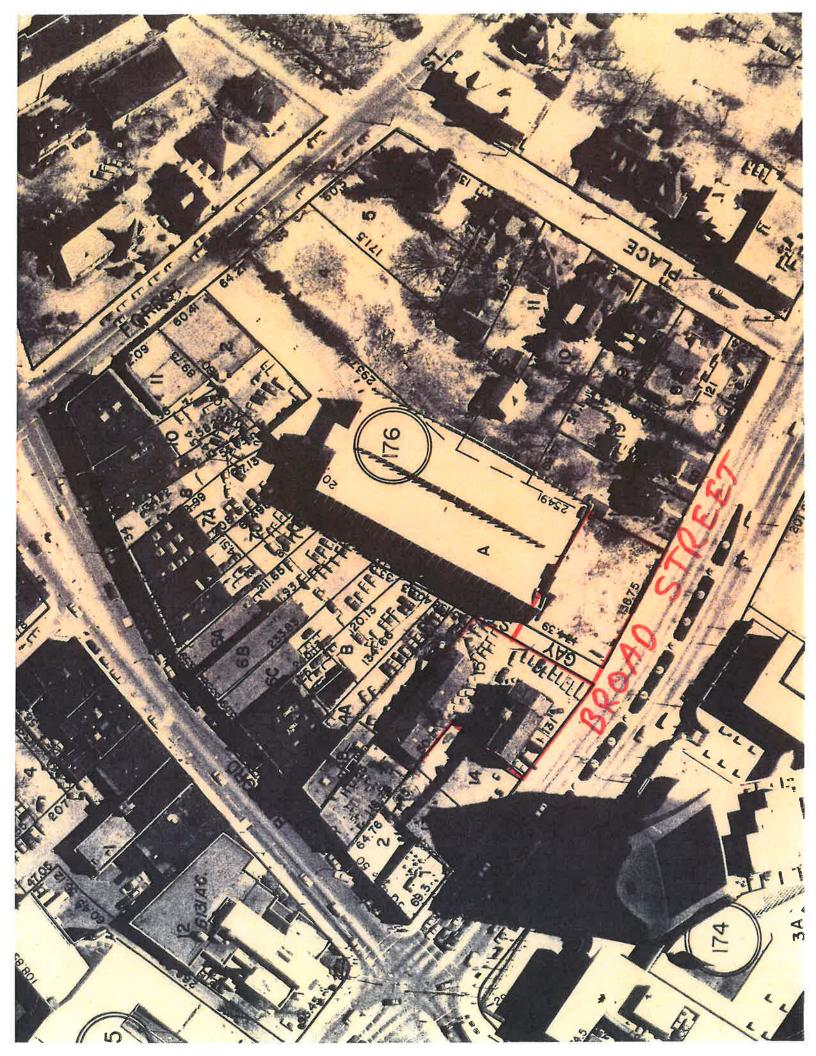
4 of 4 4/18/2022, 11:13 AM

Appendix A: 1970 Aerial Photo



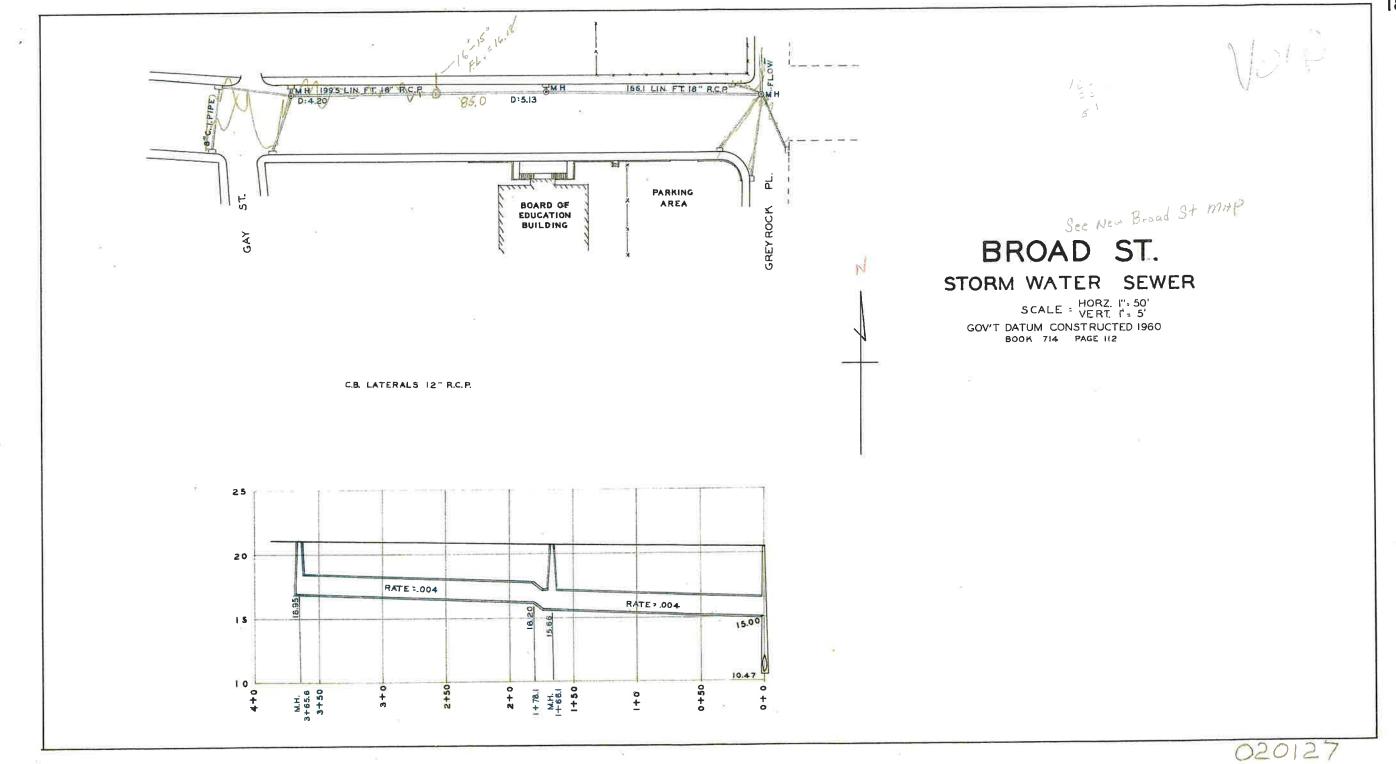
Appendix B: 1985 Aerial Photo

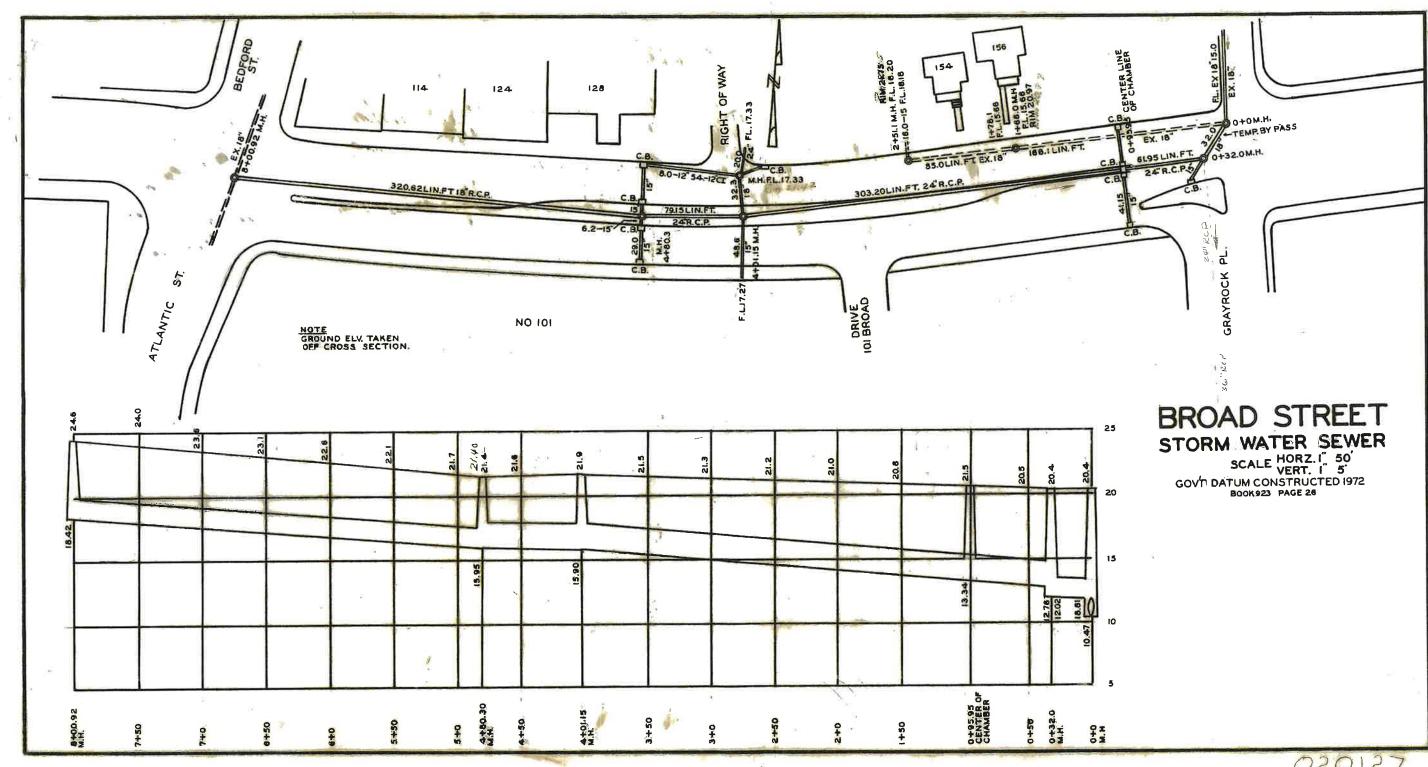




Appendix C: City of Stamford Storm Sewer Maps

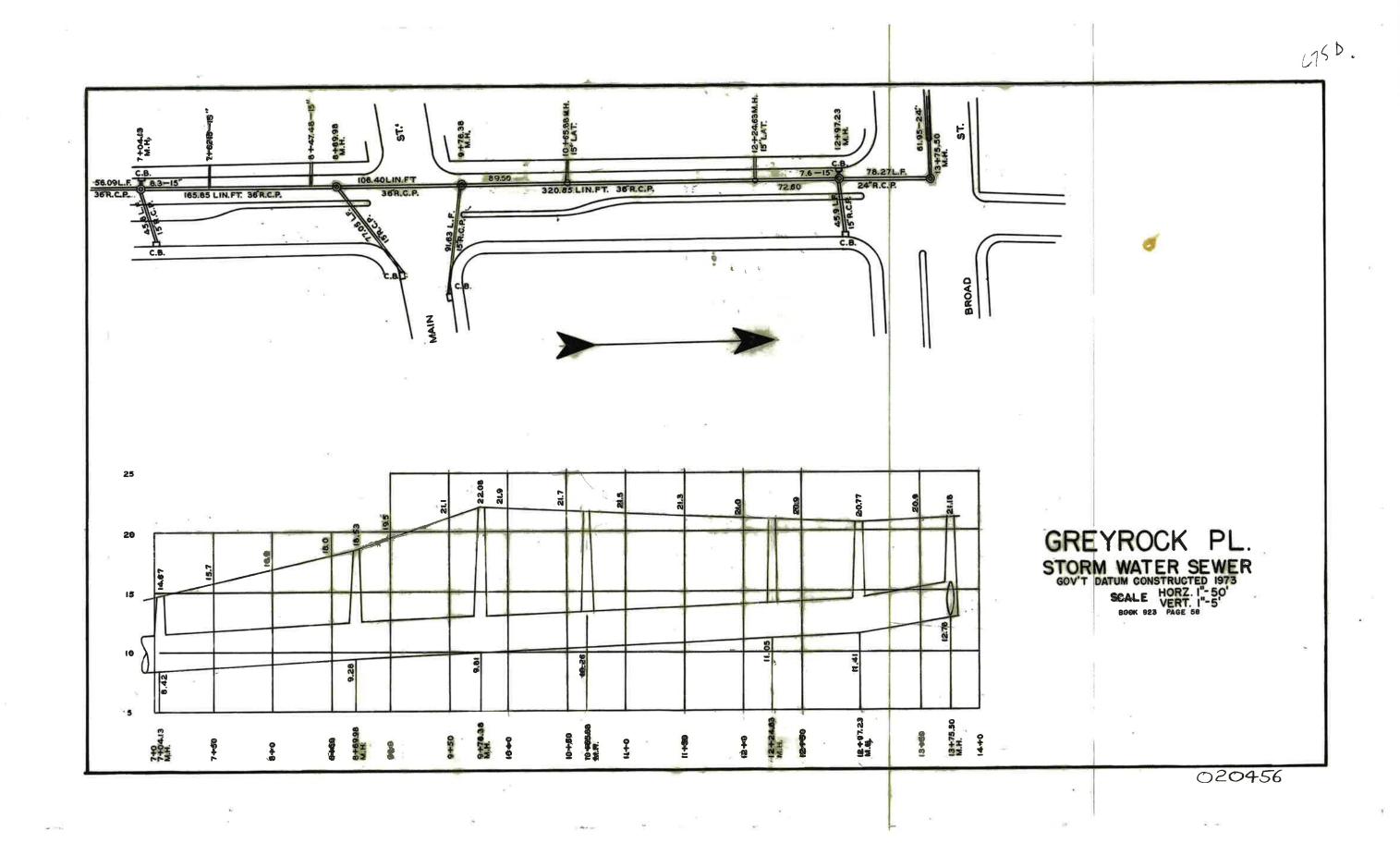






02012

0.86



Appendix D: Design Calculations

Client: TR Broad II, LLC Address: 128 Broad Street Date: October 3, 2022

□ Water Quality Volume

Watershed Data
Watershed Area = 33,888 ft^2 Impervious Cover = 33,888 ft^2 % Impervious Coverage = 100 %

$$WQV = \frac{1in}{12\frac{in}{ft}}RA$$

$$R = 0.05 + 0.9I$$

Where:

WQV = Water quality volume

$$R = 0.05 + 0.9(1) = 0.95$$

$$WQV = \frac{1}{12}(0.95)(33,888) = 2,683ft^3$$

Water Quality Volume (WQV) = $2,683 ft^3$

Storage Volume in RS $#1 = 5,926 ft^3$ (WQV provided)

□ BMP Drawdown Calculations: RS #1

$$t_{drawdown} = \frac{DV}{kA}$$

Where:

DV = Design Volume = 5,926 ft³ k = Infiltration (Rawl's) Rate = 1.02 in/hr (Sandy Loam) A = Infiltration (bottom) Area = 1,940 ft²

$$t_{drawdown} = \frac{5,926}{(1.02)(1/12)(1,940)} = 3.6$$

Drawdown time is 3.6 hours. (Standard Met)

Appendix E: DCIA Tracking Worksheet

Directly Connected Impervious Area Tracking Worksheet City of Stamford Drainage Manual



Note to user: complete all cells of this color only, as indicated by section headings

Part 1: General Information (All Projects)									
Project Name	Mixed Use Development								
Project Address	128 Broad Street								
Project Applicant	TR Broad II, LLC								
Title of Plan	Site Plan Review Set								
Revision Date of Plan	October 3, 2022								
Tax Account Number	001-2688, 004-0515								

Part 2: Project Details (All Projects)				
What type of development is this? (choose from dropdown)	Redevelopment			
2. What is the total area of the project site?	35,659	ft ²		
3. What is the total area of land disturbance for this project?	35,659			
4. Does project site drain to High Quality Waters, a Direct Waterfront, or within 500 ft. of Tidal Wetlands? (Yes/No)	No			
Does Standard 1 apply based on information above?	Yes			

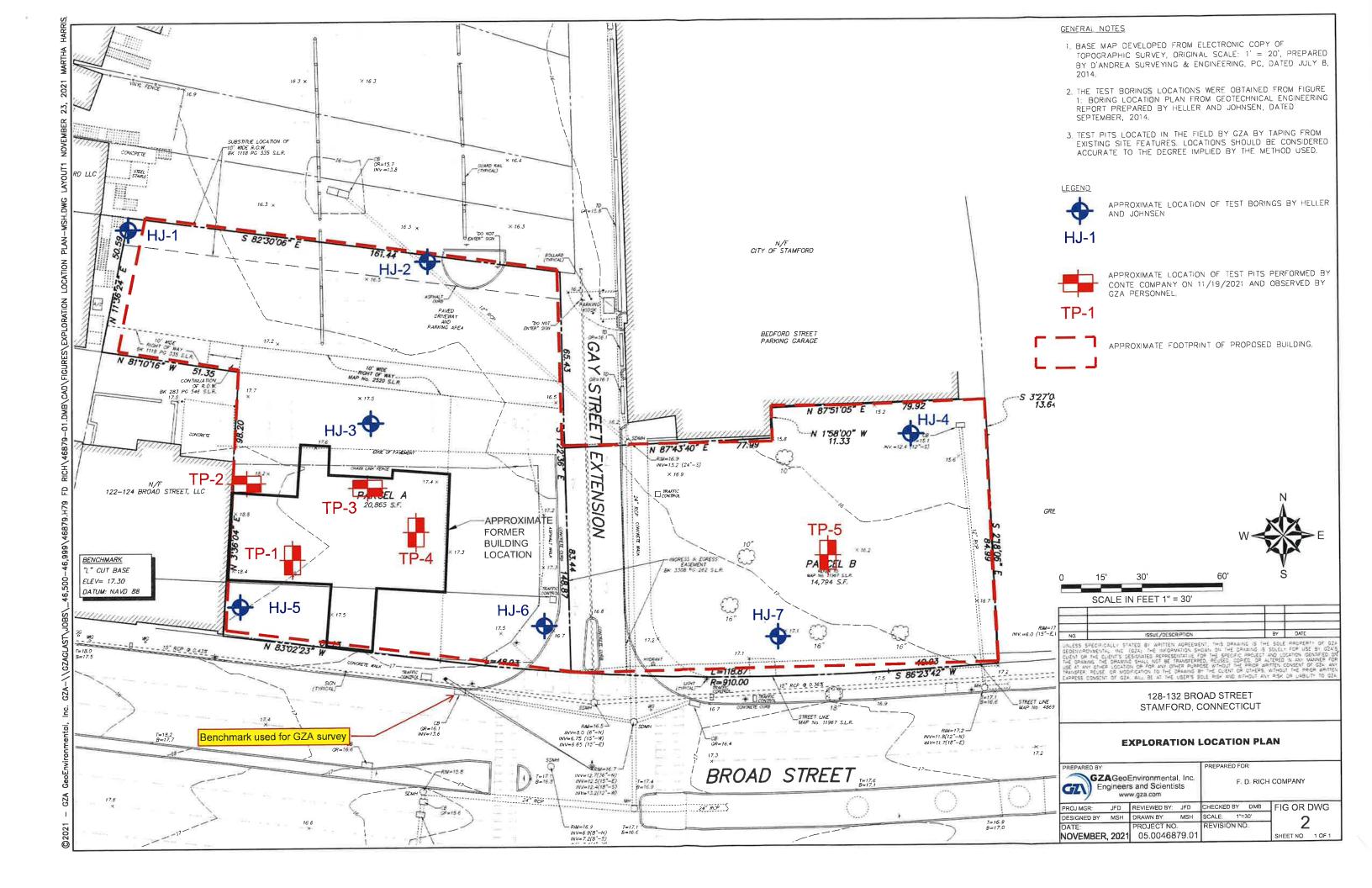
Part 3: Water Quality Target Total (Only for Standard 1 Projects)										
5. What is the current (pre-development) DCIA for the site?	14,965									
6. Will the proposed development increase <i>DCIA</i> (without consideration of proposed stormwater management)? (Yes/No)	Yes									
7. What is the <u>proposed-development</u> total impervious area for the site?	35,659	ft ²								
Water Quality Volume (WQV)	2823.0	ft ³								
Standard 1 requirement	Retain 1/2 WQV on-site									
Required retention volume	1411.5	ft ³								
Provided retention volume for proposed development	5,926.0	ft ³								

Part 4: Proposed DCIA Tracking (Only for Standard 1 Projects)									
Pre-development total impervious area	14,965	ft ²							
Current DCIA	14,965	ft ²							
Proposed-development total impervious area	35,659	ft ²							
Proposed-development DCIA (after stormwater management)	1,771	ft ²							
Net change in DCIA from current to proposed-development	-13,194	ft ²							

Part 5: Post-Development (As-Built Certified) DCIA Tracking (Only for Standard 1 Projects)									
Post-development (per as-built) total impervious area	ft ²								
Post-development (per as-built) DCIA (after stormwater management)	ft ²								
Net change in DCIA from <u>current</u> to <u>post-development</u>	ft ²								

	Certification Statemer	nt							
I hereby certify that the information contained in this worksheet is true and correct.									
Engineer's Signature	Date	Engineer's Seal							

Appendix F:
Boring and Test Pit Data



e T	FOOT	OF BRO	AD STRI			TEST BO	ORING RE	POR	RT .	BORING NO. HJ-1			
	JECT		Broad Stree				GROUND WATER RE	ADING		FILE NO.	30202		
	ATION		. Connectic	77		DATE	TIME		DEPTH	SHEET NO.	1OF2		
CLIE		Bildner (Capital Corp.			6/30/04	1830		21.0′	LOCATION	See Plan		
	ITRACTOR	_Hardima	an Company	& Associates						ELEVATION	17.8'		
	ITEM		CASING	DRIVE SAMPLER	CORE BARREL	DRILL	ING EQUIPMENT & P	ROCEDU	RES	DATUM DATE	NGVD 29 06/30/04 TO _06/30/04		
TYPE			HSA	SAMPLER	DARKEL	RIG TYPE:	Mobile Drilling B-50			START	1730 FINISH 2000		
INSI	DE DIAMETE		2-1/4	1-3/8		BIT TYPE:	-			DRILLER	Anthony Scaife		
	MER WEIGH MER FALL	T (LB) (IN)	1055 1055	140 30		DRILL MUD: HAMMER TYPE:	Safety hammer via Ca	athead a	nd rope	H & J REP	Rvan M. Laird		
D						•							
E P	CASING BLOWS	SAMPLER BLOWS	SAMPLE TYPE	SAMPLE			COIDTION AND SELL	DVC		ELEV./ DEPTH	STRATUM DESCRIPTION		
Т	PER	PER	NO. &	DEPTH (FT)		VISUAL DES	VISUAL DESCRIPTION AND REMARKS						
н	FT	6 IN	REC.	` ´ .									
0					T- 4" =	1. 1	\/EL /Acabalt\			0.4/	ASPHALT		
		11	SS1	0.5	lop 4": Da Bottom 6":	irk brown, black, GRA Dark brown, orange,	vel (Asphait). , fine to coarse SAND	, some S	Silt, little Gravel,	0.4'	527		
		8	10″	2.5					*0		-5-		
		6									FILL		
	1	7	SS2	2.5	Top 6": Da	ark brown, orange, fin	e to coarse SAND, so	me Silt,	little Gravel,	1	Te.		
		7	8"	4.5	trace Asph	alt and White Chips (Light brown, dark br	Hill). rown, SII T and fine t	o mediur	n SAND.				
		4	1		DOCCOTT Z	Light blown, dark bi	J, DIET GIG IIIC 0			4.07			
		2			Top 4": 13	ght brown, dark brow	n. SILT and fine to m	nedium S	and.	4.0′	SILT AND SAND (FILL)		
5		3 22	SS3 12"	4.5 6.0	Bottom 8"	Orange, brown, fine	to coarse SAND, son	ne Grave	l, little Silt.	5.0'			
		100/6"	1	"									
		200,0											
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			Į	1									
		-	1	1 I						1 1			
	-	—	1	1 1						1			
10			1								SILT, GRAVEL AND COBBLES		
10		20	SS4	10.0	Very dens	e, brown, white, fine	to coarse GRAVEL an	d fine to	coarse Sand,				
		55	10"	12.0	trace Silt (encountered cobbles	wille sampling).						
		30	ļ										
		31								1			
		-	1	Į 1						1			
			1	[1 1			
			1	1 1									
]										
15								_	1-	15.0′			
		8	SS5 18"	15.0 17.0	Medium d	ense, brown, fine to o	coarse SAND, trace fi	ne Grave	ele:				
		11	1 -										
		11											
										1 1			
			1								GRAVELLY SAND		
			1										
			1							1 1			
			1							+ 1			
20		6	SS6	20.0	Top 12": l	ight brown, fine to co	parse SAND.	o Cil+		1 1			
		8	24"	22.0	Bottom 12	2: Grey, brown, fine to	o megium SAND, littli	باااد د		21.0/			
		9	-	1						21.0′			
		11								1			
		-	1							1 1	SILTY SAND		
			1	1									
			1	1	ľ					1			
٦٢			4										
25		10	507	25.0		_Collection		5-11-		26.0'			
		10	SS7 18"	25.0 27.0	Top 12": (2": Grey, brown, fine to medium SAND, little Silt. n 6": Olive brown, varved SILT and fine to medium Sand.							
		14	1		POROUM 6,	varvec	_ S_E, and this to life	النسب	- 1				
		17			l						CTI T AND CAND		
					İ					1	SILT AND SAND		
			-										
			1										
			1	1	ŀ								
			1							<u> </u>			

SI	FOOT	OF BRO	JOHNSI AD STRI NECTICU			TEST B	ORING REPO	ORT	BORING NO. HJ-1		
_	JECT		Broad Stree				GROUND WATER READ	INGS	FILE NO.	30202	
	ATION		d, Connectic			6/30/04	1830	DEPTH 21.0'	SHEET NO. LOCATION	2 OF 2 See Plan	
CLIE			Capital Corp.		Torn	6/30/04	1030	21.0	ELEVATION	TO A STATE OF THE	
CON	TRACTOR			& Associates DRIVE	CORE		THE SOLUTIONS A DOCC	PEDLIDEC	DATUM	NGVD-29	
		TIEM CASING SAMPLER BARREL BARREL				EDUKES	DATE	<u>06/30/04</u> TO <u>06/30/04</u>			
TYPE	E DE DIAMETER	R (TN)	HSA 2-1/4	SS 1-3/8		RIG TYPE: BIT TYPE:	Mobile Drilling B-50		START	1730 FINISH 2000	
HAM	MER WEIGHT	T (LB)	722	140		DRILL MUD:	Safety hammer via Cathe	ad and rope	DRILLER H & J REP	Anthony Scaife Ryan M. Laird	
D HAM	MER FALL	(IN)		30		HAMMER TYPE:	Safety Hammer via Cathe	ad and Tope	11 d 3 KEI	NION TO COMO	
E P T H	CASING BLOWS PER FT	SAMPLER BLOWS PER 6 IN	SAMPLE TYPE NO. & REC.	SAMPLE DEPTH (FT)			SCRIPTION AND REMARKS		ELEV./ DEPTH (FT)	STRATUM DESCRIPTION	
30		7 8 9 15	SS8 18″	30.0 32.0	Medium de	nse, brown, orange,	SILT and fine to medium	Sand.			
										SILT AND SAND	
35		100/6"	SS9 6"	35.0 35.5	Medium de	ense, brown, fine to o 6").	coarse SAND and Silt (sam	nple penetrated rock			
						•			36.0′	E.O.B. Auger Refusal	
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			1		NOTES: Auger refu	ısal at 36.0′ <u>.</u>					
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			1								

CT	FOOT	OF BRO	JOHNSE AD STRE		Ì	T	EST BO	RING REP	ORT	BORING N	Ю. НJ-2		
PRO3			Broad Stree		1			OUND WATER REAL		FILE NO.	30202		
	TION		d. Connectic				DATE	TIME	DEPTH	SHEET NO.	1 OF2		
CLIE		Bildner	Capital Corp.				6/30/04	1130	21.0′	LOCATION	See Plan		
	TRACTOR	Hardim	rdiman Company & Associates, Inc.						ELEVATION				
	ITEM		CASING	DRIVE SAMPLER	CORE BARREL		DRILLING	EQUIPMENT & PRO	CEDURES	DATUM DATE	NGVD-29 06/30/04 TO 06/30/0		
TYPE			HSA	SAMPLER	DANNEL	RIG T	YPE: Mo	bile Drilling B-50		START	0945 FINISH 1245		
INSID	DE DIAMETER		2-1/4	1-3/8		BITT				DRILLER	Anthony Scaife		
	MER WEIGHT MER FALL	(LB) (IN)	377	140 30		HAMM	L MUD: MER TYPE: Safe	ety hammer via Cath	ead and rope	H & J REP	Rvan M. Laird		
D						_							
E	CASING BLOWS	SAMPLER BLOWS	SAMPLE TYPE	SAMPLE				VOTTON AND DESCRIPTION	5	ELEV./ DEPTH	STRATUM DESCRIPTION		
P T	PER	PER	NO. &	DEPTH (FT)			VISUAL DESCR	UPTION AND REMARK	3	(FT)	5		
Н	FT	6 IN	REC.	(/									
0		3	SS1	0		T. Cl. State China and Table					CEDAR CHIPS		
		6	16"	1.6	Top 6": Ce	dar Chir	ps and Topsoil. brown, SILT and	I Sand, trace Roots,	trace fine Gravel.	0.5'	FILL		
Ī		7			DOLLOIT 10	, JOHVE	STOTTING SEET BITC			1.5*			
L		50/1"			1					1.5			
			1										
ŀ		10	SS2	3.0	1., .			CDAVEL (C-LLI)					
		70	12"	5.0	Very dense	e, plack,	wnite and orang	ge GRAVEL (Cobbles)	•		CAMP CRAUEL AND		
ŀ		31	1								SAND, GRAVEL AND COBBLES (FILL)		
		15									000000 ()		
5		50	SS3	5.0	Top 6": Bla	ack, whi	ite GRAVEL.						
1		37	12"	7.0	Bottom 6"	: Grey, (GRAVEL, little Sil	t, little Sand, trace R	oots.				
		21	1										
-		19 20	SS4	7.0	1		C .	CAND	Cilt. little Cravel	7.0′			
	2)	23	16"	9.0	Dense, ligi	ht grey,	orange, fine to o	coarse SAND, some S	ont, nittle Gravel.				
ŀ		14	1										
		14	1										
Ī					ř.								
10				10.0	Control little Silt								
		27	SS5 14"	10.0 12.0	Very dens	Very dense, light grey, fine to coarse SAND, some Gravel, little Silt.							
-		41	1 **	12.0									
		47 41	1										
-		71			1								
			1										
ı]										
l			4										
[] ا			1	1									
15		14	SS6	15.0	Ton E"	rev fine	to medium SAN	D, little Gravel, little	Silt.				
		28	18"	17.0	Bottom 10	ייבי, ווויפ ": Grey,	, orange, fine to	coarse SAND, some	Gravel, trace Silt				
ŀ		18	1	1	- Albacootti	,	-				GRAVELLY SAND		
		20			1								
ĺ													
		-	4										
			1		1								
1			1	1	1								
_]				_				
20		7	SS7	20.0				to coarse GRAVEL,	some fine to coarse				
Į		5	6"	22.0	Sand, trac	re Siit (V	wetj.						
		15	4										
		11			1								
İ			-								ľ		
		-	1								1		
										1	1		
25										1			
ĺ	5 SS8 25.0 Medium der 5 5 5 5		lense, gr	rey, fine to coars	se SAND, trace Grave	el, trace Silt (Wet)		1					
ļ			lium dense, grey, fine to coarse SAND, trace Gravel, trace Silt (Wet).					1					
		5	1										
1					1	NOTES:					1		
			1	1									
1					red cobb	bles while augeri	ng from 1.5' to 7.0',			1			
			4										
- 1													

CT.	F001	OF BRO	AD STRI			TEST BO	RING REPO	ORT	BORING NO. HJ-2			
PRO:			Broad Stree			GRO	OUND WATER READI		FILE NO.	30202		
	ATION		. Connectic			DATE	TIME	DEPTH	SHEET NO.	2 OF2		
CLIE			Capital Corp.			6/30/04	1130	21.0′	LOCATION	See Plan		
CON	TRACTOR			& Associates	. Inc.				ELEVATION			
	ITEM		CASING	DRIVE SAMPLER	CORE BARREL	DRILLING	EQUIPMENT & PROCE	EDURES	DATUM	NGVD-29 06/30/04 TO 06/30/04		
TYPE			HSA	SAMPLER	DAKKEL	RIG TYPE: Mo	bile Drilling B-50	DATE START	0945 FINISH 1245			
INSI	DE DIAMETE	TER (IN) 2-1/4 1-3/8 BIT TYPE:					DRILLER	Anthony Scaife				
	MER WEIGH MER FALL	T (LB) (IN)		140 30		DRILL MUD: HAMMER TYPE: Safe	etv hammer via Cathea	ad and rope	H & J REP	Rvan M. Laird		
D	MER FALL	(114)		30		100000000000000000000000000000000000000						
E	CASING	SAMPLER	SAMPLE	SAMPLE					ELEV./	STRATUM DESCRIPTION		
P	BLOWS PER	BLOWS PER	TYPE NO. &	DEPTH (FT)		VISUAL DESCR	LIPTION AND REMARKS		DEPTH (FT)	STRATUM DESCRIPTION		
н	FT	6 IN	REC.	(1)					` ′			
30		38	SS9	30.0	Top 8": Ol	live brown, fine to coarse	SAND, little Gravel.					
"		58	12"	32.0	Bottom 4":	: Highly Weathered, blac	k, white ROCK (gneiss)).				
1 1		17										
		24										
										(1		
			ł						1	GRAVELLY SAND		
1			1									
35		35	SS10	35.0	Medium de	ense, grey, fine to coarse	SAND, some fine to c	oarse Gravel.				
		15	10"	37.0								
		12	1									
		12										
			1									
			İ						38.0′			
			1						1			
1 1			1									
40							10 1 6:11:/1	liable weekboood				
		15	SS11 12"	40.0 42.0	Dense, gro mica gneis	ey, fine to coarse Sand a	ind Gravel, some Silt (F	ngniy weathered				
		17	12	72.0	Tilled gires	33/-				GLACIAL TILL		
		19	-							GEACIAL TILL		
		20										
			1									
			1									
]									
			1									
45		50/0"		-					45.0′	E.O.B.		
		50/0	1	1	Fractured	rock in tip, black, white,	orange Gneiss.			Auger Refusal		
			1		Tibetarea	TOCK III cip, block, white,	0.450		1 1			
			1									
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	NOTES 1) Cobi				NOTES:	on ancountered at 201b	ile augering					
	1)				2) Auger	es encountered at 38' wh refusal at 45.0'.	ne augering.					
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1			1	1	l .				1	I		

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6.3	FOOT	OF BRO	JOHNSI AD STRI			TEST BO	RING REPO	ORT	BORING NO. HJ-3			
$\overline{}$	JECT JECT		Broad Stree		1	GR	OUND WATER READ		FILE NO.	30202		
	ATION		d. Connectic			DATE	TIME	DEPTH	SHEET NO.	OF2		
CLIE		Bildner	Capital Corp.			6/30/04	1830	21.0′	LOCATION	See Plan		
CON	TRACTOR	Hardim	an Company	& Associates		<u>, </u>			ELEVATION	17.6' NGVD-29		
	ITEM		CASING	DRIVE SAMPLER	CORE BARREL	DRILLING	G EQUIPMENT & PROC	EDURES	DATUM DATE	NGVD-29 06/30/04 TO 06/30/04		
TYPE			HSA	SS			bile Drilling B-50		START	0700 FINISH 0900		
INSIDE DIAMETER (IN) 2-1/4 1-3/8 BIT TYPE: HAMMER WEIGHT (LB) 140 DRILL MUD:						DRILLER	Anthony Scaife					
	MER FALL	(IN)	54	30		HAMMER TYPE: Cat	head with rope		H & J REP	Rvan M. Laird		
D E	CASING	SAMPLER	SAMPLE						ELEV./			
P	BLOWS	BLOWS	TYPE	SAMPLE DEPTH		VISUAL DESCR	RIPTION AND REMARKS		DEPTH	STRATUM DESCRIPTION		
T H	PER FT	PER 6 IN	NO. & REC.	(FT)					(FT)			
										ASPHALT		
0		17	SS1	0.5	Very dense	e, brown, fine to coarse	SAND, some fine to co	arse Gravel	0.25′	***************************************		
		29	16"	2.5	(Asphalt),	little Silt (Fill).						
		29		1								
		15			Dance bro	ense, brown, fine to coarse SAND, some fine to coarse Gravel, little Silt (Fill						
		18 20	SS2 8"	2.5 4.5	Delise, of	omy and to course oray	, 55	,		- 		
		15	1	(65						FILL		
		13					CAND	SIE BHIO C-200				
5		5	SS3 12"	4.5	Medium de	ense, red, brown, fine to	coarse SAND, some S	iit, little Gravel.				
3		22	12	6.0								
		100							1			
			1									
]						7.0′			
			1									
			1									
			1									
10												
		8	SS4	10.0	Top 8": Or	range, brown, medium S ': Grey, brown, GRAVEL,	AND, trace Gravel, tra					
		10	12"	12.0	BULLUIII 4	. Grey, brown, Grovec,	Some fine to course of	ario, crace succ				
		12 12	1									
		12	_									
			1									
			1									
			-									
15			1									
13		32	SS5	15.0	Verv dens	se, white, brown, fine to	coarse GRAVEL, some	fine to coarse Sand,				
		36	14"	17.0	trace Silt.							
		38 47	4									
		4/		 						SAND AND GRAVEL		
	3		1									
]									
			1							1		
	8		1									
20		9	SS6	20.0	Medium d	lense, grey, fine to coars	e SAND, some fine to	coarse Gravel, trace				
		9	16"	22.0	Silt (Wet).				1			
		8	1									
		8										
			1									
			1									
25			-									
~		6	SS7	25.0	Medical	dense, grey, fine to coars	a SAND trace Gravel	trace Silt (Wet)				
		7	6"	27.0	Medium d	iense, grey, fine to coars	E SAND, WALE GRAVEL,	ande out (wet)				
		9]									
		10		-								
			-									
			1		NOTE:							
			1		Cobbles e	encountered at 7' while a	ugering.					
			-									

		OF BRO	JOHNS	ET		TES	EST BORING REPORT BORING NO. GROUND WATER READINGS FILE NO. 30				О. НЈ-3	
$\overline{}$	JECT		Broad Stree				GRO	UND WATER READI	NGS	FILE NO.	30202	
	ATION		. Connectic			Di	ATE	TIME	DEPTH	SHEET NO.	2 OF2	
CLIE			Capital Corp.			6/3	30/04	0810	20.5′	LOCATION	See Plan	
	ITRACTOR			& Associates	Inc.				1	ELEVATION 17.6' DATUM NGVD-29		
	ITEM		CASING	DRIVE	CORE BARREL		DRILLING I	EQUIPMENT & PROCI	EDURES	DATUM	NGVD-29 06/30/04 TO 06/30/04	
TYP			HSA	SAMPLER SS	BARKEL	RIG TYPE:	Mobi	le Drilling B-50		DATE START	0700 FINISH 0900	
INSI	DE DIAMETER		2-1/4	1-3/8		BIT TYPE:		-		DRILLER	Anthony Scaife	
	IMER WEIGHT IMER FALL	(LB) (IN)	-	140 30		DRILL MUD HAMMER T); YPE: Safet	y hammer via Cathea	ad and rope	H & J REP	Rvan M. Laird	
D	IMER FALL	(114)		- 50	_	100000		,				
E P T	CASING BLOWS PER FT	SAMPLER BLOWS PER 6 IN	SAMPLE TYPE NO. & REC.	SAMPLE DEPTH (FT)		VISUAL DESCRIPTION AND REMARKS					STRATUM DESCRIPTION	
Н 30		7	SS8	30.0 32.0	Medium de Silt (Wet).	nse, grey, fin	e to coarse S	SAND, little fine to co	arse Gravel, trace			
		10	18"	32.0	Siit (Wet).							
		22									SAND AND GRAVEL	
35										35.0'		
35		15 10	SS9 12"	35.0 37.0	Top 6": Gr	ey, Varved, fi	ne to mediur	m SAND and Silt. Irse SAND, little Grav	ral little Silt trace	35,0		
		14			Weathered	Reduish grey Rock (at bot	tom).	ilse SAND, illie Grav	ci, neie one elect		SILTY SAND	
		15					Ð					
										38.0′	WEATHERED ROCK	
										39.0′	E.O.B. Auger Refusal	
40			1									
			1									
45			1									
45			1									
i i			1									
			1									
			1									
			1									
			1									
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50]									
			4									
			1									
			1									
			1									
			1									
			1									
55			1									
	1		-									
			1									
		_	1		NOTES:							
			1			usal at 39.0′,						
			-							1		
1			4	1 1						1	I	

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			TEST PIT LOG			
	Environmental, Inc. and Scientists		<u>PROJECT</u> 128-132 Broad Street Stamford, CT		No. <u>TP-2</u> No. 05.004 d by J. Day	
_	ineer M. Harris Sunny, 40°F		EXCAVATION EQUIPMENT Contractor Conte Company, LLC Operator Tim Sargent Make CAT Model 303 E Capacity 0.5 cu.yd. Reach 8 ft	Date Ground Ele Time Starte Time Comp	evation 1 ed 083	
Depth (ft)		(SURFACE SKETCH NOT TO SCALE)	Excav. Effort	Boulder Count Qty. Class	Remark No.
	0.5'	Silt, 1	brown, fine to coarse SAND, some Gravel, some race Roots, trace Glass, trace Brick, Dry	Е		
- 1 -	2'	Brow	SOIL/FILL) n, fine to coarse SAND and GRAVEL, little Silt,	E		
- 2 - - 3 -		Brow	Roots, trace Bricks, trace Metal, Dry (FILL) n, fine to coarse SAND and GRAVEL, some	Е		
		Brick	s, some Concrete, little Silt (FILL)	Е	2A	1, 2, 3
- 4 -	5'			E	2A, 5B	4, 5
- 5 - - 6 - - 7 - - 8 - - 9 - - 10 -		В	ottom of exploration 5.0 feet below grade.			
_ 11 _						
= 12 =						

- 1. Stacked bricks and boulders observed from 0.5 to at least 5 feet on the west test pit wall adjacent to the neighboring, existing building. Bricks and boulders could be foundation remnants of former building onsite. Adjacent building foundations were not evident due to cobbles and boulders. Exploration was terminated at 5 feet due to proximity to the adjacent building.
- 2. Test pit walls were screened with a 10.6 eV MiniRAE photoionization detector (PID). PID values represent meter response in parts per million (ppm) relative to benzene in air and above background readings. At 4 ft depth: North = 0.6 ppm, East = 0.9 ppm, South = 0.9 ppm. Environmental sample collected from east test pit wall at 4 feet below ground surface
- 3. Boulders observed at approximate 4.5 feet below ground surface, possibly foundation remnants.
- 4. The test pit was backfilled with approximately five, 12-inch lifts of excavated material and compacted with excavator bucket and observed to be firm and stable.

TEST PIT PLAN		<u>LEGEND</u>														
1 2 1	BOULDER	COUNT	PROPORT		ABBREVIATIONS	EXCAVATION EFFORT										
North Depth = 5 Volume = 2.6 Cu.yd.	Size Range Classification 6" - 18" 18" - 36" 36" and Larger	Letter Designation A B C	TRACE (TR) LITTLE (LI) SOME (SO) AND	0-10% 10-20% 20-35% 35-50%	F - Fine M - Medium C - Coarse F/M - Fine to Medium F/C - Fine to Coarse V - Very GR - Gray BN - Brown YEL - Yellow	E - Easy M - Moderate D - Difficult GROUNDWATER Elapsed Time 15 mins G.W.L. Not Encountered										

		TEST PIT LOG								
GZA GeoEnvi Engineers and	ironmental, Inc. Scientists	<u>PROJECT</u> 128-132 Broad Street Stamford, CT	Test Pit No. TP-3 File No. 05.0046879.01 Reviewed by J. Davis							
GZA Engineer Weather Sur		EXCAVATION EQUIPMENT Contractor Conte Company, LLC Operator Tim Sargent Make CAT Model 303 E Capacity 0.5 cu.yd. Reach 8 ft	Date 11/19/21 Ground Elevation 17.8 Time Started 0915 Time Completed 1000							
Depth (ft)		SUBSURFACE SKETCH (NOT TO SCALE)	Excav. Effort	Boulder Count Qty. Class	Remark No.					
	0.5	Dark brown, fine to coarse SAND and fine GRAVEL, some Silt, trace Roots, Dry (TOPSOIL)	Е							
1 -	2,	Light brown, fine to coarse SAND and GRAVEL,	E							
- 2 -		little Silt (FILL) Brown/dark brown, fine to coarse SAND and	Е							
- 3 -	Concrete Foundation	GRAVEL, little Silt, little Bricks, little Concrete, trace Metal, trace Plastic, Dry (FILL)	М	2A						
- 4 -		, , ,	Е	2A, 5B	1					
5 -	6,		Е		2					
- 6 -	West	Brown, fine to coarse SAND and GRAVEL, some oricks, little Silt, little Fly Ash, trace Plastic, trace	М							
7 -		Metal, trace Wood, trace Glass (FILL)	M							
8 -	8.5	(CONCRETE SLAB)	D		3					
- 9 -	Concrete Slab	Bottom of exploration 8.5 feet below grade.								
_ 10										
_ 11 _										
- 12 -										
REMARKS:	. C. letiene energy	orad along porth and east test nit walls extending from ah	out 4 to 8 5 f	eet below gra	ade.					

- 1. Concrete foundations encountered along north and east test pit walls extending from about 4 to 8.5 feet below grade. Horizontal limits of foundations outside of the test pit were not determined.
- 2. Test pit walls were screened with a 10.6 eV MiniRAE photoionization detector (PID). PID values represent meter response in parts per million (ppm) relative to benzene in air and above background readings. At 5.5 ft depth: West = 1.8 ppm, South = 1.7 ppm. Environmental samples were taken from west test pit wall from 5.5 feet below ground surface.
- 3. Exploration was terminated at 8.5 feet below ground surface due to bucket refusal on suspected concrete slab. The test pit was backfilled with approximately eight, 12-inch lifts of excavated material compacted with the excavator bucket and observed to be firm and stable.

TEST PIT PLAN		<u>LEGEND</u>														
1 46 1	BOULDER	COUNT	PROPORT	TIONS	ABBREVIATIONS	EXCAVATION EFFORT										
6' 3.5'	Size Range Classification 6" - 18" 18" - 36" 36" and Larger	Letter Designation A B C	TRACE (TR) LITTLE (LI) SOME (SO) AND	0-10% 10-20% 20-35% 35-50%	F - Fine M - Medium C - Coarse F/M - Fine to Medium F/C - Fine to Coarse V - Very GR - Gray BN - Brown YEL - Yellow	E - Easy M - Moderate D - Difficult GROUNDWATER Elapsed Time 15 mins G.W.L. Not Encountered										



Photographic Log

Client Name:
F. D. Rich Construction Company

Site Location:

128-132 Broad Street Stamford, Connecticut **Project No.** 05.0046879.01

Photo No.

Date: 11/19/21

Direction Photo Taken:

North

Description:

TP-1

Bricks observed in Fill.

Possible Foundation Remnants

Sand and Gravel observed beneath Fill.

Photo No.

Date: 11/19/21

Direction Photo Taken:

Northwest

Description:

TP-1 Spoil Pile





Photographic Log

Client Name:

F. D. Rich Construction Company

Site Location:

128-132 Broad Street Stamford, Connecticut **Project No.** 05.0046879.01

Photo No.

Date: 11/19/21

Direction Photo Taken:

Northwest

Description:

TP-2

Stacked brick and boulders adjacent to neighboring existing building, possibly foundation remnants.

Adjacent building foundations were not evident.



Photo No.

Date: 11/19/21

Direction Photo Taken:

East

Description:

TP-2 spoil pile.





Photographic Log

Client Name:

F. D. Rich Construction Company

Site Location:

128-132 Broad Street Stamford, Connecticut **Project No.** 05.00468791.01

Photo No.

Date: 11/19/21

Direction Photo Taken:Northeast

Description:

TP-3

Concrete foundations encountered along north and west test pit sidewalls from about 4 to 8.5 feet below ground surface.

Test pit refusal on concrete slab at approximately 8.5 feet below ground surface.



Photo No.

Date: 11/19/21

Direction Photo Taken:

West

Description:

TP-3 Spoil Pile



Appendix G:
Existing Strom Drain
Conveyance System Capacity

Note: All capacity calculations are based on mannings equation

Existing Storm Drainage Conveyance System

							Qfull using
						Existing25	Mannings
Uphill	Downhill					yr Storm	Equation
Structure	Structure	Size (in)	Туре	n	Slope (ft/ft)	(CFS)	(CFS)
Ex. SDMH #1	Ex. SDMH #2	24	RCP	0.013	0.0049	21.31	15.9
Ex. SDMH #2	Ex. SDMH #3	18	RCP	0.013	0.0390	20.98	20.8
Ex. SDMH#3	Downstream	24	RCP	0.013	0.0084	-	20.8
Ex. CB#1	Ex. SDMH#6	12	RCP	0.013	0.006	1.09	2.8
Ex. SDMH #6	Downstream	18	RCP	0.013	0.004	1.09	6.7

Appendix H: Conveyance Computations

The following is a summary of the computations performed to design the proposed storm drainage system drain sizes. The proposed watershed flows were taken from the results of the HyrdoCAD storm drainage analysis performed on the site. Refer to Appendix "L" for HydroCAD model input data, computations, and results. Refer to Exhibit "B" for a depiction of the proposed on-site watershed areas. HydroCAD runoff computations are based on the 25-year design storm frequency event. Culvert conveyance computations are based on the Manning's Equation.

Culvert Capacity Summary Table

Maximum pipe capacities were calculated using the Manning equation for full flow conditions. The proposed pipe information, 25-year peak design flows, and corresponding maximum capacities are summarized in the following table. Refer to the Development Plan for pipe and structure locations. All pipes have been sized to convey the flow rates for at least the 25-year design storm frequency event.

Uphill Structure	Downhill Structure	Diameter (in)	Tyne	Roughness (n)	Slope (ft/ft)	25-yr Storm (CFS)	Qfull using Mannings Equation (CFS)
JB#2	JB#1	12	PVC	0.011	0.006	2.30	3.27
JB#1	Double CB	12	PVC	0.011	0.005	2.30	2.99
Double CB	SDMH#5	18	PVC	0.011	0.005	12.82	17.60
SDMH#5	SDMH#4	18	PVC	0.011	0.005	12.82	17.60
SDMH#4	SDMH#3	18	PVC	0.011	0.005	16.97	17.60
Ex. SDMH	SDMH#3	24	PVC	0.011	0.005	5.22	18.96
SDMH#3	SDMH#2	18	PVC	0.011	0.005	21.93	17.60
SDMH#2	SDMH#1	18	PVC	0.011	0.005	21.93	17.60
SDMH#1	Ex. SDMH#2	18	PVC	0.011	0.005	20.46	17.60
Ex. SDMH#	Ex. SDMH#3	18	PVC	0.011	0.039	20.87	24.58
CB#1	JB#3	12	PVC	0.011	0.010	0.05	4.22
SDMH#1	JB#3	8	PVC	0.011	0.005	1.54	1.01
JB#3	Ex. SDMH#6	12	PVC	0.011	0.010	1.59	4.22

Appendix I: Stage-Area-Storage Tables	
22	

Page 1

Stage-Area-Storage for Pond 5P: Ex. SDMH #1 / POC A

Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)
13.20	0	15.80	186
13.25	1	15.85	245
13.30	1	15.90	326
13.35	2	15.95	432
13.40	2 3 3	16.00	564
13.45	3	16.05	729
13.50	4	16.10	930
13.55	4	16.15	1,171
13.60	4 5 6	16.20	1,456
13.65	0	16.25	1,798
13.70	6 7	16.30 16.35	2,210 2,690
13.75 13.80	8	16.40	3,232
13.85	8	16.45	3,843
13.90	9	16.50	4,530
13.95	9	16.55	5,290
14.00	10	16.60	6,121
14.05	11	16.65	7,027
14.10	11	16.70	8,011
14.15	12	16.75	9,063
14.20	13	16.80	10,174
14.25	13	16.85	10,174
14.30	14	16.90	10,175
14.35	14	16.95	10,175
14.40	15	17.00	10,175
14.45	16	17.05	10,175
14.50	16	17.10	10,175
14.55	17		
14.60	18		
14.65	18		
14.70	19		
14.75	19		
14.80	20		
14.85	21		
14.90	21		
14.95 15.00	22 23		
15.05	23		
15.10	24		
15.15	25		
15.20	25		
15.25	26		
15.30	26		
15.35	27		
15.40	28		
15.45	29		
15.50	32		
15.55	39		
15.60	54		
15.65	76		
15.70	105		
15.75	141		
		ļ.	

Page 2

Stage-Area-Storage for Pond 10P: Parking Lot

			_
Elevation (feet)	Storage (cubic-feet)	Elevation (feet)	Storage (cubic-feet)
13.40		16.00	564
	0		
13.45	1	16.05	723
13.50	2	16.10	915
13.55	2	16.15	1,144
13.60	3	16.20	1,412
13.65	2 2 3 4	16.25	1,733
13.70	5	16.30	2,119
13.75	6	16.35	2,568
13.80	6	16.40	3,071
13.85	7	16.45	3,636
13.90	8	16.50	4,268
	9	16.55	4,959
13.95	10		5,700
14.00		16.60	
14.05	10	16.65	6,493
14.10	11	16.70	7,337
14.15	12	16.75	8,237
14.20	13	16.80	9,197
14.25	14	16.85	9,197
14.30	14	16.90	9,197
14.35	15	16.95	9,197
14.40	16	17.00	9,197
14.45	17	17.05	9,197
14.50	18	17.10	9,197
14.55	18		•
14.60	19		
14.65	20		
14.70	21		
14.75	22		
14.80	22		
14.85	23		
14.90	24		
14.95	25		
15.00	26		
15.05	26		
15.10	27		
15.15	28		
15.20	29		
15.25	30		
15.30	30		
15.35	31		
15.40	32		
15.45	34		
15.50	37		
15.55	44		
15.60	59		
15.65	82		
15.70	110		
15.75	145		
15.80	190		
15.85	249		
15.90	329		
15.95	433		

Page 3

Stage-Area-Storage for Pond 17P: Retention System#1

Elevation	Storage	Elevation	Storage
(feet)	(cubic-feet)	(feet)	(cubic-feet)
9.20	0	14.40	7,248
9.30	78	14.50	7,395
9.40	155	14.60	7,542
9.50	233	14.70	7,689
9.60	310	14.80	7,706
9.70	388 534	14.90 15.00	7,723 7,741
9.80 9.90	679	15.00	7,741
10.00	825	15.20	7,776
10.10	970	15.30	7,793
10.20	1,116	15.40	7,805
10.30	1,262	15.50	7,806
10.40	1,407	15.60	7,808
10.50	1,553	15.70	7,809
10.60	1,698	15.80	7,810
10.70	1,844	15.90	7,811
10.80	1,989	16.00	7,813
10.90	2,135	16.10	7,814
11.00	2,281	16.20	7,815
11.10	2,426	16.30	7,816
11.20 11.30	2,572	16.40 16.50	7,818 7,819
11.40	2,717 2,863	16.60	7,819 7,820
11.50	3,009	16.70	7,821
11.60	3,154	16.80	7,823
11.70	3,300	16.90	7,824
11.80	3,445	17.00	7,825
11.90	3,591	I	
12.00	3,736		
12.10	3,882		
12.20	4,028		
12.30	4,173		
12.40	4,319		
12.50	4,464		
12.60 12.70	4,610 4,756		
12.70	4,730 4,901		
12.90	5,047		
13.00	5,192	100	
13.10	5,339		
13.20	5,486		
13.30	5,633		
13.40	5,780		
13.50	5,926		
13.60	6,073		
13.70	6,220		
13.80	6,367		
13.90 14.00	6,514 6,661		
14.10	6,808		
14.10	6,954		
14.30	7,101		
	.,	,	



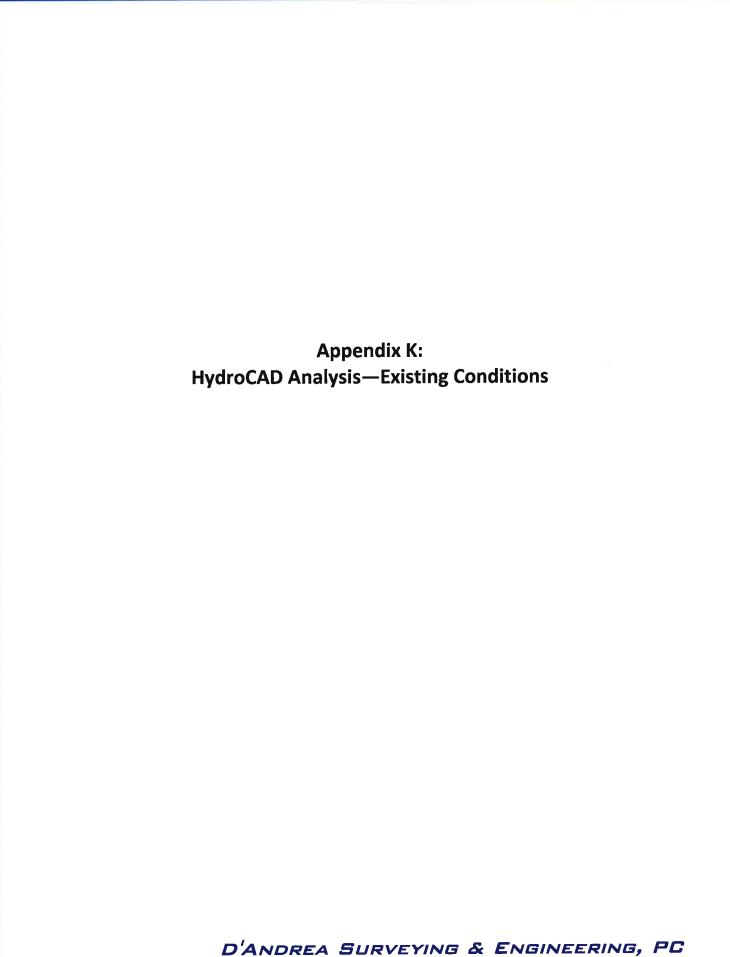
HydroCAD Summary TR Broad II, LLC 128 Broad Street Stamford, CT Project ID: 21UT

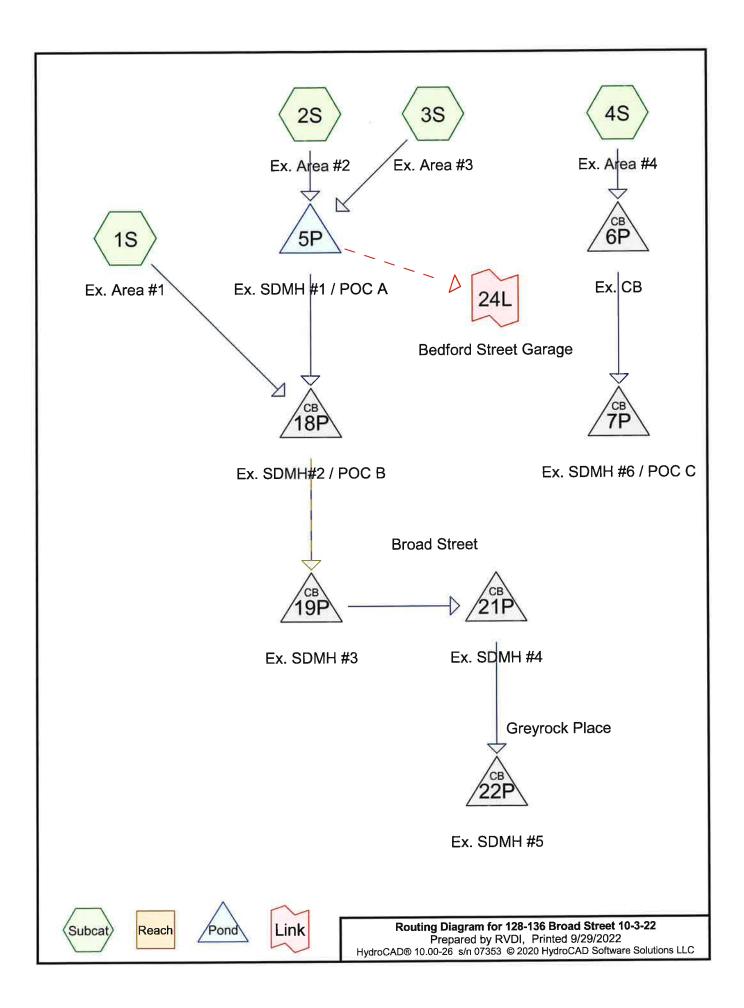
	1 Year Storm 2 Ye						r Storm		5 Year Storm					10 Yea	r Storm			25 Yea	r Storm			50 Year	r Storm		100 year Storm			
POC	q _{ex} (ft³/s)	q _p (ft ³ /s)	Δq (ft³/s)	%∆q (ft³/s)	q _{ex} (ft ³ /s)	q _p (ft ³ /s)	Δq (ft³/s)	%∆q (ft³/s)	q _{ex} (ft³/s)	q _p (ft³/s)	Δq (ft³/s)	%∆q (ft³/s)	q _{cs} (ft ³ /s)	q _p (ft ³ /s)	Δq (ft³/s)	%∆q (ft³/s)	q _{ex} (ft³/s)	q _p (ft ³ /s)	$\Delta q (ft^3/s)$	%∆q (ft³/s)	q _{ck} (ft ³ /s)	q _p (ft³/s)	$\Delta q (ft^3/s)$	%∆q (ft³/s)	q _{ex} (ft ³ /s)	q _p (ft ³ /s)	Δq (ft³/s)	%Δq (ft³/s)
A	9,65	8,76	-0.89	-9%	11,43	10,64	-0.79	-7%	15.20	13.72	-1,48	-10%	18,01	18.88	0.87	5%	21.31	21.93	0.62	3%	23,42	20,80	-2,62	-11%	25,31	33.72	8,41	33%
В	10.02	8,90	+1.12	-11%	11.91	10,67	-1.24	-10%	15,91	13.22	-2.69	-17%	18.88	17.86	-1.02	-5%	20,98	20.87	-0.11	-1%	21.26	19,79	-1,47	-7%	21.32	31,80	10,48	49%
С	0.31	0.04	-0.27	-87%	0.43	0.18	-0,25	-58%	0.65	0.82	0.17	26%	0,83	1,28	0.45	54%	1.09	1.59	0.50	46%	1.29	1.54	0,25	19%	1,50	2,04	0.54	36%
Parking Garage	0.00	0.00	0,00	0%	0.00	0.00	0.00	0%	0.00	0.00	0.00	0%	0.00	0,00	0,00	0%	1.30	0,73	-0,57	3	3.87	3.25	-0.62	-16%	7.99	9.90	1,91	24%

Table 1: Comparison of Existing and Proposed Peak Flow Rates for all Points of Concern.

		1 Year S	Storm			2 Yea	r Storm			5 Year	Storm			10 Yea	r Storm			25 Yea	r Storm			50 Year	Storm			100 Year	Storm	
POC	Vex (cf)	Vp (cf)	Δv (cf)	%∆v (cf)	Vex (cf)	Vp (cf)	Δv (cf)	%Δv (cf)	Vek (cf)	Vp (cf)	Δv (cf)	%Δv (cf)	_{Vex} (cf)	v _p (cf)	Δv (cf)	%∆v (cf)	_{Vex} (cf)	Vp (cf)	Δv (cf)	%∆v (cf)	_{Vex} (cf)	Vp (cf)	Δv (cf)	%∆v (cf)	_{Vex} (cf)	Vp (cf)	Δv (cf)	%Δv (cf)
A	38,300	36,837	-1,463	-4%	47,066	46,486	-580	-1%	61,709	62,381	672	1%	73,804	75,481	1,677	2%	90,293	93,553	3,260	4%	102,445	105,598	3,153	3%	115,658	115,447	-211	0%
В	39,553	37,450	-2,103	-5%	48,695	47,181	-1,514	-3%	63,974	63,004	-970	-2%	76,601	75,553	-1,048	-1%	93,174	92,894	-280	0%	103,996	104,583	587	1%	114,845	113,954	-891	-1%
С	1,239	79	-1,160	-94%	1,723	154	-1,569	-91%	2,576	484	-2,092	-81%	3,313	1,247	-2,066	-62%	4,375	2,273	-2,102	-48%	5,173	2,847	-2,326	-45%	6,049	3,560	-2,489	-41%
Parking Garage	0	0	0	0%	0	0	0	0%	0	0	0	0%	0	0	0	0%	666	183	-483	(3.0)	2,551	1,860	-691	-27%	5,518	6,461	943	17%

Table 2: Comparison of Existing and Proposed Runoff Volumes for all Points of Concern.





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Page 2

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Ex. Area #1 Runoff Area=7,923 sf 51.43% Impervious Runoff Depth=1.90"

Flow Length=181' Tc=5.8 min CN=89.3 Runoff=0.40 cfs 1,253 cf

Subcatchment 2S: Ex. Area #2 Runoff Area=132,315 sf 97.01% Impervious Runoff Depth=2.68"

Tc=10.0 min CN=97.5 Runoff=7.56 cfs 29,584 cf

Subcatchment 3S: Ex. Area #3 Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=2.74"

Tc=5.0 min CN=98.0 Runoff=2.58 cfs 8,717 cf

Subcatchment 4S: Ex. Area #4 Runoff Area=12,053 sf 0.54% Impervious Runoff Depth=1.23"

Flow Length=119' Tc=13.7 min CN=80.1 Runoff=0.31 cfs 1,239 cf

Pond 5P: Ex. SDMH #1 / POC A Peak Elev=15.11' Storage=24 cf Inflow=9.67 cfs 38,300 cf

Primary=9.65 cfs 38,300 cf Secondary=0.00 cfs 0 cf Outflow=9.65 cfs 38,300 cf

Pond 6P: Ex. CB Peak Elev=12.70' Inflow=0.31 cfs 1,239 cf

12.0" Round Culvert n=0.013 L=98.0' S=0.0061 '/' Outflow=0.31 cfs 1,239 cf

Pond 7P: Ex. SDMH #6 / POC C Peak Elev=11.99' Inflow=0.31 cfs 1,239 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=0.31 cfs 1,239 cf

Pond 18P: Ex. SDMH#2 / POC B Peak Elev=14.54' Inflow=10.02 cfs 39,553 cf

Primary=10.02 cfs 39,553 cf Secondary=0.00 cfs 0 cf Tertiary=0.00 cfs 0 cf Outflow=10.02 cfs 39,553 cf

Pond 19P: Ex. SDMH #3 Peak Elev=12.46' Inflow=10.02 cfs 39,553 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=10.02 cfs 39,553 cf

Pond 21P: Ex. SDMH #4 Peak Elev=10.04' Inflow=10.02 cfs 39,553 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=10.02 cfs 39,553 cf

Pond 22P: Ex. SDMH #5 Peak Elev=9.25' Inflow=10.02 cfs 39,553 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=10.02 cfs 39,553 cf

Link 24L: Bedford Street Garage Inflow=0.00 cfs 0 cf

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Ex. Area #1 Runoff Area=7,923 sf 51.43% Impervious Runoff Depth=2.47"

Flow Length=181' Tc=5.8 min CN=89.3 Runoff=0.52 cfs 1,629 cf

Subcatchment 2S: Ex. Area #2 Runoff Area=132,315 sf 97.01% Impervious Runoff Depth=3.30"

Tc=10.0 min CN=97.5 Runoff=9.21 cfs 36,383 cf

Subcatchment 3S: Ex. Area #3 Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=3.36"

Tc=5.0 min CN=98.0 Runoff=3.13 cfs 10,683 cf

Subcatchment 4S: Ex. Area #4 Runoff Area=12,053 sf 0.54% Impervious Runoff Depth=1.72"

Flow Length=119' Tc=13.7 min CN=80.1 Runoff=0.43 cfs 1,723 cf

Pond 5P: Ex. SDMH #1 / POC A Peak Elev=15.65' Storage=76 cf Inflow=11.76 cfs 47,066 cf

Primary=11.43 cfs 47,066 cf Secondary=0.00 cfs 0 cf Outflow=11.43 cfs 47,066 cf

Pond 6P: Ex. CB Peak Elev=12.76' Inflow=0.43 cfs 1,723 cf

12.0" Round Culvert n=0.013 L=98.0' S=0.0061 '/' Outflow=0.43 cfs 1,723 cf

Pond 7P: Ex. SDMH #6 / POC C Peak Elev=12.05' Inflow=0.43 cfs 1,723 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=0.43 cfs 1,723 cf

Pond 18P: Ex. SDMH#2 / POC B Peak Elev=15.11' Inflow=11.91 cfs 48,695 cf

Primary=11.91 cfs 48,695 cf Secondary=0.00 cfs 0 cf Tertiary=0.00 cfs 0 cf Outflow=11.91 cfs 48,695 cf

Pond 19P: Ex. SDMH #3 Peak Elev=12.65' Inflow=11.91 cfs 48,695 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=11.91 cfs 48,695 cf

Pond 21P: Ex. SDMH #4 Peak Elev=10.26' Inflow=11.91 cfs 48,695 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=11.91 cfs 48,695 cf

Pond 22P: Ex. SDMH #5 Peak Elev=9.43' Inflow=11.91 cfs 48,695 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=11.91 cfs 48,695 cf

Link 24L: Bedford Street Garage Inflow=0.00 cfs 0 cf

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Time span=0.00-36.00 hrs. dt=0.04 hrs. 901 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=7,923 sf 51.43% Impervious Runoff Depth=3.43" Subcatchment 1S: Ex. Area #1

Flow Length=181' Tc=5.8 min CN=89.3 Runoff=0.71 cfs 2,265 cf

Runoff Area=132,315 sf 97.01% Impervious Runoff Depth=4.32" Subcatchment 2S: Ex. Area #2

Tc=10.0 min CN=97.5 Runoff=11.90 cfs 47,589 cf

Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=4.37" Subcatchment 3S: Ex. Area #3

Tc=5.0 min CN=98.0 Runoff=4.03 cfs 13,922 cf

Runoff Area=12.053 sf 0.54% Impervious Runoff Depth=2.56" Subcatchment 4S: Ex. Area #4

Flow Length=119' Tc=13.7 min CN=80.1 Runoff=0.65 cfs 2,576 cf

Peak Elev=16.27' Storage=1,930 cf Inflow=15.19 cfs 61,511 cf Pond 5P: Ex. SDMH #1 / POC A

Primary=18.90 cfs 61,709 cf Secondary=0.00 cfs 0 cf Outflow=18.90 cfs 61,709 cf

Peak Elev=12.85' Inflow=0.65 cfs 2.576 cf Pond 6P: Ex. CB

12.0" Round Culvert n=0.013 L=98.0' S=0.0061 '/' Outflow=0.65 cfs 2,576 cf

Peak Elev=12.13' Inflow=0.65 cfs 2,576 cf Pond 7P: Ex. SDMH #6 / POC C

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=0.65 cfs 2,576 cf

Peak Elev=16.32' Inflow=19.21 cfs 63,974 cf Pond 18P: Ex. SDMH#2 / POC B

Primary=15.15 cfs 61,911 cf Secondary=4.06 cfs 2,063 cf Tertiary=0.00 cfs 0 cf Outflow=19.21 cfs 63,974 cf

Peak Elev=13.61' Inflow=19.21 cfs 63,974 cf Pond 19P: Ex. SDMH #3

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=19.21 cfs 63,974 cf

Peak Elev=11.12' Inflow=19.21 cfs 63,974 cf Pond 21P: Ex. SDMH #4

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=19.21 cfs 63,974 cf

Peak Elev=10.41' Inflow=19.21 cfs 63,974 cf Pond 22P: Ex. SDMH #5

24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=19.21 cfs 63,974 cf

Inflow=0.00 cfs 0 cf Link 24L: Bedford Street Garage

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Ex. Area #1 Runoff Area=7,923 sf 51.43% Impervious Runoff Depth=4.24"

Flow Length=181' Tc=5.8 min CN=89.3 Runoff=0.87 cfs 2,797 cf

Subcatchment 2S: Ex. Area #2 Runoff Area=132,315 sf 97.01% Impervious Runoff Depth=5.15"

Tc=10.0 min CN=97.5 Runoff=14.11 cfs 56,829 cf

Subcatchment 3S: Ex. Area #3 Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=5.21"

Tc=5.0 min CN=98.0 Runoff=4.78 cfs 16,592 cf

Subcatchment 4S: Ex. Area #4 Runoff Area=12,053 sf 0.54% Impervious Runoff Depth=3.30"

Flow Length=119' Tc=13.7 min CN=80.1 Runoff=0.83 cfs 3,313 cf

Pond 5P: Ex. SDMH #1 / POC A Peak Elev=16.42' Storage=3,436 cf Inflow=18.01 cfs 73,420 cf

Primary=19.76 cfs 73,804 cf Secondary=0.00 cfs 0 cf Outflow=19.76 cfs 73,804 cf

Pond 6P: Ex. CB Peak Elev=12.92' Inflow=0.83 cfs 3,313 cf

12.0" Round Culvert n=0.013 L=98.0' S=0.0061 '/' Outflow=0.83 cfs 3,313 cf

Pond 7P: Ex. SDMH #6 / POC C Peak Elev=12.19' Inflow=0.83 cfs 3,313 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=0.83 cfs 3,313 cf

Pond 18P; Ex. SDMH#2 / POC B Peak Elev=16.36' Inflow=20.20 cfs 76,601 cf

Primary=15.25 cfs 72,897 cf Secondary=4.96 cfs 3,704 cf Tertiary=0.00 cfs 0 cf Outflow=20.20 cfs 76,601 cf

Pond 19P: Ex. SDMH #3 Peak Elev=14.02' Inflow=20.20 cfs 76,601 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=20.20 cfs 76,601 cf

Pond 21P: Ex. SDMH #4 Peak Elev=11.26' Inflow=20.20 cfs 76,601 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=20.20 cfs 76,601 cf

Pond 22P: Ex. SDMH #5 Peak Elev=10.58' Inflow=20.20 cfs 76,601 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173'/' Outflow=20.20 cfs 76,601 cf

Link 24L: Bedford Street Garage

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Summary for Subcatchment 1S: Ex. Area #1

Runoff = 1.09 cfs @ 12.08 hrs, Volume= 3,547 cf, Depth= 5.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

	Α	rea (sf)	CN	Description	nn			
_		3,848	80.0	>75% Grass cover, Good, HSG D				
		4,075	98.0	Paved parking, HSG D				
		7,923	89.3	Weighted Average				
		3,848		48.57% Pervious Area				
		4,075		51.43% Impervious Area				
		., - : -						
	Тс	Length	Slope	Velocity	Capacity	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	4.8	48	0.0270	0.17		Sheet Flow, Grass		
	7.0	40	0.0210	0.17		Grass: Short n= 0.150 P2= 3.30"		
	0.1	10	0.0400	1.16		Sheet Flow, Paved		
	0.1	10	0.0400	1.10		Smooth surfaces n= 0.011 P2= 3.30"		
	0.0	50	0.0070	4.70				
	0.6	58	0.0070	1.70		Shallow Concentrated Flow, Gutter		
						Paved Kv= 20.3 fps		
	0.3	65	0.0060	3.51	2.76	Pipe Channel, 12" RCP		
						12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'		
						n= 0.013		
	5.8	181	Total					

Summary for Subcatchment 2S: Ex. Area #2

Runoff = 17.18 cfs @ 12.13 hrs, Volume= 69,707 cf, Depth= 6.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

<i>F</i>	Area (sf)	CN	Description	n		
2	3,953	80.0	>75% Gra	ass cover, (Good, HSG D	
	128,362	98.0	Paved par	Paved parking, HSG D		
	132,315	97.5	Weighted	Average		
	3,953		2.99% Pe	rvious Area	a	
	128,362		97.01% In	npervious A	Area	
Tc (min)	9	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
10.0		17	XX		Direct Entry,	

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Summary for Subcatchment 3S: Ex. Area #3

Runoff = 5.81 cfs @ 12.07 hrs, Volume=

20,312 cf, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

-	Α	rea (sf)	CN	Description	n	
		38,197	98.0	Roofs, HS	SG D	
		38,197		100.00%	Impervious	Area
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	5.0					Direct Entry.

Summary for Subcatchment 4S: Ex. Area #4

Runoff = 1.09 cfs @ 12.19 hrs, Volume=

4,375 cf, Depth= 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

	A	rea (sf)	CN	Description			
-		65	98.0	Paved parking, HSG D			
		11,988	80.0	>75% Grass cover, Good, HSG D			
- 5		12,053	80.1	Weighted	Average		
		11,988		99.46% P	ervious Are	ea	
		65		0.54% lm	pervious A	rea	
	_		0.1			5 3.6	
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	4.4	24	0.0083	0.09		Sheet Flow, Grass	
						Grass: Short n= 0.150	P2= 3.30"
	9.3	95	0.0200	0.17		Sheet Flow, Grass	
						Grass: Short n= 0.150	P2= 3.30"
	13.7	119	Total				

Summary for Pond 5P: Ex. SDMH #1 / POC A

Inflow Area =	170,512 sf, 97.68% Impervious,	Inflow Depth = 6.34" for 25-Year event
Inflow =	21.93 cfs @ 12.12 hrs, Volume=	90,019 cf
Outflow =	21.31 cfs @ 12.24 hrs, Volume=	90,293 cf, Atten= 3%, Lag= 7.5 min
Primary =	20.21 cfs @ 12.16 hrs, Volume=	89,627 cf
Secondary =	1.30 cfs @ 12.25 hrs, Volume=	666 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Peak Elev= 16.55' @ 12.25 hrs Surf.Area= 16,021 sf Storage= 5,357 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 1.5 min (750.5 - 749.0)

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Volume	Invert	Avail.Storage	Storage Description
#1	13.20'	46 cf	4.00'D x 3.70'H Mahole
#2	15.40'	10,128 cf	Trench Drain / Double CB (Irregular) Listed below (Recalc)
-			

10,175 cf	Total	Availa	able	Storag	jе

Elevation (feet)	Surf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
15.40	8	12.0	0	0	8
15.50	72	36.0	3	3	100
15.60	378	130.0	20	24	1,341
15.70	620	166.0	49	73	2,190
15.80	986	212.0	80	153	3,573
15.90	1,843	326.0	139	292	8,454
16.00	2,941	396.0	237	529	12,476
16.10	4,386	455.0	364	893	16,472
16.20	6,169	545.0	525	1,418	23,634
16.30	8,980	684.0	753	2,172	37,228
16.40	11,481	725.0	1,020	3,192	41,826
16.50	14,507	781.0	1,296	4,488	48,538
16.60	17,337	847.0	1,590	6,079	57,089
16.70	20,473	796.0	1,888	7,967	63,757
16.80	22,778	818.0	2,162	10,128	66,584

Device	Routing	Invert	Outlet Devices
#1	Primary	13.20'	24.0" Round RCP_Round 24"
	•		L= 103.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 13.20' / 12.70' S= 0.0049 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 3.14 sf
#2	Secondary	16.45'	Asymmetrical Weir, C= 3.27
			Offset (feet) 0.00 9.10 17.80 26.65 36.06 43.97 53.90 62.08
			71.77
			Height (feet) 0.69 0.26 0.14 0.10 0.00 0.02 0.24 0.41 0.69

Primary OutFlow Max=6.50 cfs @ 12.16 hrs HW=16.49' TW=16.30' (Dynamic Tailwater) 1=RCP Round 24" (Outlet Controls 6.50 cfs @ 2.07 fps)

Secondary OutFlow Max=1.25 cfs @ 12.25 hrs HW=16.55' TW=0.00' (Dynamic Tailwater) 2=Asymmetrical Weir (Weir Controls 1.25 cfs @ 0.60 fps)

Summary for Pond 6P: Ex. CB

Inflow Are	a =	12,053 sf,	0.54% Impervious,	Inflow Depth = 4.36"	for 25-Year event
Inflow	=	1.09 cfs @	12.19 hrs, Volume=	4,375 cf	
Outflow	=	1.09 cfs @	12.19 hrs, Volume=	4,375 cf, Atte	n= 0%, Lag= 0.0 min
Primary	=	1.09 cfs @	12.19 hrs. Volume=	4.375 cf	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 13.01' @ 12.19 hrs

Flood Elev= 15.10'

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Device	Routing	Invert	Outlet Devices
#1	Primary	12.40'	12.0" Round RCP_Round 12"
			L= 98.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 12.40' / 11.80' S= 0.0061 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 0.79 sf

Primary OutFlow Max=1.08 cfs @ 12.19 hrs HW=13.00' TW=12.26' (Dynamic Tailwater) 1=RCP_Round 12" (Outlet Controls 1.08 cfs @ 3.14 fps)

Summary for Pond 7P: Ex. SDMH #6 / POC C

Inflow Area	=	12,053 sf,	0.54% lm	pervious,	Inflow Depth =	4.36"	for 25-Year event
Inflow =	=	1.09 cfs @	12.19 hrs, '	Volume=	4,375 cf	f	
Outflow =	•	1.09 cfs @	12.19 hrs,	Volume=	4,375 cf	f, Atter	n= 0%, Lag= 0.0 min
Primary =	•	1.09 cfs @	12.19 hrs,	Volume=	4,375 cf	f	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Peak Elev= 12.26' @ 12.19 hrs

Flood Elev= 17.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	11.70'	18.0" Round 18" RCP
	_		L= 100.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 11.70' / 11.30' S= 0.0040 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.77 sf

Primary OutFlow Max=1.09 cfs @ 12.19 hrs HW=12.26' (Free Discharge) 1=18" RCP (Barrel Controls 1.09 cfs @ 2.69 fps)

Summary for Pond 18P: Ex. SDMH#2 / POC B

Inflow Area =	178,435 sf, 95.63% Impervious,	Inflow Depth = 6.27" for 25-Year event
Inflow =	20.98 cfs @ 12.16 hrs, Volume=	93,174 cf
Outflow =	20.98 cfs @ 12.16 hrs, Volume=	93,174 cf, Atten= 0%, Lag= 0.0 min
Primary =	15.32 cfs @ 12.16 hrs, Volume=	88,200 cf
Secondary =	5.67 cfs @ 12.16 hrs, Volume=	4,973 cf
Tertiary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 16.40' @ 12.16 hrs

Flood Elev= 16.70'

Device	Routing	Invert	Outlet Devices	
#1	Primary	12.40'	18.0" Round RCP_Round 18"	
			L= 30.0' RCP, square edge headw	/all, Ke= 0.500
			Inlet / Outlet Invert= 12.40' / 11.20'	S= 0.0400 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.77 sf	
#2	Secondary	16.10'	24.0" x 48.0" Horiz. Orifice/Grate	C= 0.600
	•		Limited to weir flow at low heads	
#3	Tertiary	16.40'	24.0" x 48.0" Horiz. Orifice/Grate Limited to weir flow at low heads	C= 0.600
			Limited to weir flow at low neads	

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Primary OutFlow Max=12.61 cfs @ 12.16 hrs HW=16.27' TW=14.08' (Dynamic Tailwater) 1=RCP Round 18" (Inlet Controls 12.61 cfs @ 7.14 fps)

Secondary OutFlow Max=5.67 cfs @ 12.16 hrs HW=16.38' TW=14.19' (Dynamic Tailwater) 2=Orifice/Grate (Weir Controls 5.67 cfs @ 1.72 fps)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=12.40' TW=11.00' (Dynamic Tailwater) 3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 19P: Ex. SDMH #3

Inflow Area = 178.435 sf. 95.63% Impervious, Inflow Depth = 6.27" for 25-Year event

Inflow = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf

Outflow = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf, Atten= 0%, Lag= 0.0 min

Primary = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 14.41' @ 12.24 hrs

Flood Elev= 16.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	11.00'	24.0" Round RCP_Round 24"
	•		L= 303.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 11.00' / 8.40' S= 0.0086 '/' Cc= 0.900
			n= 0.013. Flow Area= 3.14 sf

Primary OutFlow Max=18.25 cfs @ 12.16 hrs HW=14.12' TW=11.35' (Dynamic Tailwater) 1=RCP Round 24" (Outlet Controls 18.25 cfs @ 5.81 fps)

Summary for Pond 21P: Ex. SDMH #4

Inflow Area = 178,435 sf, 95.63% Impervious, Inflow Depth = 6.27" for 25-Year event

Inflow = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf

Outflow = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf, Atten= 0%, Lag= 0.0 min

Primary = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 11.38' @ 12.17 hrs

Flood Elev= 16.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	8.40'	24.0" Round RCP_Round 24"
	•		L= 62.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 8.40' / 7.80' S= 0.0097 '/' Cc= 0.900
			n= 0.013, Flow Area= 3.14 sf

Primary OutFlow Max=12.71 cfs @ 12.16 hrs HW=11.35' TW=10.64' (Dynamic Tailwater) 1=RCP_Round 24" (Inlet Controls 12.71 cfs @ 4.05 fps)

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Summary for Pond 22P: Ex. SDMH #5

Inflow Area = 178,435 sf, 95.63% Impervious, Inflow Depth = 6.27" for 25-Year event

Inflow = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf

Outflow = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf, Atten= 0%, Lag= 0.0 min

Primary = 20.98 cfs @ 12.16 hrs, Volume= 93,174 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 10.72' @ 12.16 hrs

Flood Elev= 16.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	7.80'	24.0" Round RCP_Round 24"
	-		L= 78.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.80' / 6.45' S= 0.0173 '/' Cc= 0.900
			n= 0.013, Flow Area= 3.14 sf

Primary OutFlow Max=20.54 cfs @ 12.16 hrs HW=10.64' (Free Discharge) 1=RCP_Round 24" (Inlet Controls 20.54 cfs @ 6.54 fps)

Summary for Link 24L: Bedford Street Garage

Inflow = 1.30 cfs @ 12.25 hrs, Volume= 666 cf

Primary = 1.30 cfs @ 12.25 hrs, Volume= 666 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Ex. Area #1 Runoff Area=7,923 sf 51.43% Impervious Runoff Depth=6.21"

Flow Length=181' Tc=5.8 min CN=89.3 Runoff=1.25 cfs 4,102 cf

Subcatchment 2S: Ex. Area #2 Runoff Area=132,315 sf 97.01% Impervious Runoff Depth=7.18"

Tc=10.0 min CN=97.5 Runoff=19.43 cfs 79,178 cf

Subcatchment 3S: Ex. Area #3 Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=7.24"

Tc=5.0 min CN=98.0 Runoff=6.57 cfs 23,047 cf

Subcatchment 4S: Ex. Area #4 Runoff Area=12,053 sf 0.54% Impervious Runoff Depth=5.15"

Flow Length=119' Tc=13.7 min CN=80.1 Runoff=1.29 cfs 5,173 cf

Pond 5P: Ex. SDMH #1 / POC A Peak Elev=16.62' Storage=6,493 cf Inflow=24.80 cfs 102,225 cf

Primary=20.63 cfs 99,894 cf Secondary=3.87 cfs 2,551 cf Outflow=23.42 cfs 102,445 cf

Pond 6P: Ex. CB Peak Elev=13.07' Inflow=1.29 cfs 5,173 cf

12.0" Round Culvert n=0.013 L=98.0' S=0.0061 '/' Outflow=1.29 cfs 5,173 cf

Pond 7P: Ex. SDMH #6 / POC C Peak Elev=12.31' Inflow=1.29 cfs 5,173 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=1.29 cfs 5,173 cf

Pond 18P: Ex. SDMH#2 / POC B Peak Elev=16.42' Inflow=21.26 cfs 103,996 cf

Primary=15.30 cfs 98,824 cf Secondary=5.96 cfs 5,172 cf Tertiary=0.00 cfs 0 cf Outflow=21.26 cfs 103,996 cf

Pond 19P: Ex. SDMH #3 Peak Elev=14.50' Inflow=21.26 cfs 103,996 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=21.26 cfs 103,996 cf

Pond 21P: Ex. SDMH #4 Peak Elev=11.46' Inflow=21.26 cfs 103,996 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=21.26 cfs 103,996 cf

Pond 22P: Ex. SDMH #5 Peak Elev=10.77' Inflow=21.26 cfs 103,996 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173'/' Outflow=21.26 cfs 103,996 cf

Link 24L: Bedford Street Garage Inflow=3.87 cfs 2,551 cf Primary=3.87 cfs 2,551 cf

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Ex. Area #1 Runoff Area=7,923 sf 51.43% Impervious Runoff Depth=7.13"

Flow Length=181' Tc=5.8 min CN=89.3 Runoff=1.42 cfs 4,705 cf

Subcatchment 2S: Ex. Area #2 Runoff Area=132,315 sf 97.01% Impervious Runoff Depth=8.11"

Tc=10.0 min CN=97.5 Runoff=21.87 cfs 89,422 cf

Subcatchment 3S: Ex. Area #3 Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=8.17"

Tc=5.0 min CN=98.0 Runoff=7.39 cfs 26,006 cf

Subcatchment 4S: Ex. Area #4 Runoff Area=12,053 sf 0.54% Impervious Runoff Depth=6.02"

Flow Length=119' Tc=13.7 min CN=80.1 Runoff=1.50 cfs 6,049 cf

Pond 5P: Ex. SDMH #1 / POC A Peak Elev=16.69' Storage=7,735 cf Inflow=27.91 cfs 115,428 cf

Primary=20.48 cfs 110,140 cf Secondary=7.99 cfs 5,518 cf Outflow=25.31 cfs 115,658 cf

Pond 6P: Ex. CB Peak Elev=13.13' Inflow=1.50 cfs 6,049 cf

12.0" Round Culvert n=0.013 L=98.0' S=0.0061 '/' Outflow=1.50 cfs 6,049 cf

Pond 7P: Ex. SDMH #6 / POC C Peak Elev=12.36' Inflow=1.50 cfs 6,049 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=1.50 cfs 6,049 cf

Pond 18P: Ex. SDMH#2 / POC B Peak Elev=16.43' Inflow=21.32 cfs 114,845 cf

Primary=15.31 cfs 109,536 cf Secondary=6.01 cfs 5,308 cf Tertiary=0.00 cfs 0 cf Outflow=21.32 cfs 114,845 cf

Pond 19P; Ex. SDMH #3 Peak Elev=14.53' Inflow=21.32 cfs 114,845 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=21.32 cfs 114,845 cf

Pond 21P: Ex. SDMH #4 Peak Elev=11.49' Inflow=21.32 cfs 114,845 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=21.32 cfs 114,845 cf

Pond 22P: Ex. SDMH #5 Peak Elev=10.79' Inflow=21.32 cfs 114,845 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=21.32 cfs 114,845 cf

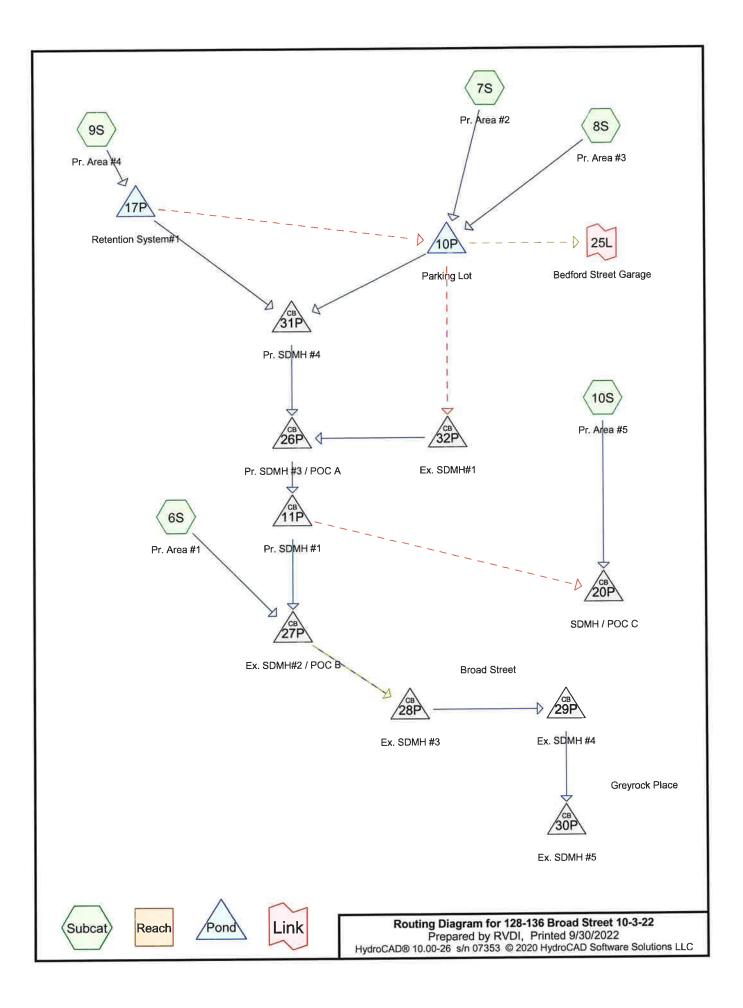
Link 24L: Bedford Street Garage Inflow=7.99 cfs 5,518 cf

Primary=7.99 cfs 5,518 cf

Appendix L: HydroCAD Analysis—Proposed Conditions

ENGINEERING, PC =RS • ENGINEERS • SURVEYORS

D'



Runoff Area=2,714 sf 100.00% Impervious Runoff Depth=2.74"

Subcatchment 6S: Pr. Area #1

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Tc=5.0 min CN=98.0 Runoff=0.18 cfs 619 cf

Subcatchment 7S: Pr. Area #2

Runoff Area=115,349 sf 100.00% Impervious Runoff Depth=2.74"
Tc=10.0 min CN=98.0 Runoff=6.65 cfs 26,323 cf

Subcatchment 8S: Pr. Area #3

Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=2.74"
Tc=5.0 min CN=98.0 Runoff=2.58 cfs 8,717 cf

Subcatchment 9S: Pr. Area #4

Runoff Area=33,888 sf 100.00% Impervious Runoff Depth=2.74"
Tc=5.0 min CN=98.0 Runoff=2.28 cfs 7,733 cf

Subcatchment 10S: Pr. Area #5

Runoff Area=322 sf 100.00% Impervious Runoff Depth=2.74"
Tc=5.0 min CN=98.0 Runoff=0.02 cfs 73 cf

Peak Elev=14.81' Storage=23 cf Inflow=8.77 cfs 35,039 cf

Primary=5.45 cfs 7,900 cf Secondary=3.34 cfs 27,138 cf Tertiary=0.00 cfs 0 cf Outflow=8.76 cfs 35,038 cf

Pond 11P: Pr. SDMH #1

Peak Elev=13.79' Inflow=8.76 cfs 36,837 cf

Primary=8.74 cfs 36,831 cf Secondary=0.02 cfs 6 cf Outflow=8.76 cfs 36,837 cf

Pond 17P: Retention System#1 Peak Elev=13.64' Storage=6,125 cf Inflow=2.28 cfs 7,733 cf
Primary=0.10 cfs 1,798 cf Secondary=0.00 cfs 0 cf Outflow=0.10 cfs 1,798 cf

Pond 20P: SDMH / POC C

Peak Elev=11.81' Inflow=0.04 cfs 79 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=0.04 cfs 79 cf

Pond 26P: Pr. SDMH #3 / POC A Peak Elev=14.34' Inflow=8.76 cfs 36,837 cf 18.0" Round Culvert x 2.00 n=0.011 L=96.0' S=0.0052 '/' Outflow=8.76 cfs 36,837 cf

Pond 27P: Ex. SDMH#2 / POC B

Primary=8.90 cfs 37,450 cf

Secondary=0.00 cfs 0 cf

Tertiary=0.00 cfs 0 cf

Outflow=8.90 cfs 37,450 cf

Outflow=8.90 cfs 37,450 cf

Pond 28P: Ex. SDMH #3

Peak Elev=12.35' Inflow=8.90 cfs 37,450 cf 24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=8.90 cfs 37,450 cf

Pond 29P: Ex. SDMH #4 Peak Elev=9.91' Inflow=8.90 cfs 37,450 cf 24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=8.90 cfs 37,450 cf

Pond 30P: Ex. SDMH #5

Peak Elev=9.15' Inflow=8.90 cfs 37,450 cf
24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=8.90 cfs 37,450 cf

Pond 31P: Pr. SDMH #4 Peak Elev=14.48' Inflow=5.45 cfs 9,698 cf 18.0" Round Culvert x 2.00 n=0.011 L=29.0' S=0.0052 '/' Outflow=5.45 cfs 9,698 cf

Pond 32P: Ex. SDMH#1

Peak Elev=14.45' Inflow=3.34 cfs 27,138 cf
24.0" Round Culvert n=0.011 L=18.0' S=0.0056 '/' Outflow=3.34 cfs 27,138 cf

Type III 24-hr 1-Year Rainfall=2.97" Printed 9/30/2022

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Link 25L: Bedford Street Garage

Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=2,714 sf 100.00% Impervious Runoff Depth=3.36" Subcatchment 6S: Pr. Area #1

Tc=5.0 min CN=98.0 Runoff=0.22 cfs 759 cf

Runoff Area=115,349 sf 100.00% Impervious Runoff Depth=3.36" Subcatchment 7S: Pr. Area #2

Tc=10.0 min CN=98.0 Runoff=8.07 cfs 32,261 cf

Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=3.36" Subcatchment 8S: Pr. Area #3

Tc=5.0 min CN=98.0 Runoff=3.13 cfs 10,683 cf

Runoff Area=33,888 sf 100.00% Impervious Runoff Depth=3.36" Subcatchment 9S: Pr. Area #4

Tc=5.0 min CN=98.0 Runoff=2.77 cfs 9,478 cf

Runoff Area=322 sf 100.00% Impervious Runoff Depth=3.36" Subcatchment 10S: Pr. Area #5

Tc=5.0 min CN=98.0 Runoff=0.03 cfs 90 cf

Peak Elev=15.01' Storage=26 cf Inflow=10.65 cfs 42,944 cf Pond 10P: Parking Lot

Primary=7.07 cfs 10,806 cf Secondary=3.62 cfs 32,137 cf Tertiary=0.00 cfs 0 cf Outflow=10.64 cfs 42,943 cf

Peak Elev=13.94' Inflow=10.64 cfs 46,486 cf Pond 11P: Pr. SDMH #1

Primary=10.48 cfs 46,422 cf Secondary=0.16 cfs 64 cf Outflow=10.64 cfs 46,486 cf

Peak Elev=13.86' Storage=6,461 cf Inflow=2.77 cfs 9,478 cf Pond 17P: Retention System#1

Primary=0.42 cfs 3,543 cf Secondary=0.00 cfs 0 cf Outflow=0.42 cfs 3,543 cf

Peak Elev=11.93' Inflow=0.18 cfs 154 cf Pond 20P: SDMH / POC C

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=0.18 cfs 154 cf

Peak Elev=14.52' Inflow=10.64 cfs 46,486 cf Pond 26P: Pr. SDMH #3 / POC A

18.0" Round Culvert x 2.00 n=0.011 L=96.0' S=0.0052 '/' Outflow=10.64 cfs 46,486 cf

Peak Elev=13.55' Inflow=10.67 cfs 47,181 cf Pond 27P: Ex. SDMH#2 / POC B

Primary=10.67 cfs 47,181 cf Secondary=0.00 cfs 0 cf Tertiary=0.00 cfs 0 cf Outflow=10.67 cfs 47,181 cf

Peak Elev=12.52' Inflow=10.67 cfs 47,181 cf Pond 28P: Ex. SDMH #3

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=10.67 cfs 47,181 cf

Peak Elev=10.11' Inflow=10.67 cfs 47,181 cf Pond 29P: Ex. SDMH #4

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=10.67 cfs 47.181 cf

Peak Elev=9.31' Inflow=10.67 cfs 47,181 cf Pond 30P: Ex. SDMH #5

24.0" Round Culvert n=0.013 L=78.0' S=0.0173'/' Outflow=10.67 cfs 47,181 cf

Peak Elev=14.68' Inflow=7.07 cfs 14,349 cf Pond 31P: Pr. SDMH #4

18.0" Round Culvert x 2.00 n=0.011 L=29.0' S=0.0052 '/' Outflow=7.07 cfs 14,349 cf

Peak Elev=14.61' Inflow=3.62 cfs 32,137 cf Pond 32P: Ex. SDMH#1

24.0" Round Culvert n=0.011 L=18.0' S=0.0056 '/' Outflow=3.62 cfs 32.137 cf

Type III 24-hr 2-Year Rainfall=3.59" Printed 9/30/2022

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Link 25L: Bedford Street Garage

Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Runoff Area=2,714 sf 100.00% Impervious Runoff Depth=4.37" Subcatchment 6S: Pr. Area #1

Tc=5.0 min CN=98.0 Runoff=0.29 cfs 989 cf

Runoff Area=115,349 sf 100.00% Impervious Runoff Depth=4.37" Subcatchment 7S: Pr. Area #2

Tc=10.0 min CN=98.0 Runoff=10.41 cfs 42,043 cf

Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=4.37" Subcatchment 8S: Pr. Area #3

Tc=5.0 min CN=98.0 Runoff=4.03 cfs 13,922 cf

Runoff Area=33.888 sf 100.00% Impervious Runoff Depth=4.37" Subcatchment 9S: Pr. Area #4

Tc=5.0 min CN=98.0 Runoff=3.58 cfs 12,352 cf

Runoff Area=322 sf 100.00% Impervious Runoff Depth=4.37" Subcatchment 10S: Pr. Area #5

Tc=5.0 min CN=98.0 Runoff=0.03 cfs 117 cf

Peak Elev=15.39' Storage=32 cf Inflow=13.73 cfs 55,965 cf Pond 10P: Parking Lot

Primary=9.78 cfs 16,144 cf Secondary=3.99 cfs 39,821 cf Tertiary=0.00 cfs 0 cf Outflow=13.72 cfs 55,965 cf

Peak Elev=14.31' Inflow=13.72 cfs 62,381 cf Pond 11P: Pr. SDMH #1

Primary=12.96 cfs 62,015 cf Secondary=0.80 cfs 366 cf Outflow=13.72 cfs 62,381 cf

Peak Elev=14.65' Storage=7,621 cf inflow=3.58 cfs 12,352 cf Pond 17P: Retention System#1

Primary=2.11 cfs 6,417 cf Secondary=0.00 cfs 0 cf Outflow=2.11 cfs 6,417 cf

Peak Elev=12.18' Inflow=0.82 cfs 484 cf Pond 20P: SDMH / POC C

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=0.82 cfs 484 cf

Peak Elev=14.87' Inflow=13.72 cfs 62,381 cf Pond 26P: Pr. SDMH #3 / POC A

18.0" Round Culvert x 2.00 n=0.011 L=96.0' S=0.0052 '/' Outflow=13.72 cfs 62,381 cf

Peak Elev=13.75' Inflow=13.22 cfs 63,004 cf Pond 27P: Ex. SDMH#2 / POC B

Primary=13.22 cfs 63,004 cf Secondary=0.00 cfs 0 cf Tertiary=0.00 cfs 0 cf Outflow=13.22 cfs 63,004 cf

Peak Elev=12.78' Inflow=13.22 cfs 63,004 cf Pond 28P: Ex. SDMH #3

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=13.22 cfs 63,004 cf

Peak Elev=10.41' Inflow=13.22 cfs 63,004 cf Pond 29P: Ex. SDMH #4

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=13.22 cfs 63,004 cf

Peak Elev=9.56' Inflow=13.22 cfs 63,004 cf Pond 30P: Ex. SDMH #5

24.0" Round Culvert n=0.013 L=78.0' S=0.0173'/' Outflow=13.22 cfs 63,004 cf

Peak Elev=15.09' Inflow=9.78 cfs 22.560 cf Pond 31P: Pr. SDMH #4

18.0" Round Culvert x 2.00 n=0.011 L=29.0' S=0.0052 '/' Outflow=9.78 cfs 22,560 cf

Peak Elev=14.93' Inflow=3.99 cfs 39,821 cf Pond 32P: Ex. SDMH#1

24.0" Round Culvert n=0.011 L=18.0' S=0.0056 '/' Outflow=3.99 cfs 39,821 cf

Type III 24-hr 5-Year Rainfall=4.61" Printed 9/30/2022

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Link 25L: Bedford Street Garage

Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 6S: Pr. Area #1 Runoff Area=2,714 sf 100.00% Impervious Runoff Depth=5.21"

Tc=5.0 min CN=98.0 Runoff=0.34 cfs 1,179 cf

Subcatchment 7S: Pr. Area #2 Runoff Area=115,349 sf 100.00% Impervious Runoff Depth=5.21"

Tc=10.0 min CN=98.0 Runoff=12.33 cfs 50,105 cf

Subcatchment 8S: Pr. Area #3 Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=5.21"

Tc=5.0 min CN=98.0 Runoff=4.78 cfs 16,592 cf

Subcatchment 9S: Pr. Area #4 Runoff Area=33,888 sf 100.00% Impervious Runoff Depth=5.21"

Tc=5.0 min CN=98.0 Runoff=4.24 cfs 14,720 cf

Subcatchment 10S: Pr. Area #5 Runoff Area=322 sf 100.00% Impervious Runoff Depth=5.21"

Tc=5.0 min CN=98.0 Runoff=0.04 cfs 140 cf

Pond 10P: Parking Lot Peak Elev=16.14' Storage=1,078 cf Inflow=16.26 cfs 66,697 cf

Primary=11.71 cfs 21,113 cf Secondary=4.58 cfs 45,583 cf Tertiary=0.00 cfs 0 cf Outflow=16.08 cfs 66,696 cf

Pond 11P: Pr. SDMH #1 Peak Elev=14.95' Inflow=18.88 cfs 75,481 cf

Primary=17.62 cfs 74,374 cf Secondary=1.25 cfs 1,107 cf Outflow=18.88 cfs 75,481 cf

Pond 17P: Retention System#1 Peak Elev=16.06' Storage=7,813 cf Inflow=4.24 cfs 14,720 cf

Primary=4.22 cfs 8,785 cf Secondary=0.00 cfs 0 cf Outflow=4.22 cfs 8,785 cf

Pond 20P: SDMH / POC C Peak Elev=12.31' Inflow=1.28 cfs 1,247 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=1.28 cfs 1,247 cf

Pond 26P: Pr. SDMH #3 / POC A Peak Elev=15.82' Inflow=18.88 cfs 75,481 cf

18.0" Round Culvert x 2.00 n=0.011 L=96.0' S=0.0052'/' Outflow=18.88 cfs 75,481 cf

Pond 27P: Ex. SDMH#2 / POC B Peak Elev=14.19' Inflow=17.86 cfs 75,553 cf

Primary=17.86 cfs 75,553 cf Secondary=0.00 cfs 0 cf Tertiary=0.00 cfs 0 cf Outflow=17.86 cfs 75,553 cf

Pond 28P: Ex. SDMH #3 Peak Elev=13.32' Inflow=17.86 cfs 75,553 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=17.86 cfs 75,553 cf

Pond 29P: Ex. SDMH #4 Peak Elev=11.10' Inflow=17.86 cfs 75,553 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=17.86 cfs 75,553 cf

Pond 30P: Ex. SDMH #5 Peak Elev=10.15' Inflow=17.86 cfs 75,553 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=17.86 cfs 75,553 cf

Pond 31P: Pr. SDMH #4 Peak Elev=16.03' Inflow=14.71 cfs 29,898 cf

18.0" Round Culvert x 2.00 n=0.011 L=29.0' S=0.0052 '/' Outflow=14.71 cfs 29,898 cf

Pond 32P: Ex. SDMH#1 Peak Elev=15.88' Inflow=4.58 cfs 45,583 cf

24.0" Round Culvert n=0.011 L=18.0' S=0.0056 '/' Outflow=4.58 cfs 45,583 cf

Type III 24-hr 10-Year Rainfall=5.45" Printed 9/30/2022

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Link 25L: Bedford Street Garage

Inflow=0.00 cfs 0 cf Primary=0.00 cfs 0 cf

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Summary for Subcatchment 6S: Pr. Area #1

Runoff = 0.41 cfs @ 12.07 hrs, Volume=

1,443 cf, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

A	rea (sf)	CN	Description	n	<u></u>			
	2,714	98.0	Paved parking, HSG D					
:	2,714		100.00%	mpervious	s Area			
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•			
5.0		= x:			Direct Entry,			

Summary for Subcatchment 7S: Pr. Area #2

Runoff = 15.00 cfs @ 12.13 hrs, Volume=

61,339 cf, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

	Α	rea (sf)	CN	Description	n		
<u> </u>	1	15,349	98.0	Paved parking, HSG D			
0,=	1	15,349		100.00%	Impervious	s Area	
(r	Tc min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	10.0					Direct Entry,	

Summary for Subcatchment 8S: Pr. Area #3

Runoff = 5.81 cfs @ 12.07 hrs, Volume=

20,312 cf, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

A	rea (sf)	CN	Description	n		
	38,197	98.0	Roofs, HSG D			
	38,197		100.00%	Impervious	Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0					Direct Entry,	

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Summary for Subcatchment 9S: Pr. Area #4

Runoff = 5.15 cfs @ 12.07 hrs, Volume= 18,021 cf, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

A	rea (sf)	CN	Description	n			
	33,888	98.0	Roofs, HSG B				
-	33,888		100.00%	Impervious	s Area		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
5.0		**			Direct Entry,		

Summary for Subcatchment 10S: Pr. Area #5

Runoff = 0.05 cfs @ 12.07 hrs, Volume= 171 cf, Depth= 6.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Type III 24-hr 25-Year Rainfall=6.62"

Α	rea (sf)	CN	Description	n			
	322	98.0	Paved parking, HSG D				
	0	80.0	>75% Gra	ss cover, (Good, HSG D		
	322	98.0	Weighted	Average			
	322		100.00%	Impervious	s Area		
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•		
5.0		× 11.	***		Direct Entry,		

Summary for Pond 10P: Parking Lot

Inflow Area =	153,546 sf,100.00% Impervious,	Inflow Depth = 6.38" for 25-Year event
Inflow =	19.79 cfs @ 12.11 hrs, Volume=	81,651 cf
Outflow =	18.29 cfs @ 12.23 hrs, Volume=	81,650 cf, Atten= 8%, Lag= 6.8 min
Primary =	12.82 cfs @ 12.23 hrs, Volume=	27,690 cf
Secondary =	5.22 cfs @ 12.24 hrs, Volume=	53,778 cf
Tertiary =	0.73 cfs @ 12.21 hrs, Volume=	183 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Peak Elev= 16.53' @ 12.21 hrs Surf.Area= 13,955 sf Storage= 4,689 cf Flood Elev= 16.90' Surf.Area= 19,811 sf Storage= 9,197 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 1.0 min (747.3 - 746.3)

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Volume	Invert	t Avail.S	Storage	Storage Description	on	
#1	13.40	ı	37 cf	4.00'W x 4.00'L x		
#2	15.40	' 9	,160 cf	Trench Drain / Do	ouble CB (Irregula	r) Listed below (Recalc)
:(,197 cf	Total Available St		
			,		· ·	
Elevation	on S	urf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	<u>(sq-ft)</u>
15.4	Ю	8	12.0	0	0	8
15.5	50	72	36.0	3	3	100
15.6	60	378	130.0	20	24	1,341
15.7	' 0	620	166.0	49	73	2,190
15.8	30	986	212.0	80	153	3,573
15.9	90	1,843	326.0	139	292	8,454
16.0	00	2,886	393.0	235	527	12,288
16.1	10	4,188	448.0	352	878	15,969
16.2	20	5,792	544.0	497	1,375	23,547
16.3	30	8,436	679.0	707	2,083	36,686
16.4	10	10,645	710.0	952	3,034	40,113
16.5	50	13,336	740.0	1,197	4,231	43,576
16.6	80	15,337	779.0	1,432	5,663	48,291
16.7	' 0	17,423	794.0	1,637	7,300	50,170
16.8	30	19,795	822.0	1,860	9,160	53,771
Davisa	Davidaa	love	- Out	at Davisas		
Device	Routing	Inve		et Devices	DVC V 2.00	
#1	Primary	13.8		" Round Twin 18'		Ko- 0 500
			L= 1	17.0' CPP, square	e euge neauwaii,	.0047 '/' Cc= 0.900
						.0047 / CC= 0.900
40	0	. 40.4		.011, Flow Area= " W x 12.0" H Bo x		
#2	Secondary	/ 13.4		0.0' Box, headwa		s Ka= 0.500
			L- I	/ Outlet Inverte 12	11 W/3 Square euge	.0250 '/' Cc= 0.900
				.013, Flow Area=		.0200 / 00- 0.000
#3	Tertiary	16.4		mmetrical Weir, C		
#3	rentary	10.4	∪ Asy i	ot (foot) 0 00 0 10	- 3.21) 17 80 26 65 36	.06 43.97 53.90 62.08
			71.7		7 17.00 20.00 00	100 -10101 00100 0E100
					6 0.14 0.10 0.00	0.02 0.24 0.41 0.69

Primary OutFlow Max=8.86 cfs @ 12.23 hrs HW=16.51' TW=16.22' (Dynamic Tailwater) 1=Twin 18" PVC (Outlet Controls 8.86 cfs @ 2.51 fps)

Secondary OutFlow Max=4.05 cfs @ 12.24 hrs HW=16.50' TW=15.79' (Dynamic Tailwater) = Culvert (Inlet Controls 4.05 cfs @ 4.05 fps)

Tertiary OutFlow Max=0.65 cfs @ 12.21 hrs HW=16.52' TW=0.00' (Dynamic Tailwater) 3=Asymmetrical Weir (Weir Controls 0.65 cfs @ 0.52 fps)

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Summary for Pond 11P: Pr. SDMH #1

Inflow Area =	187,434 sf,100.00% Impervious,	Inflow Depth = 5.99" for 25-Year event
Inflow =	21.93 cfs @ 12.06 hrs, Volume=	93,553 cf
Outflow =	21.93 cfs @ 12.06 hrs, Volume=	93,553 cf, Atten= 0%, Lag= 0.0 min
Primary =	20.46 cfs @ 12.06 hrs, Volume=	91,451 cf
Secondary =	1.54 cfs @ 12.08 hrs, Volume=	2,102 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Peak Elev= 15.64' @ 12.08 hrs Flood Elev= 16.60'

Device	Routing	Invert	Outlet Devices
#1	Primary	12.55'	18.0" Round 24" PVC X 2.00
	•		L= 10.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 12.55' / 12.50' S= 0.0050 '/' Cc= 0.900
			n= 0.011, Flow Area= 1.77 sf
#2	Secondary	13.70'	8.0" Round Culvert
	•		L= 130.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 13.70' / 13.00' S= 0.0054 '/' Cc= 0.900
			n= 0.011, Flow Area= 0.35 sf

Primary OutFlow Max=13.70 cfs @ 12.06 hrs HW=15.30' TW=14.65' (Dynamic Tailwater) 1=24" PVC (Inlet Controls 13.70 cfs @ 3.88 fps)

Secondary OutFlow Max=1.52 cfs @ 12.08 hrs HW=15.59' TW=12.38' (Dynamic Tailwater) —2=Culvert (Barrel Controls 1.52 cfs @ 4.36 fps)

Summary for Pond 17P: Retention System#1

Inflow Area =	33,888 sf,100.00% Impervious,	Inflow Depth = 6.38" for 25-Year event
Inflow =	5.15 cfs @ 12.07 hrs, Volume=	18,021 cf
Outflow =	4.94 cfs @ 12.09 hrs, Volume=	12,085 cf, Atten= 4%, Lag= 0.9 min
Primary =	4.94 cfs @ 12.09 hrs, Volume=	12,085 cf
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs Peak Elev= 16.58' @ 12.14 hrs Surf.Area= 1,953 sf Storage= 7,820 cf

Plug-Flow detention time= 213.2 min calculated for 12,072 cf (67% of inflow) Center-of-Mass det. time= 113.7 min (856.5 - 742.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	9.20'	1,304 cf	10.00'W x 194.00'L x 6.17'H Field A
			11,963 cf Overall - 8,704 cf Embedded = 3,259 cf x 40.0% Voids
#2A	9.70'	6,471 cf	retain_it retain_it 5.0' x 24 Inside #1
			Inside= 84.0"W x 60.0"H => 36.41 sf x 8.00'L = 291.3 cf
			Outside= 96.0"W x 68.0"H => 45.33 sf x 8.00'L = 362.7 cf
			1 Rows adjusted for 519.5 cf perimeter wall
#3	13.00'	50 cf	4.00'D x 4.00'H Vertical Cone/Cylinder

7,825 cf Total Available Storage

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Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	13.50'	18.0" Round 18" PVC
			L= 12.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 13.50' / 13.30' S= 0.0167 '/' Cc= 0.900
			n= 0.011, Flow Area= 1.77 sf
#2	Secondary	16.60'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=0.00 cfs @ 12.09 hrs HW=15.89' TW=16.29' (Dynamic Tailwater) 1=18" PVC (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=9.20' TW=13.40' (Dynamic Tailwater) 2=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 20P: SDMH / POC C

Inflow Area = 322 sf,100.00% Impervious, Inflow Depth = 84.70" for 25-Year event

Inflow = 1.59 cfs @ 12.08 hrs, Volume= 2,273 cf

Outflow = 1.59 cfs @ 12.08 hrs, Volume= 2,273 cf, Atten= 0%, Lag= 0.0 min

Primary = 1.59 cfs @ 12.08 hrs, Volume= 2,273 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 12.38' @ 12.08 hrs

Flood Elev= 17.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	11.70'	18.0" Round 18" RCP L= 100.0' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 11.70' / 11.30' S= 0.0040 '/' Cc= 0.900 n= 0.013, Flow Area= 1.77 sf

Primary OutFlow Max=1.57 cfs @ 12.08 hrs HW=12.38' (Free Discharge) 1=18" RCP (Barrel Controls 1.57 cfs @ 2.97 fps)

Summary for Pond 26P: Pr. SDMH #3 / POC A

Inflow Area = 187,434 sf,100.00% Impervious, Inflow Depth = 5.99" for 25-Year event

Inflow = 21.93 cfs @ 12.06 hrs, Volume= 93,553 cf

Outflow = 21.93 cfs @ 12.06 hrs, Volume= 93,553 cf, Atten= 0%, Lag= 0.0 min

Primary = 21.93 cfs @ 12.06 hrs, Volume= 93,553 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 16.36' @ 12.09 hrs

Flood Elev= 17.00'

Device	Routing	Invert	Outlet Devices	
#1	Primary	13.10'	18.0" Round Culvert X 2.00	
			L= 96.0' CPP, square edge headwall, Ke= 0.500	

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Inlet / Outlet Invert= 13.10' / 12.60' S= 0.0052 '/' Cc= 0.900 n= 0.011, Flow Area= 1.77 sf

Primary OutFlow Max=13.64 cfs @ 12.06 hrs HW=15.96' TW=15.32' (Dynamic Tailwater) 1=Culvert (Inlet Controls 13.64 cfs @ 3.86 fps)

Summary for Pond 27P: Ex. SDMH#2 / POC B

Inflow Area =	190,148 sf,100.00% Impervious,	Inflow Depth = 5.86" for 25-Year event
Inflow =	20.87 cfs @ 12.06 hrs, Volume=	92,894 cf
Outflow =	20.87 cfs @ 12.06 hrs, Volume=	92,894 cf, Atten= 0%, Lag= 0.0 min
Primary =	20.87 cfs @ 12.06 hrs, Volume=	92,894 cf
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf
Tertiary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 14.87' @ 12.08 hrs

Flood Elev= 16.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	12.40'	18.0" Round Culvert X 2.00
	•		L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 12.40' / 11.20' S= 0.0400 '/' Cc= 0.900
			n= 0.011, Flow Area= 1.77 sf
#2	Secondary	16.10'	24.0" x 48.0" Horiz. Orifice/Grate C= 0.600
	,		Limited to weir flow at low heads
#3	Tertiary	16.40'	24.0" x 48.0" Horiz. Orifice/Grate C= 0.600
	,		I imited to weir flow at low heads

Primary OutFlow Max=14.49 cfs @ 12.06 hrs HW=14.65' TW=13.92' (Dynamic Tailwater) 1=Culvert (Inlet Controls 14.49 cfs @ 4.10 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=12.40' TW=11.00' (Dynamic Tailwater) 2=Orifice/Grate (Controls 0.00 cfs)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=12.40' TW=11.00' (Dynamic Tailwater) 3=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond 28P: Ex. SDMH #3

Inflow Area =		190,148 sf,100.00% Impervious	, Inflow Depth = 5.86" for 25-Year event
Inflow	=	20.87 cfs @ 12.06 hrs, Volume=	
Outflow	=	20.87 cfs @ 12.06 hrs, Volume=	92,894 cf, Atten= 0%, Lag= 0.0 min
Primary	=	20.87 cfs @ 12.06 hrs, Volume=	92,894 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 14.25' @ 12.07 hrs

Flood Elev= 16.70'

Device	Routing	Invert	Outlet Devices	
#1	Primary	11.00'	24.0" Round RCP_Round 24"	

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L= 303.0' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 11.00' / 8.40' S= 0.0086 '/' Cc= 0.900 n= 0.013, Flow Area= 3.14 sf

Primary OutFlow Max=16.78 cfs @ 12.06 hrs HW=13.92' TW=11.59' (Dynamic Tailwater) 1=RCP Round 24" (Outlet Controls 16.78 cfs @ 5.34 fps)

Summary for Pond 29P: Ex. SDMH #4

Inflow Area = 190,148 sf,100.00% Impervious, Inflow Depth = 5.86" for 25-Year event

Inflow = 20.87 cfs @ 12.06 hrs, Volume= 92,894 cf

Outflow = 20.87 cfs @ 12.06 hrs, Volume= 92,894 cf, Atten= 0%, Lag= 0.0 min

Primary = 20.87 cfs @ 12.06 hrs, Volume= 92,894 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 12.03' @ 12.08 hrs

Flood Elev= 16.10'

Device	Routing	Invert	Outlet Devices
#1	Primary		24.0" Round RCP_Round 24"
	•		L= 62.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 8.40' / 7.80' S= 0.0097 '/' Cc= 0.900
			n= 0.013, Flow Area= 3.14 sf

Primary OutFlow Max=16.33 cfs @ 12.06 hrs HW=11.59' TW=10.42' (Dynamic Tailwater) 1=RCP Round 24" (Inlet Controls 16.33 cfs @ 5.20 fps)

Summary for Pond 30P: Ex. SDMH #5

Inflow Area = 190,148 sf,100.00% Impervious, Inflow Depth = 5.86" for 25-Year event

Inflow = 20.87 cfs @ 12.06 hrs, Volume= 92,894 cf

Outflow = 20.87 cfs @ 12.06 hrs, Volume= 92,894 cf, Atten= 0%, Lag= 0.0 min

Primary = 20.87 cfs @ 12.06 hrs, Volume= 92,894 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 10.62' @ 12.06 hrs

Flood Elev= 16.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	7.80'	24.0" Round RCP_Round 24"
	•		L= 78.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.80' / 6.45' S= 0.0173 '/' Cc= 0.900
			n= 0.013, Flow Area= 3.14 sf

Primary OutFlow Max=19.27 cfs @ 12.06 hrs HW=10.42' (Free Discharge)
1=RCP Round 24" (Inlet Controls 19.27 cfs @ 6.13 fps)

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Summary for Pond 31P: Pr. SDMH #4

Inflow Area = 187,434 sf,100.00% Impervious, Inflow Depth = 2.55" for 25-Year event

Inflow = 16.97 cfs @ 12.06 hrs, Volume= 39,775 cf

Outflow = 16.97 cfs @ 12.06 hrs, Volume= 39,775 cf, Atten= 0%, Lag= 0.0 min

Primary = 16.97 cfs @ 12.06 hrs, Volume= 39,775 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 16.41' @ 12.11 hrs

Flood Elev= 16.60'

Device	Routing	Invert	Outlet Devices
#1	Primary		18.0" Round Culvert X 2.00
			L= 29.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 13.25' / 13.10' S= 0.0052 '/' Cc= 0.900
			n= 0.011. Flow Area= 1.77 sf

Primary OutFlow Max=0.00 cfs @ 12.06 hrs HW=15.87' TW=15.91' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond 32P: Ex. SDMH#1

Inflow = 5.22 cfs @ 12.24 hrs, Volume= 53,778 cf

Outflow = 5.22 cfs @ 12.24 hrs, Volume= 53,778 cf, Atten= 0%, Lag= 0.0 min

Primary = 5.22 cfs @ 12.24 hrs, Volume= 53,778 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Peak Elev= 16.42' @ 12.13 hrs

Flood Elev= 17.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	13.20'	24.0" Round Culvert
	_		L= 18.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 13.20' / 13.10' S= 0.0056 '/' Cc= 0.900
			n= 0.011, Flow Area= 3.14 sf

Primary OutFlow Max=0.00 cfs @ 12.24 hrs HW=15.79' TW=15.88' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Link 25L: Bedford Street Garage

Inflow = 0.73 cfs @ 12.21 hrs, Volume= 183 cf

Primary = 0.73 cfs @ 12.21 hrs, Volume= 183 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 6S: Pr. Area #1 Runoff Area=2,714 sf 100.00% Impervious Runoff Depth=7.24"

Tc=5.0 min CN=98.0 Runoff=0.47 cfs 1,638 cf

Subcatchment 7S: Pr. Area #2 Runoff Area=115,349 sf 100.00% Impervious Runoff Depth=7.24"

Tc=10.0 min CN=98.0 Runoff=16.97 cfs 69,599 cf

Subcatchment 8S: Pr. Area #3 Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=7.24"

Tc=5.0 min CN=98.0 Runoff=6.57 cfs 23,047 cf

Subcatchment 9S: Pr. Area #4 Runoff Area=33,888 sf 100.00% Impervious Runoff Depth=7.24"

Tc=5.0 min CN=98.0 Runoff=5.83 cfs 20,447 cf

Subcatchment 10S: Pr. Area #5 Runoff Area=322 sf 100.00% Impervious Runoff Depth=7.24"

Tc=5.0 min CN=98.0 Runoff=0.06 cfs 194 cf

Pond 10P: Parking Lot Peak Elev=16.61' Storage=5,827 cf Inflow=23.28 cfs 92,786 cf

Primary=14.97 cfs 33,187 cf Secondary=5.60 cfs 58,039 cf Tertiary=3.25 cfs 1,860 cf Outflow=21.55 cfs 93,086 cf

Pond 11P: Pr. SDMH #1 Peak Elev=15.50' Inflow=20.80 cfs 105,598 cf

Primary=19.37 cfs 102,945 cf Secondary=1.49 cfs 2,653 cf Outflow=20.80 cfs 105,598 cf

Pond 17P: Retention System#1 Peak Elev=16.73' Storage=7,822 cf Inflow=5.83 cfs 20,447 cf

Primary=6.47 cfs 14,372 cf Secondary=0.92 cfs 140 cf Outflow=6.45 cfs 14,512 cf

Pond 20P: SDMH / POC C Peak Elev=12.37' Inflow=1.54 cfs 2,847 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=1.54 cfs 2,847 cf

Pond 26P: Pr. SDMH #3 / POC A Peak Elev=16.37' Inflow=20.80 cfs 105,598 cf

18.0" Round Culvert x 2.00 n=0.011 L=96.0' S=0.0052 '/' Outflow=20.80 cfs 105,598 cf

Pond 27P: Ex. SDMH#2 / POC B Peak Elev=14.83' Inflow=19.79 cfs 104,583 cf

Primary=19.79 cfs 104,583 cf Secondary=0.00 cfs 0 cf Tertiary=0.00 cfs 0 cf Outflow=19.79 cfs 104,583 cf

Pond 28P: Ex. SDMH #3 Peak Elev=13.95' Inflow=19.79 cfs 104,583 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=19.79 cfs 104,583 cf

Pond 29P: Ex. SDMH #4 Peak Elev=11.80' Inflow=19.79 cfs 104,583 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=19.79 cfs 104,583 cf

Pond 30P: Ex. SDMH #5 Peak Elev=10.51' Inflow=19.79 cfs 104,583 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=19.79 cfs 104,583 cf

Pond 31P: Pr. SDMH #4 Peak Elev=16.59' Inflow=16.03 cfs 47,560 cf

18.0" Round Culvert x 2.00 n=0.011 L=29.0' S=0.0052'/' Outflow=16.03 cfs 47,560 cf

Pond 32P: Ex. SDMH#1 Peak Elev=16.41' Inflow=5.60 cfs 58,039 cf

24.0" Round Culvert n=0.011 L=18.0' S=0.0056 '/' Outflow=5.60 cfs 58,039 cf

Type III 24-hr 50-Year Rainfall=7.48" Printed 9/30/2022

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Link 25L: Bedford Street Garage

Inflow=3.25 cfs 1,860 cf Primary=3.25 cfs 1,860 cf

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 6S: Pr. Area #1

Runoff Area=2,714 sf 100.00% Impervious Runoff Depth=8.17"

Tc=5.0 min CN=98.0 Runoff=0.53 cfs 1,848 cf

Subcatchment 7S: Pr. Area #2

Runoff Area=115,349 sf 100.00% Impervious Runoff Depth=8.17"

Tc=10.0 min CN=98.0 Runoff=19.09 cfs 78,533 cf

Subcatchment 8S: Pr. Area #3

Runoff Area=38,197 sf 100.00% Impervious Runoff Depth=8.17"

Tc=5.0 min CN=98.0 Runoff=7.39 cfs 26,006 cf

Subcatchment 9S: Pr. Area #4

Runoff Area=33,888 sf 100.00% Impervious Runoff Depth=8.17"

Tc=5.0 min CN=98.0 Runoff=6.56 cfs 23,072 cf

Subcatchment 10S: Pr. Area #5

Runoff Area=322 sf 100.00% Impervious Runoff Depth=8.17"

Tc=5.0 min CN=98.0 Runoff=0.06 cfs 219 cf

Pond 10P: Parking Lot

Peak Elev=16.71' Storage=7,518 cf Inflow=27.53 cfs 105,657 cf

Primary=21.95 cfs 36,723 cf Secondary=7.69 cfs 62,706 cf Tertiary=9.90 cfs 6,461 cf Outflow=30.63 cfs 105,891 cf

Pond 11P: Pr. SDMH #1

Peak Elev=17.08' Inflow=33.72 cfs 115,447 cf

Primary=31.69 cfs 112,107 cf Secondary=2.03 cfs 3,341 cf Outflow=33.72 cfs 115,447 cf

Pond 17P: Retention System#1

Peak Elev=16.91' Storage=7,824 cf Inflow=6.56 cfs 23,072 cf

Primary=7.20 cfs 16,018 cf Secondary=2.36 cfs 1,119 cf Outflow=7.29 cfs 17,137 cf

Pond 20P: SDMH / POC C

Peak Elev=12.48' Inflow=2.04 cfs 3,560 cf

18.0" Round Culvert n=0.013 L=100.0' S=0.0040 '/' Outflow=2.04 cfs 3,560 cf

Pond 26P: Pr. SDMH #3 / POC A

Peak Elev=18.03' Inflow=33.72 cfs 115,447 cf

18.0" Round Culvert x 2.00 n=0.011 L=96.0' S=0.0052 '/' Outflow=33.72 cfs 115,447 cf

Pond 27P: Ex. SDMH#2 / POC B

Peak Elev=18.87' Inflow=31.80 cfs 113,954 cf

Primary=29.88 cfs 112,635 cf Secondary=1.92 cfs 963 cf Tertiary=1.74 cfs 357 cf Outflow=31.80 cfs 113,954 cf

Pond 28P: Ex. SDMH #3

Peak Elev=18.80' Inflow=31.80 cfs 113,954 cf

24.0" Round Culvert n=0.013 L=303.0' S=0.0086 '/' Outflow=31.80 cfs 113,954 cf

Pond 29P: Ex. SDMH #4

Peak Elev=14.28' Inflow=31.80 cfs 113,954 cf

24.0" Round Culvert n=0.013 L=62.0' S=0.0097 '/' Outflow=31.80 cfs 113,954 cf

Pond 30P: Ex. SDMH #5

Peak Elev=13.22' Inflow=31.80 cfs 113,954 cf

24.0" Round Culvert n=0.013 L=78.0' S=0.0173 '/' Outflow=31.80 cfs 113,954 cf

Pond 31P: Pr. SDMH #4

Peak Elev=19.00' Inflow=26.03 cfs 52,741 cf

18.0" Round Culvert x 2.00 n=0.011 L=29.0' S=0.0052 '/' Outflow=26.03 cfs 52,741 cf

Pond 32P: Ex. SDMH#1

Peak Elev=18.04' Inflow=7.69 cfs 62,706 cf

24.0" Round Culvert n=0.011 L=18.0' S=0.0056 '/' Outflow=7.69 cfs 62,706 cf

Type III 24-hr 100-Year Rainfall=8.41"

Prepared by RVDI

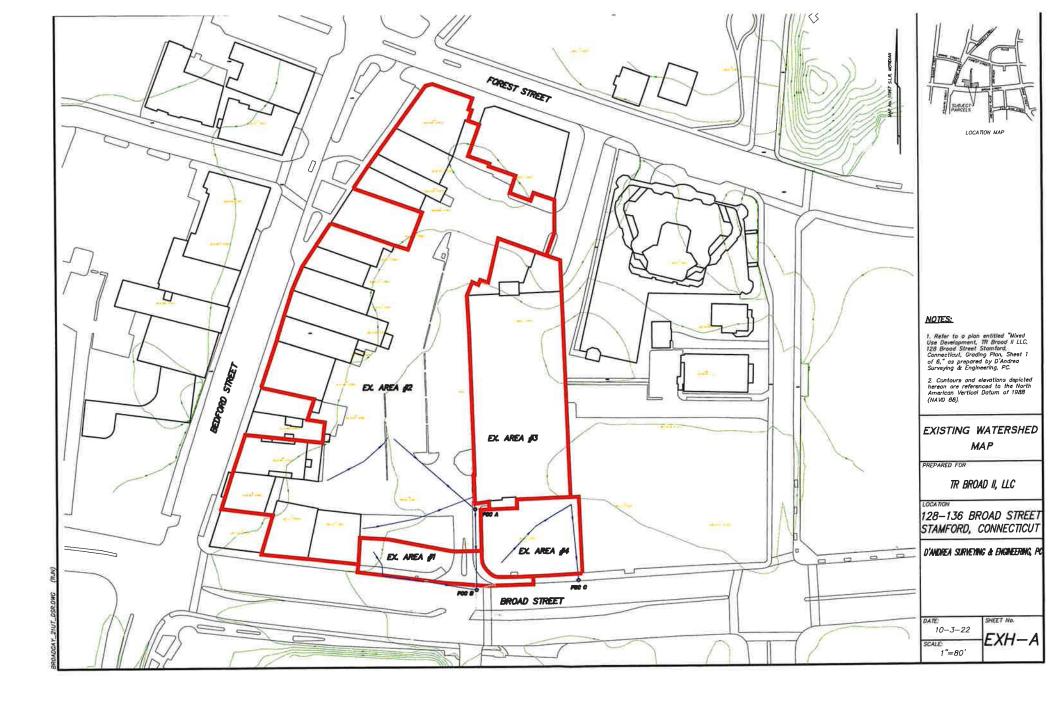
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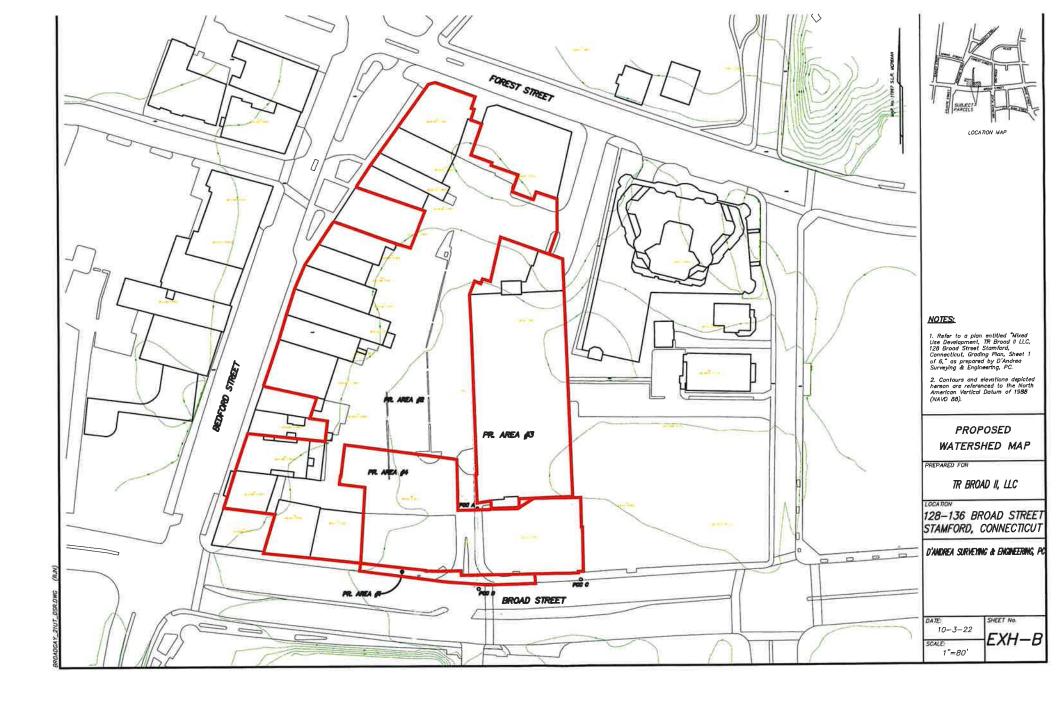
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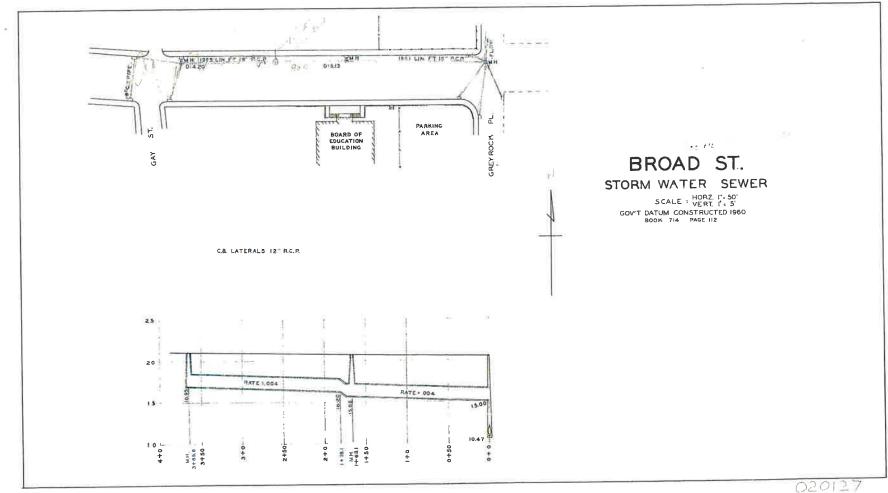
Page 21

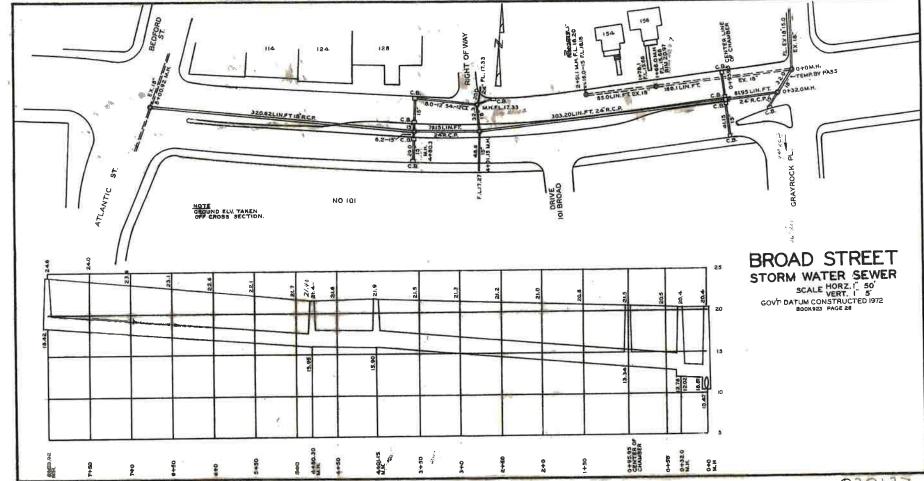
Link 25L: Bedford Street Garage

Inflow=9.90 cfs 6,461 cf Primary=9.90 cfs 6,461 cf

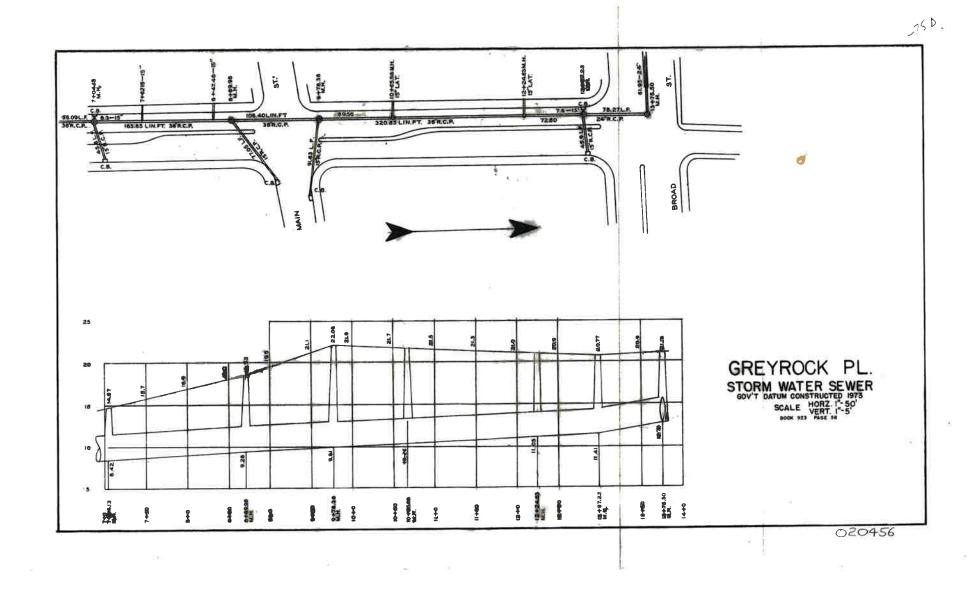


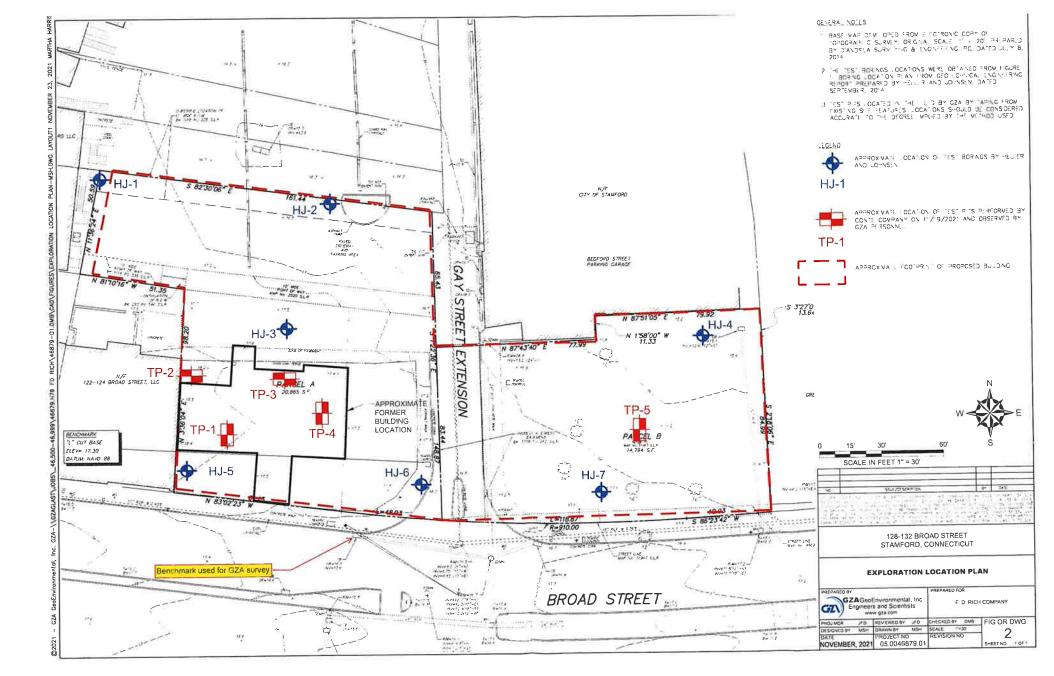






020127







City of Stamford Engineering Bureau 888 Washington Boulevard, 7th Floor Stamford, CT 06901 Phone 203-977-4189

CHECKLISTS

Projec	t Name: Mixed Use Development
Projec	t Address 128-136 Broad Street
Prope	ty Owner(s) TR Broad II LLC
Tax A	count Number(s) 001-2688, 004-0515
Engin	eer's Signature Date: Date:
100	
	ecklists must be completed and submitted. Provide a brief explanation for any items not provided. c boxes as completed or N/A as not applicable.
Chec	k boxes as completed or N/A as not applicable.
Chec	Existing Conditions Plan
Chec	Existing Conditions Plan Stormwater Management Report

Checklist for Existing Conditions Plan

I. General Information

√	Site address
✓	Orientation, block, zone, City, street name
✓	Applicant name and legal address
√	Surveyor name, address, contact information
1	North arrow, bar scale, horizontal and vertical datum
1	24" x 36" sheet size unless otherwise approved
✓	Existing conditions survey shall be prepared in accordance with the Minimum Standards for Surveys and Maps in the State of Connecticut. The class of survey shall be A-2 and T-2 and shall be represented as such on the map. The base map shall be sealed and signed by a Professional Land Surveyor licensed in the State of Connecticut.
√	Drawing scale shall be set at $1'' = 20'$ or $1'' = 40'$ when possible

May 2020 Page 1



City of Stamford Engineering Bureau 888 Washington Boulevard, 7th Floor Stamford, CT 06901 Phone 203-977-4189

II. Existing Conditions Plan Elements

✓	Show and label all property boundaries with linear bearing / distances and curve information
	Required zoning setbacks
✓	Show and label monument information
✓	Show and label at least one permanent benchmark on the parcel with northing, easting and elevation
✓	Label adjacent property ownership information
✓	Existing contours based on NAVD 88 (no exceptions) at 2 foot contour interval or 1 foot contour interval when slope is flatter than 2 percent at a minimum of 20 ft. beyond the property boundaries of the subject parcel
✓	Show spot elevations at low points, high points, and where topography is flatter than 2 percent
1	All buildings and structures (label current use and finished floor elevations)
1	All pavement, parking, driveways, property access points
✓	All roadways, streets, and rights-of-way. Label streets as public or private with street name
1	All patios, decks, walkways, sidewalks, curb ramps (both adjacent to and opposite and existing roadways or intersections)
✓	Show and label (size, material, inverts) all existing utilities (overhead and underground) within the right-of-way and the project site (label ownership) including but not limited to water, gas and electrical services, wells, storm sewers, sanitary sewers and subsurface sewerage disposal systems.
1	Show and label existing conveyance systems (swales, ditches, storm drains) including dimensions, elevations, sizes, slopes, and direction of flow
✓	Show and label boundaries of all easements, both public and private, with type, owner, and width
✓	Show and label all other existing features and improvements (e.g. light poles, mature trees of 8" (dbh) diameter or greater, vegetation, walls with top and bottom elevations, fences, pavement markings)

III. Resource Areas

Show and label limits of inland wetlands, tidal wetlands and any associated setbacks. Show and label existing natural site features including tree canopy, outcroppings, permanent and intermittent
watercourses, waterbodies, streams
Show and label limits of floodplain and floodway along with FIRM references (Community Number, Panel, Suffix, and Date) including any effective Letters of Map Revision/Amendment, zone designation and elevation.
Show and label any Conservation Easement Areas
Show and label Connecticut Coastal Jurisdiction Line (CJL)

May 2020 Page 2



Checklist for Stormwater Management Report

I. Project Report

Α	Applicant / Site Information
✓	Applicant name, legal address, contact information (email & phone)
✓	Engineers name, legal address, contact information (email & phone)
✓	Site address and legal description
✓	Current / proposed zoning and land use
✓	Site vicinity map (8.5" x 11")
В.	Project Description and Purpose
✓	Project description including proposed project elements and anticipated construction schedule
C.	Existing Conditions Description
√	Site area, ground cover, vegetation, features (roads, buildings, utilities, etc.)
1	Site topography, slopes, drainage patterns, conveyances systems (swales, storm drains, etc.), stormwater
	discharge locations Receiving waterbody information including stormwater impairments and TMDL information (See the most recent State of Connecticut Integrated Water Quality Report)
✓	Site soils information including soil types, hydrologic soil group, bedrock / outcroppings, groundwater elevation, significant geologic features
✓	Provide NRCS Soils Mapping
	Resource protection areas (wetlands, streams, lakes, etc.), buffers, floodplains, floodways
D.	Summary of Applicable General Design Criteria
✓	Methodology, design storm frequency
✓	Hydrologic design criteria
✓	Hydraulic design criteria
	Flood hazard areas
	Applying under "Lite" Stormwater Management: Skip to Section I (Refer to Flow Chart on page vii of the City of Stamford Stormwater Drainage Manual)
E.	Project Type in Accordance with Standard 1 Definitions
	Area of disturbance, receiving waterbody classification (High Quality, Tidal Wetlands, Direct Waterfront)
✓	Project type (development, redevelopment, linear development)
1	Pollutant reduction standard per flowchart Section 2.4



Ez	Summary of LID Site Constraints			
	Description of sensitive areas for protection			
	Mature tree inventory, which shall include 8-inch (dbh) diameter trees or greater			
Steep slopes				
	Ledge and bedrock depth			
Seasonal high groundwater elevation				
	Poliutant hotspots			
	Summary of infiltration rates			
G.	Summary of Proposed Stormwater Treatment Practices			
√	Proposed LID controls (i.e. minimize impervious, minimize DCIA, minimize disturbance, increase time of concentrations, other LID controls and strategies)			
✓	Location, size, types			
1	Design criteria and references			
✓	Stormwater treatment practice, drainage area characteristics / details			
Н.	Summary of Compliance with Standards 1			
1	Required pollutant reduction criteria			
1	Provided pollutant reduction (WQV) by stormwater treatment practice			
✓	Summary of compliance with Standard 1			
I.	Summary of Compliance with Standards 2, 3, and 4			
1	Description of proposed stormwater management system			
1	Pre-development site hydrology with delineation of each watershed area and sub-basin			
1	Post-development site hydrology with delineation of each watershed area and sub-basin			
1	Comparison table of pre- and post-development hydrology, peak flow, volume, and percent difference			
✓	Summary table of watershed areas and sub-basin areas, time of concentration and runoff coefficients			
	Summary table demonstrating the 2-year, 24-hour post development peak flow rate is less than or equal to the			
✓	lowest of either: - The pre-development 1-year, 24-hour storm peak flow rate - 50 percent of the pre-development 2-year, 24-hour storm peak flow rate			
1	Conveyance protection, emergency outlet sizing			
	Hydraulic grade line summary and tail water elevation used in analysis			
1	Construction erosion and sediment control description, Standard 3			
1	Operation and Maintenance, maintenance tasks and schedule on construction plans per Standard 4			



J.	Summary of Compliance with Applicable Drainage Facility Design Requirements			
√	Description of applicable design requirements and compliance			
✓	Description of proposed drainage facilities and compliance			
K.	K. Stormwater Management Report			
/	Signed and stamped by professional engineer licensed in the State of Connecticut			
1	Drainage impact statement in accordance with Standard 5B.			
II.	II. Supporting Calculations (as appendix to Project Report)			
	Applying under "Lite" Stormwater Management: Skip to Section N			
L.	Water Quality Volume / Water Quality Flow Calculations			
√	Calculations demonstrating the total Water Quality Volume generated by the post-development site and the required retention/treatment volume per Standard 1 in cubic feet.			
✓	Calculations demonstrating the total Water Quality Volume retained/treated by each stormwater treatment practice and the total Water Quality Volume generated by the post-development contributing drainage area to each stormwater treatment practice			
M.	Stormwater Treatment Practice Sizing Calculations Calculations demonstrating how each stormwater treatment practice has been designed and sized in accordance with the Structural Stormwater BMP Design references in Appendix B. Calculations will vary by stormwater treatment practice, but a minimum, applicants shall provide calculations in accordance with design criteria from the Connecticut Stormwater Quality Manual.			
N.	Hydrologic and Hydraulic Design Calculations			
1	Stream channel protection, Standard 2A			
1	Conveyance protection, Standard 2B			
1	Peak flow control (1-year, 2-year, 5-year, 10-year, 25-year, and 50-year storms), Standard 2C			
	Inlet analysis			
	Gutter flow (Site by site basis as requested by Engineering Bureau)			
✓	Storm sewers and culverts (velocities, capacity, hydraulics)			
	Hydraulic grade line required when pipe is flowing at full capacity o Provide existing and proposed summary table o Provide existing and proposed mapping, label structures			
✓	Detention facilities (outlet structure, stage/storage, freeboard)			
1	Emergency outlet sizing, safely pass the 100 year storm, Standard 2D			
	Outlet protection calculations, based on conveyance protection (i.e. ripran, energy dissipater)			



0.	Hydrologic and Hydraulic Model, Existing and Proposed			
√	Drainage routing diagram			
√	Summary			
1	Storage pond input			
P.				
	Downstream analysis, Standard 2E			
111	III. Supporting Mapping (as appendix to Project Report)			
Q.	Pre-Development Drainage Basin Area Mapping			
✓	11" x 17" or 8.5" x 11" sheet size			
✓	Topography, drainage patterns, drainage area boundaries and sub basins, flow paths, times of concentration			
1	Locations of existing stormwater discharges			
	Perennial and intermittent streams, wetlands, and floodplain / floodways			
	NRCS soil types, locations, boring locations, infiltration testing locations			
	Vegetation and groundcover			
✓	Existing roads, buildings, driveways, parking areas, walks, patios, pools and other impervious surfaces, decks and other structures			
✓	Location, size, type of existing structural stormwater controls, facilities and conveyance systems			
R.	Post-Development Drainage Basin Area Mapping			
✓	11" x 17" or 8.5" x 11" sheet size			
✓	Topography, drainage patterns, drainage area boundaries and sub basins, flow paths, times of concentration			
✓	Locations of proposed stormwater discharges			
	Perennial and intermittent streams, wetlands, and floodplain / floodways			
	NRCS soil types, locations, boring locations, infiltration testing locations			
	Vegetation, ground cover and proposed limits of clearing/disturbance			
✓	Proposed, roads, buildings, driveways, parking areas, walks, patios, pools and other impervious surfaces, decks and other structures			
✓	Location, size, type of proposed structural stormwater controls, facilities and conveyance systems			
IV.	DCIA Tracking Worksheet (as appendix to Project Report)			
1	DCIA Tracking Worksheet (Use form found in Appendix E)			



V. Proposed LID Review Map

	Applying under "Lite" Stormwater Management - Proposed LID Review Map NOT required.		
۹.	General		
	Site address		
	Applicant name, legal address, contact information		
	Engineers name, address, contact information		
	North arrow, bar scale, horizontal and vertical datum		
	Drawing scale shall be set at 1"=20' or 1"=40' when possible		
	Signed and stamped by a Licensed Professional Engineer in the State of Connecticut		
	11" x 17" or 24" x 36" sheet size unless otherwise approved Existing and proposed contours based on NAVD 88 at 2 foot contour interval or 1 foot contour interval when slope		
	is flatter than 2 percent		
	Locations of existing stormwater discharges Roads, buildings, driveways, parking areas, walks, patios, pools and other impervious surfaces, and decks and other structures		
	Location, size, ownership of stormwater conveyance systems (swales, pipes, etc.)		
i.	LID Constraints:		
	Boring / test pit locations		
	Infiltration testing locations and results		
	Vegetation and proposed limits of clearing / disturbance		
	NRCS soils mapping		
	Steep slopes		
	Surface waters / Perennial and intermittent streams		
	Resource protection areas and buffers, wetlands, floodplain / floodways		
	Existing vegetation and mature trees, which shall include 8-inch (dbh) diameter trees or greater		
	Poor soils (HSG C & D)		
	Shallow bedrock / ledge		
	Seasonal high groundwater elevation		
Other site constraints (e.g. brownfield caps)			
·	Proposed Stormwater Treatment Measures:		
	Location, size, type, limits, and WQV provided by each proposed stormwater treatment practices		
	Drainage area to each proposed stormwater treatment practice (total area, impervious area, WQV)		
)	Site Summary Table:		
	Total site area, disturbed area, pre- and post-development impervious areas		
	Required pollutant reduction volume (retention or detention)		
Provided pollutant reduction volume (retention or detention)			



Checklist for Stormwater Management Plan / Construction Plans

_A	<u>General</u>			
✓	Site orientation, address and legal description			
✓	Applicant name, legal address, contact information			
✓	Engineers name, address, contact information			
1	North arrow, bar scale, horizontal and vertical datum			
1	Drawing scale shall be set at 1"=20' or 1"=40' when possible			
1	Stamped by a Licensed Professional Engineer in the State of Connecticut			
✓	24" x 36" sheet size unless otherwise approved			
B. Site Development Plans				
1	City of Stamford Standard Notes			
1	As required by the Drainage Maintenance Agreement, provide a written narrative describing the nature of the proposed development activity and the program for operation and maintenance of drainage facilities and control measures throughout the life of the project.			
✓	Existing and proposed contours based on NAVD 88 at 2 foot contour interval or 1 foot contour interval when slope is flatter than 2 percent			
1	All required spot elevations to clearly depict positive pitch			
1	Top and bottom elevation of all walls			
✓	Roads, buildings, driveways, parking areas, walks, patios, pools and other impervious surfaces, and decks and other structures			
1	All utilities and easements			
✓	Location, size, maintenance access, type of proposed structural stormwater controls and facilities with elevations and inverts			
✓	Location, size, maintenance access, type of proposed non-structural stormwater controls and facilities with elevations and inverts			
✓	Location, size, type of proposed stormwater infrastructure, inlets, manholes, infiltration and detentions systems, control structures with elevations and inverts			
	Location, size, ownership of stormwater conveyance systems (swales, pipes, etc.) with elevations and inverts			
1	Identify roof leaders, curtain drains and foundation drains with elevations and inverts			
1	Proposed water quality treatment systems, size and model type			
✓	Final stabilization measures which may include slope stabilization			
C	Erosion and Sedimentation Control Plan			
J.	Dhasing and sekedule			

✓	Phasing and schedule		
1	Construction access and staging and stock pile areas		
1	Operation and maintenance of erosion and sedimentation controls		
	Tree protection		
1	Downstream protection such as location of silt fencing		
✓	Limit of disturbance		
1	Construction fencing		



_D.	Construction Details		
1	Standard City of Stamford details		
✓	Infiltration system details		
1	Control structure details		
1	Water quality treatment details		
	Infiltration testing results		
	Checklist for Certificate of Occupancy		

Final Improvement Location Survey	
	Stormwater Management Certification Form
Final DCIA Tracking Worksheet	
	Standard City of Stamford Drainage Maintenance Agreement (Agreement Covenant)

Other Certifications at the discretion of the Engineering Bureau and/or EPB

Wall Certification
Landscape Certification
Landscape Maintenance Agreement
Waiver Covering Storm Sewer Connection
Waiver Covering Granite Block, Depressed Curb, and Driveway Aprons
Flood Certification

FINAL SITE PLAN REVIEW SET "MIXED USE DEVELOPMENT"

LOCATION

128 BROAD STREET STAMFORD, CONNECTICUT

PREPARED FOR

TR BROAD II LLC

BLOCK No. 176
"C-G" ZONING DISTRICT
PARCEL A = 20,865 SQ.FT.
PARCEL B = 14,794 SQ.FT.

LOCATION MAP

SHEET NDEX

<u>SHEET</u>	<u>TITLE</u>	REVISION	DATE
	TOPOGRAPHIC SURVEY	3	6-28-22
1 OF 6	GRADING PLAN	O	10 - 28 - 22
2 OF 6	STORM DRAINAGE & UTILITY PLAN	0	10-28-22
3 OF 6	PAVEMENT MARKINGS & SIGNAGE PLAN	0	10 - 28 - 22
4 OF 6	SEDIMENTATION & EROSION CONTROL PLAN	Ο	10-28-22
5 OF 6	NOTES AND DETAILS	Ο	10-28-22
6 OF 6	DETAILS	0	10-28-22
1 OF 1	OFFSITE PARKING LOT MODIFICATION PLAN	0	10 - 28 - 22
1 OF 1	CROSS SECTION PLAN	0	10 - 28 - 22
1 OF 1	CONSTRUCTION LOGISTICS PLAN	0	10 - 28 - 22

ENGINEERING PLANS PREPARED BY:

D'ANDREA SURVEYING & ENGINEERING, PC. LEONARD C. D'ANDREA, CT PE No. 14869

ONLY COPIES OF THIS SET, BEARING AN ORIGINAL IMPRINT OF THE ENGINEER'S / SURVEYOR'S EMBOSSED SEAL SHALL BE CONSIDERED TO BE TRUE, VALID COPIES.

	D'ANDRI P.O. BOX 549 RIVERSIDE, CT	EA SURVEYING & ENGINEERING, PC • LAND PLANNERS • ENGINEERS • SURVEYORS 6 NEIL LANE 06878 TEL. 637-1779	
	PROJECT	MIXED USE DEVELOPMENT	
	PREPARED FOR	TR BROAD II LLC	
ZONING SUBMISSION	LOCATION	128 BROAD STREET	

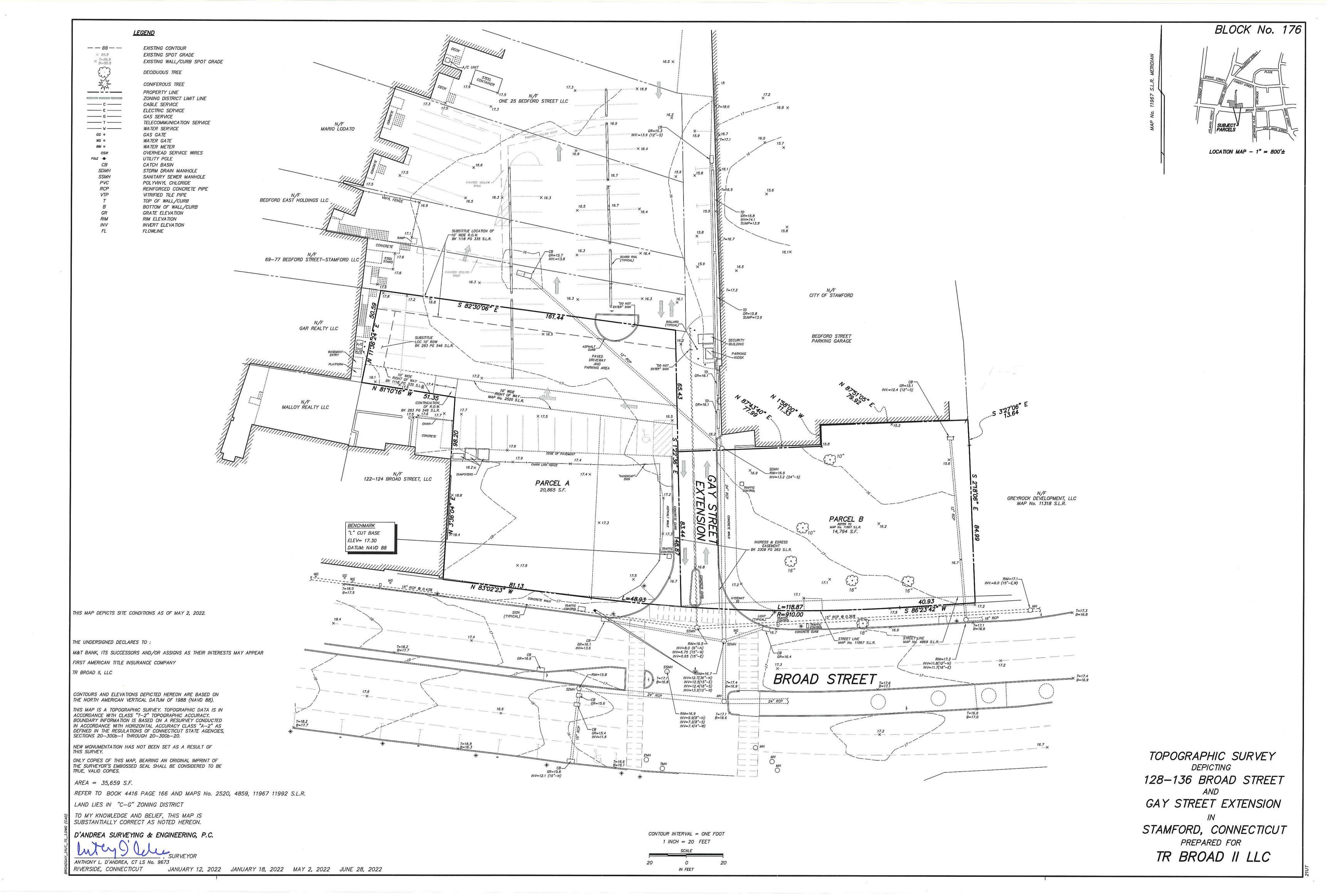
STAMFORD, CONNECTICUT

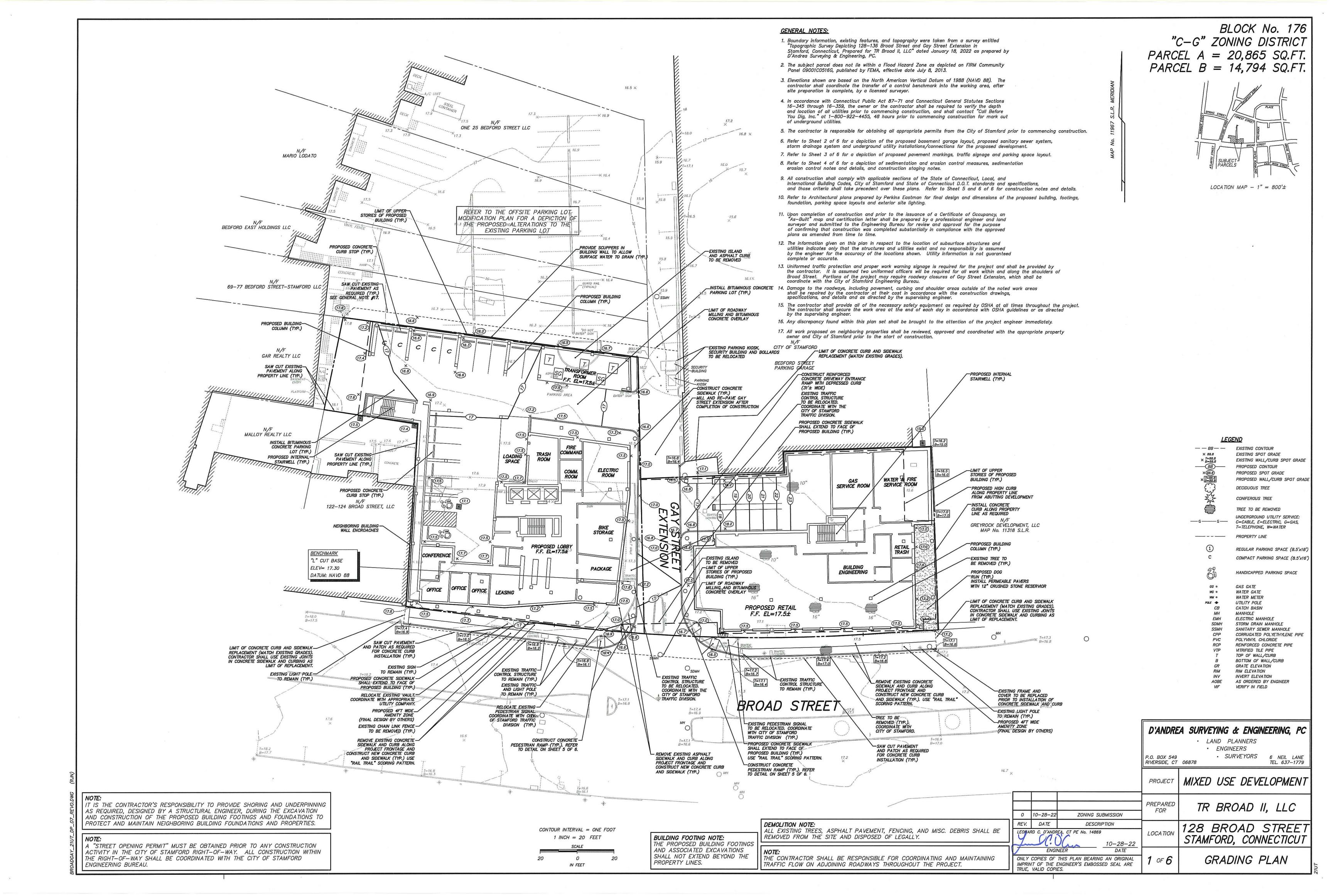
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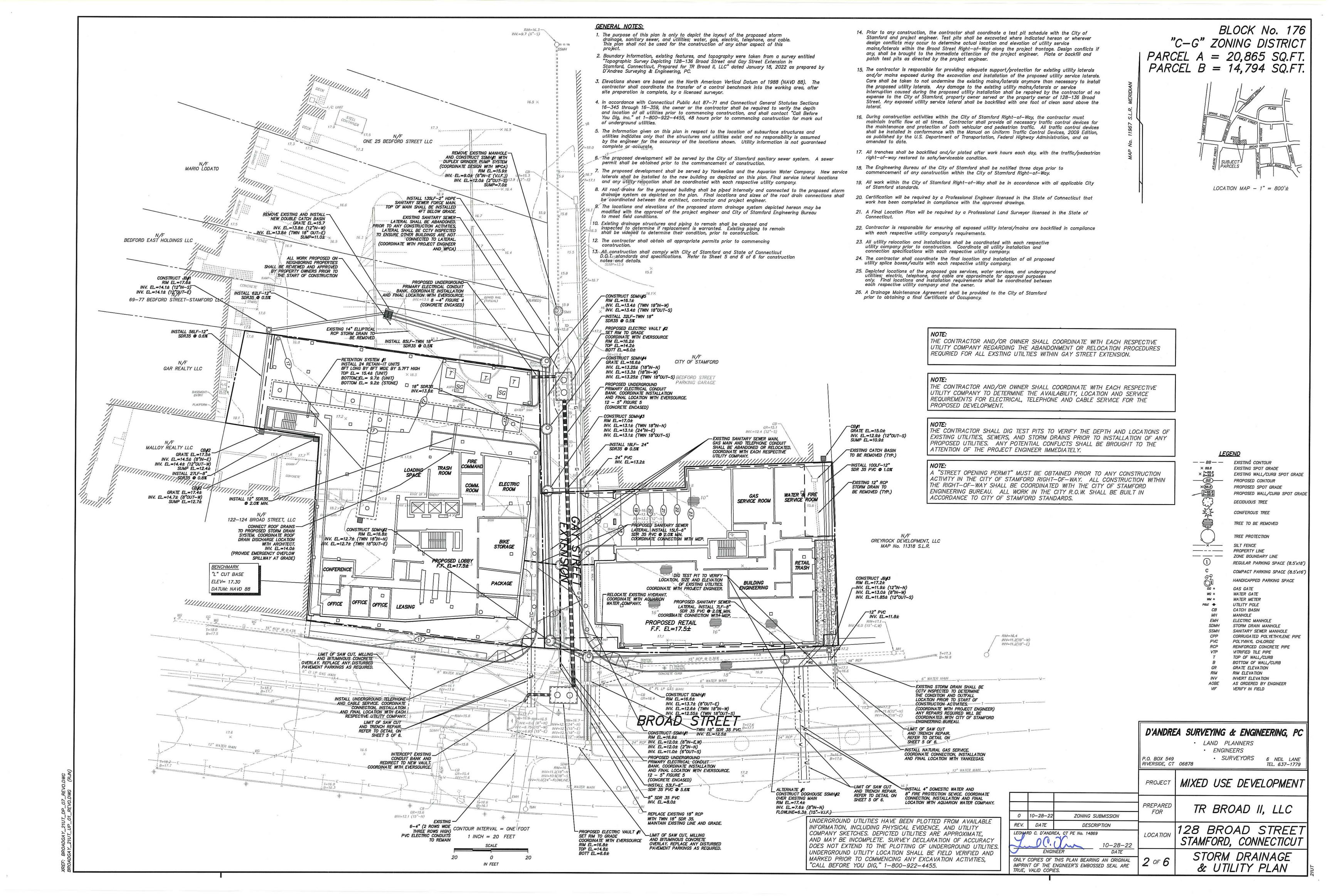
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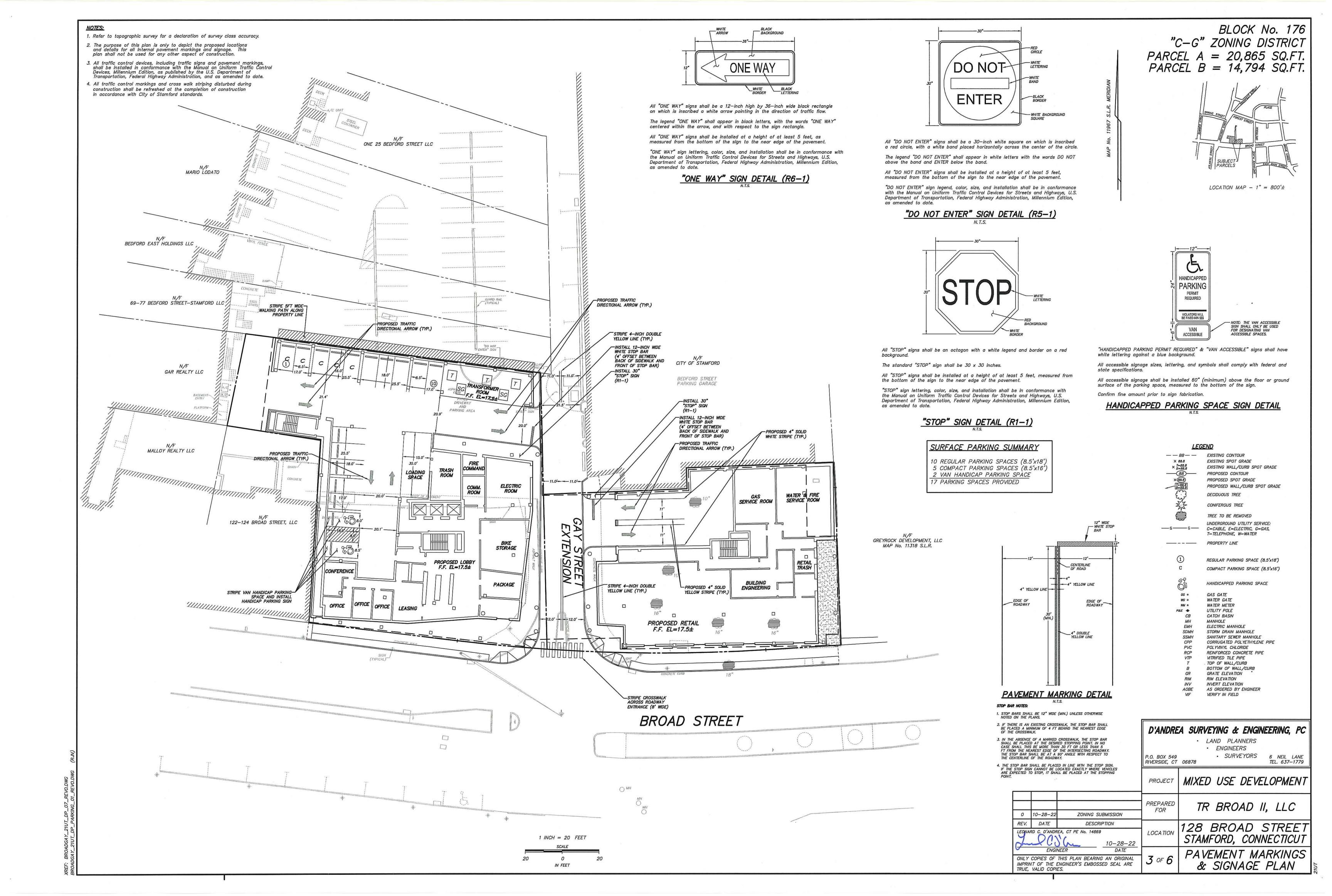
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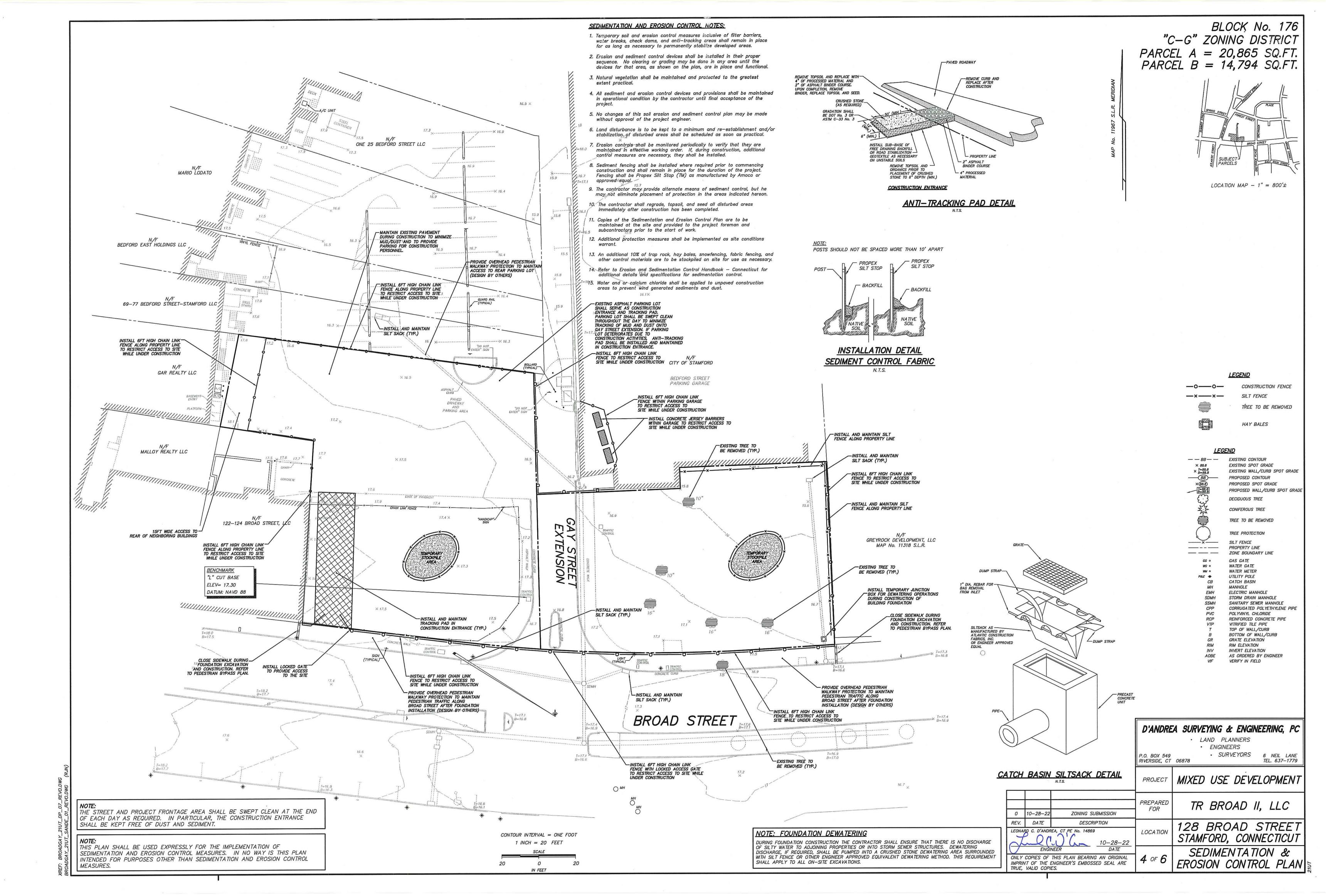
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CONSTRUCTION NOTES:

- 1. In accordance with Connecticut Public Act 87-71 and Connecticut General Statutes Sections 16-345 through 16-359, the owner or the contractor shall be required to verify the depth and location of all utilities prior to commencing construction, and shall contact "Call Before You Dig, Inc." at 1-800-922-4455, 48 hours prior to commencing construction for mark out of
- 2. The contractor shall be solely responsible to coordinate his work with the work being done by others. The contractor shall likewise bear the responsibility for delays or other factors related to the work by others. No claims shall be allowed due to the contractor's failure to adequately coordinate such work.
- I. THE CITY OF STAMFORD ENGINEERING BUREAU SHALL BE NOTIFIED THREE DAYS PRIOR TO THE COMMENCEMENT OF EACH PHASE OF CONSTRUCTION AFFECTING THE CITY RIGHT-OF-WAY.
- 4. All construction shall comply with applicable sections of the State of Conecticut, Local, and International Building codes, and those criteria shall take precedent over these plans.
- 5. All construction shall be inspected by a professional engineer prior to backfill and as the work
- 6. The project engineer shall be notified a minimum of three working days prior to the commencement of each phase of construction.
- 7. Appropriate measures shall be taken to control any sedimentation and erosion which may result during construction.
- 8. All excavated material shall be stockpiled and contained on-site within silt fencing. The contractor shall be responsible for the removal of all excess material excavated durina construction. All excess material shall be removed in a careful and environmentally sound manner 9. and shall be disposed of legally off-site.
- 9. All specimen trees shall be protected during the construction period, except those specifically designated to be removed, in accordance with generally accepted standards.
- The proposed building shall be designed by an architect in order to conform with current applicable zoning setback criteria and regulations, and a building permit shall be obtained prior to commencing construction.
- 11. Existing utilities in conflict through or above this parcel shall be relocated as directed by the appropriate utility company or the owner. The contractor shall excavate test pits to verify the location and depth of utilities where conflicts may exist.
- 12. Pavement replacement shall be bituminous concrete, placed in accordance with the City of Stamford standards and/or Connecticut State Highway specifications.
- 13. Shoulders and disturbed areas shall receive four inches of topsoil; fine graded and seeded as soon as practical to prevent erosion.
- 14. The contractor shall not commence any paving until the grading and shaping of the compacted gravel base has been approved by the project engineer.
- 15. Regrading, filling, and other such alterations to the site shall be restricted to the minimum level necessary to complete the project as shown on the plan.
- 16. Existing inverts on storm drains, sanitary sewers, and utility conduits shall be field verified where appropriate, before commencing construction. The contractor shall excavate test pits where indicated hereon or wherever design conflicts may occur. The contractor shall notify the project engineer of the test pit schedule. Design conflicts if any, shall be brought to the immediate attention of the project engineer. Plate or backfill and patch test pits as directed by the project engineer.
- 17. The project engineer, with the approval of the owner and City of Stamford, may direct a change in the location of the utilities, storm drainage or sanitary sewer structures to meet field conditions or requirements of final building design.
- 18. Junction boxes shall be 32"x32" as manufactured by Eastern Precast Co., Inc., with Pattern No. 1057, cast iron frame and cover, as manufactured by Campbell Foundry, Co., or engineer approved equal, unless noted otherwise. All junction boxes shall have 2' (minimum) sumps and bell traps, installed immediately upon making pipe connections, unless noted otherwise. 19. Manhole structures shall be precast concrete with gaskets as manufactured by Eastern Precast
- Co., Inc. or engineer approved equal, unless noted otherwise. 20. All gravity PVC storm drain and sanitary sewer pipes shall conform to ASTM D 3034 "Standard
- Specification for type PSM Poly Vinyl Chloride (PVC) Sewer Pipe and Fittings" or approved equal
- 21. All reinforced concrete pipe shall be Class IV with joints as approved by the City of Stamford Engineering Bureau.
- 22. Where unsuitable foundation is encountered during construction of storm drains or sanitary sewers, the contractor shall remove the unsuitable material and replace it with other material approved by the project engineer. All unsuitable material shall be removed from the project area and disposed of legally.
- 23. Bedding and backfill material shall conform to ASTM D2321 specification "standard recommended practice for underground installations of flexible thermoplastic sewer pipe (PVC)."
- 24. All site drainage and sewer connections shall be sloped at 2% (minimum) or as otherwise noted.
- 25. All drainage and sewer conduits if located under a paved or traveled way shall have 2 1/2 foot minimum cover within the municipal right-of-way, or be encased in concrete as ordered by the
- 26. The contractor shall provide all equipment, tools, labor and materials necessary to satisfactorily clean and remove all visible obstructions, dirt, sand, sludge, roots, gravel, stones, etc., from the storm drains, sanitary sewers, and manholes.
- 27. Processed aggregate shall be in accordance with the City of Stamford standards and/or Connecticut State Highway specifications.
- 28. Roadway and parking lot pavement shall be 2 course bituminous concrete placed in accordance with the City of Stamford standards and/or Connecticut State Highway specifications.

29. All existing manhole frames, catch basin grates, and utility structures shall be adjusted to new

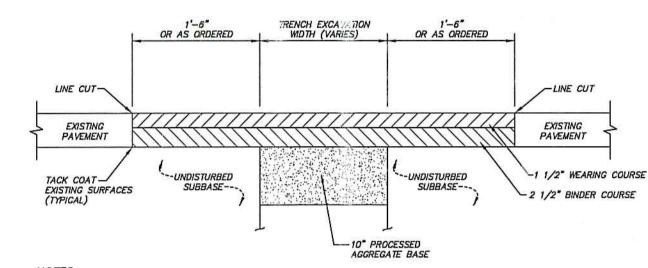
- finish grade as required. Contractor to coordinate with existing utility companies to ensure their facilities are adjusted to finish grade.
- 30. Storm drain manhole sumps and risers shall be 48" diameter as manufactured by Eastern Precast Co., Inc., or engineer approved equivalent. Frames and rims located in the City of Stamford right—of—way shall be pattern no. 1027 as manufactured by Campbell Foundry Co., Inc., or engineer approved equivalent, and shall have "Stamford CONN" cast on cover. Sanitary sewer manhole sumps and risers shall be 48" diameter as manufactured by Eastern Precast Co., Inc., or engineer approved equivalent. Frames and rims located in the City of Stamford right—of—way shall be pattern no. 1027 as
- manufactured by Campbell Foundry Co., Inc., or engineer approved equivalent, and shall have "Sewer" cast on cover. 32. Connections between manholes and PVC sanitary sewer pipes shall be made with flexible rubber boot type connections, sealed water tight with a stainless steel Connections to manholes for reinforced concrete storm and sanitary sewer pipe shall be made with concrete brick masonry and non-shrink grout. The
- manholes are water tight. 33. Precast concrete cone sections shall be eccentric cones, and flat slab tops are to have eccentric openings. Eccentric cone sections shall be used when the vertical distance between the manhole frame and the top of the highest pipe is six (6) feet or greater. Otherwise, flat slab tops shall be used. Aluminum manhole steps (drop form type) shall be provided in all manholes at 12 inch intervals. Each step shall be capable of supporting a minimum load of 1,000 pounds. Wall joints shall be "O-ring" rubber gasket types with the interior

contractor shall make sure that all connections of new sanitary sewers to

- and exterior joint faces sealed with waterproof non-shrink grout. 34. Exterior surfaces of all sanitary manholes shall be coated with two (2) coats of coal—tar sealer as manufactured by Kopper, Mobil or PPG, or engineer approved
- 35. Sanitary sewer manholes shall be watertight; all leaks shall be permanently
- 36. All traffic control devices, including traffic signs and pavement markings, shall be installed in conformance with the Manual on Uniform Traffic Control Devices, Millennium Edition, as published by the U.S. Department of Transportation, Federal Highway Administration, and as amended to date.
- 37. All new utilities including electric, telephone and cable TV shall be installed underground.
- 38. Proposed services such as gas, water, and electric are shown schematically only. Final design for all utilities, other than sewer and drainage shall be provided by the respective utility company.
- 39. Curbs and sidewalks in the City right—of—way shall be constructed in accordance with the City of Stamford standards and specifications. The contractor shall pay specific attention to the location of construction joints.
- 40. The project engineer, with the approval of the City of Stamford, may direct a change in the location of the proposed storm drainage structures to meet field conditions, or requirements of final design.
- 41. Any changes to the plan without the prior written approval of the design engineer is not permitted.
- 42. All traffic control devices, including traffic signs and pavement markings, shall be installed in conformance with the Manual on Uniform Traffic Control Devices, Millennium Edition, as published by the U.S. Department of Transportation, Federal Highway Administration, and as amended to date.
- 43. Stamford Police Officers shall be used during the portion of work involving right-of-way restrictions as required by the City of Stamford to ensure pedestrian, vehicular, and work site safety.
- 44. Pursuant to Sec. 14-314b of the Connecticut General Statutes, no traffic control sign, signal, device, pavement marking, guardrail, or like device or part thereof shall be removed, obstructed, relocated, or otherwise disturbed, altered, or rendered ineffective in any way without the prior approval from the City of Stamford Contractor is responsible for replacement, to the specification and satisfaction of the Engineering Bureau, of any pavement markings or other traffic control devices emoved or damaged due to work done or related activity.

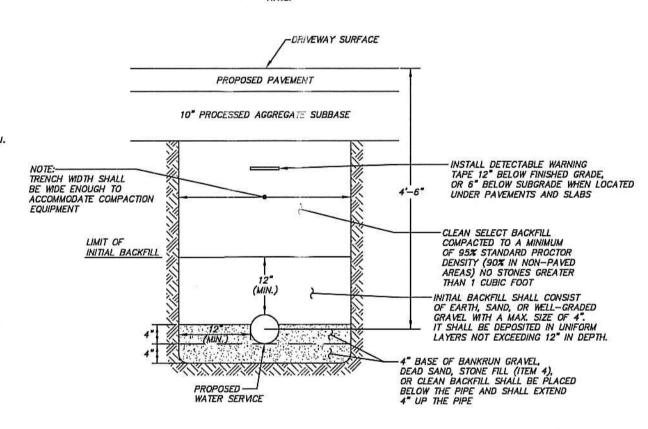
CITY OF STAMFORD STANDARD NOTES:

- A Street Opening Permit is required for all work within the City of Stamford Right-of-Way.
- All work within the City of Stamford Right-or-Way shall be constructed to City of Stamford requirements, the State of Connecticut Basic Building Code and the Connecticut Guidelines for Soil Erosion and Sedimentation Control.
- The City of Stamford Engineering Bureau shall be notified three days prior to any commencement of work within the City of Stamford Right-of- Way.
- 4. Trees within the City of Stamford Right-of-Way to be removed shall be posted in accordance with the Tree Ordinance.
- 5. Prior to any excavation the Contractor and/cr Applicant/Owner, in accordance with Public Act 77-350, shall be required to contact "Call Before You Dig" at 1-800-922-4455 for mark out of
- 6. All retaining walls greater than three (3) fee: are required to be designed, and inspected during construction by a Professional Engineer licensed in the State of Connecticut. Certification of the retaining wall shall be required prior to issuance of a Certificate of Occupancy and/or bond release.
- 7. Certification will be required by a Professional Engineer licensed in the State of Connecticut that work has been completed in compliance with the approved drawings.
- 8. A Final Location Plan will be required by a Professional Land Surveyor licensed in the State of Connecticut depicting all completed improvements.
- Granite block or other decorative stone or brick, depressed curb, driveway apron and curbing within the City of Stamford Right-of-Way shall require a waiver from the City of Stamford Engineering
- 10. Sediment and erosion controls shall be maintained and repaired as necessary throughout construction until the site is stabilized.
- 11. Trees proposed to be planted within the City of Stamford Right-of-Way shall be reviewed and approved by the City's Tree Warden.



1. IF ANY EXISTING ASPHALT IS THICKER THAN 4" THEN MATCH EXISTING ASPHALT THICKNESS. 2. ANY CONCRETE ROADWAY BASE THAT IS REMOVED SHALL BE REPLACED IN KIND.

DETAIL FOR TRENCH REPAIR



2" - 1 - D - S 1 - D - 1 - 2

REFER TO NORTHEAST UTILITIES

DTR 73.209

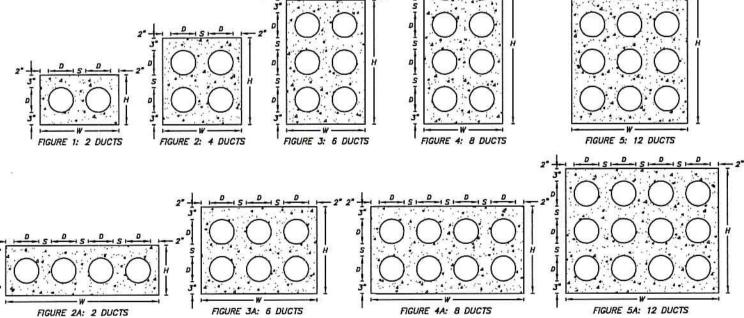
CONDUIT BANK CONSTRUCTION DETAIL

DETAIL FOR WATER SERVICE INSTALLATION

1. THE CONTRACTOR SHALL HAVE ALL MATERIAL SELECTION AND INSTALLATION SPECIFICATIONS APPROVED BY THE AQUARION WATER COMPANY PRIOR TO INSTALLATION.

2" --- 15 --- 1

2. THIS SECTION IS DESIGNED TO RESIST UPLIFT FLOOD FORCES ASSOCIATED WITH THE MINIMUM ELEVATION STANDARD AS SPECIFIED IN THE ZONING REGULATION.

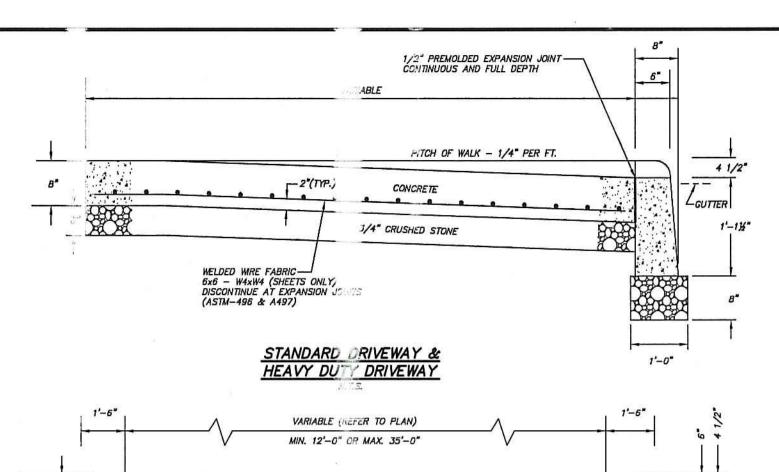


	Dimensions in Inches								
Fig	4" Duct			5" Duct			6" Duct		
	₩	Н	S	W	Н	S	₩	Н	S
1	14-1/2	10-1/2	1-1/2	16-1/2	11-1/2	1-1/2	19	12-1/2	2
2	14-1/2	16-1/2	1-1/2	16-1/2	18-1/2	1-1/2	19	21	2
2A	26-1/2	10-1/2	1-1/2	30-1/2	11-1/2	1-1/2	36	12-1/2	2
3	14-1/2	22-1/2	1-1/2	16-1/2	25-1/2	1-1/2	19	29-1/2	2
3A	20-1/2	16-1/2	1-1/2	23-1/2	18-1/2	1-1/2	27-1/2	21	2
4	14-1/2	28-1/2	1-1/2	16-1/2	32-1/2	1-1/2	18	38	2
4A	26-1/2	16-1/2	1-1/2	30-1/2	18-1/2	1-1/2	36	21	2
5	20-1/2	28-1/2	1-1/2	23-1/2	32-1/2	1-1/2	27-1/2	38	2
5A	26-1/2	22-1/2	1-1/2	30-1/2	25-1/2	1-1/2	36	29-1/2	2

1. At monholes condult banks shall be per Figures 1, 2, 3, 4, or 5.
2. Minimum cover from top of a conduit bank to the pavement of earth surface shall be:
a. State highways — 36 inches
b. Rallroad tracks — 60 Inches

. All other areas - 24 inches In the conduit run between manholes if obstructions are encountered or to reduce trench depth, Figures 2A, 3A, 4A, or 5A are permissible.
 Concrete shall be 2,500 psi, 1/2 inch maximum stone, 6-9 inch slump of such consistency hat spading will ensure the flow of concrete between and under the individual ducts, but not so wet as to float the ducts. For tier buildup construction a stiffer consistency

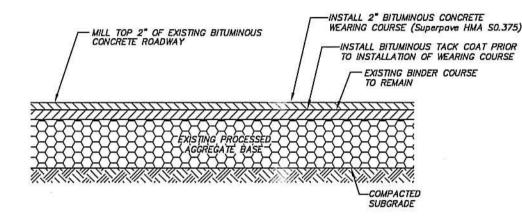
CONDUIT BANK CONSTRUCTION DETAIL



TYPICAL CONSTRUCTION OF CURB AT DRIVEWAY

1. ALL REINFORCING SHALL BE SUPPORTED ON CHAIRS OR OTHER POSITIVE TYPE SUPPORTS APPROXIMATELY ONE PER 25 SQ. FT. 2. CONCRETE SHALL BE CLASS "C" CEMENT TYPE II, 3000 PSI 3. AIR ENTRAINMENT SHALL BE BETWEEN 6 - 7%

REINFORCED CONCRETE DRIVEWAY ENTRANCE



BITUMINOUS CONCRETE ROADWAY OVERLAY DETAIL

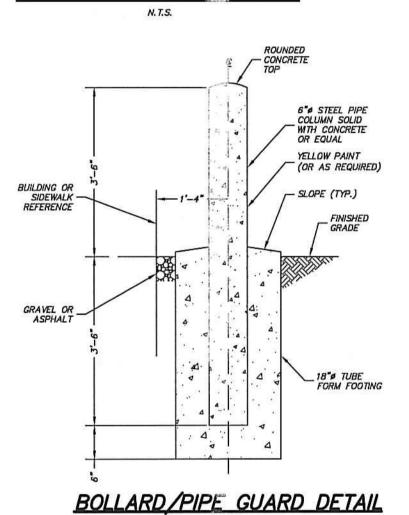


PHOTO RECORD (CONTRACTOR TAKE NOTICE)

THE SITE CONTRACTOR SHALL BE RESPONSIBLE TO TAKE SITE

PICTURES OF ALL THE FOLLOWING MILESTONES AND TO NOTIFY

THE PROJECT ENGINEER OF EACH MILESTONE BEING REACHED.

THE CONTRACTOR SHALL PROVIDE THE PROJECT ENGINEER WITH

DIGITAL LIBRARY OF THE PHOTOGRAPHY AS THE PROJECT

E & S Controls at start of construction

detention/retention/structural LID BMP

Amended soils verification for each BMP

Each detention/retention/structural LID BMP

Each detention/retention/structural LID BMP

Each detention/retention/structural LID BMP

Final site inspection throughout site

Soils verification for each

prior to backfilling/completion

during construction

at completion

SITE WORK PHASE.

PROGRESSES WITH A COMPLETE LIBRARY AT THE END OF THE

PROJECT MILESTONES

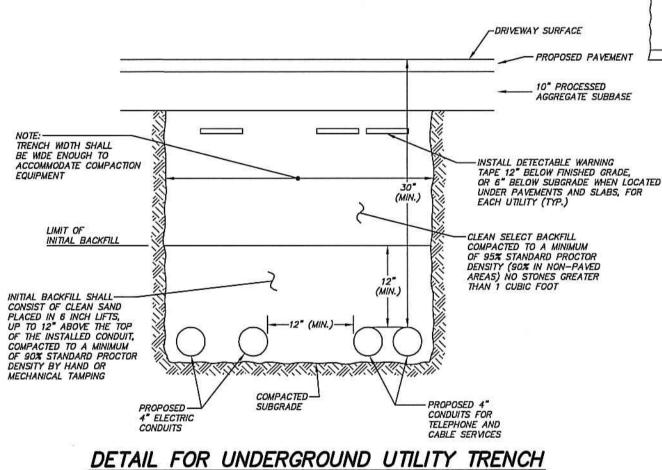
Protection and/or installation of each non—structural

BITUMINOUS CONCRETE ROADWAY & PARKING LOT DETAIL

SEE NOTE 12-

NOTES:

110" PROCESSED
AGCREGATE BASE



-2 1/2" BITUMINOUS CONCRETE BINDER COURSE (CLASS-1)

- 1. COORDINATE INSTALLATION WITH EACH RESPECTIVE UTILITY COMPANY PRIOR TO INSTALLATION. 2. ACTUAL NUMBER AND SIZE OF CONDUITS TO BE INSTALLED MAY VARY. CONTRACTOR SHALL COORDINATE ACTUAL NUMBER AND SIZE OF CONDUITS TO BE INSTALLED WITH BOTH THE OWNER AND EACH RESPECTIVE UTILITY COMPANY
- 3. THIS SECTION IS DESIGNED TO RESIST UPLIFT FLOOD FORCES ASSOCIATED WITH THE MINIMUM ELEVATION STANDARD AS SPECIFIED IN THE ZONING REGULATION.

RAMP ELEVATION AT-

CONSTRUCT THICKER PORTION

STONE OR CONCRETE CURBING

WITH SIDEWALK RAMP WILL NOT BUTT UP AGAINST A

FACE OF

GUTTER LINE

. MAXIMUM SLOPES OF ADJOINING GUTTERS AND ROAD SURFACES IMMEDIATELY ADJACENT TO THE SIDEWALK RAMP OR ACCESSIBLE ROUTE SHOULD NOT EXCEED 20:1.

SIDEWALK RAMPS SHALL HAVE A COARSE BROOM FINISH TRANSVERSE TO THE SLOPE OF THE RAMP. THE SURFACE ALONG ACCESSIBLE ROUTES SHALL BE STABLE, FIRM AND SLIP RESISTANT IN COMPLIANCE WITH ADAAG SECTION 4.5.

DIAGONAL SIDEWALK RAMPS AT MARKED CROSSINGS SHALL BE WHOLLY CONTAINED WITHIN THE MARKINGS, EXCLUDING ANY FLARED SIDES. REMOVAL OF EXISTING SIDEWALK FOR NEW RAMP INSTALLATIONS SHALL BE TO THE NEAREST EXPANSION/CONTRACTION JOINT OR DUMMY JOINT, 12:1 MAY NOT BE

7. EXPANSION JOINTS IN CONCRETE SHALL MATCH THOSE IN ADJACENT SIDEWALKS BUT IN NO CASE SHALL THE SPACING BETWEEN EXPANSION JOINTS EXCEED 12'

UNLESS DIFFERINGS IN MARKED CROSSINGS SHALL HAVE SIDEWALK RAMPS AT BOTH SIDES AND A LEVEL AREA AT LEAST 4' LONG BETWEEN THE RAMPS. IF THIS CANNOT BE ACHIEVED, THE RAISED ISLAND SHALL BE CUT THROUGH LEVEL WITH THE ROADWAY AS SHOWN ON THE PLANS OR AS DIRECTED BY THE ENGINEER.

9. SIDEWALK RAMPS SHALL BE CONSTRUCTED AND PAID FOR UNDER THE ITEM "CONCRETE SIDEWALK" INCLUDING CURBING WITHIN THE LIMITS OF THE NEW SIDEWALK RAMP AND DETECTABLE WARNING STRIPS.

12. TRANSITION TO FULL HEIGHT CURB. INSTALL STONE CURBING IF ADJACENT CURBING IS STONE. INSTALL CONCRETE CURBING IF ADJACENT CURBING IS CONCRETE

NAME AND DETECTABLE WARKING STRIPS.

O. CURBING WITHIN THE LIMITS OF NEW SIDEWALK RAMP SHALL BE CONSTRUCTED IN CONFORMANCE WITH THE REQUIREMENTS OF FORM 814A SECTIONS 8.11 AND 8.13.

HANDICAP RAMPS CONFORMING WITH CONNECTICUT GENERAL STATUTES, SEC. 7—118A, SHALL BE INCORPORATED IN ALL PROPOSED SIDEWALKS AT ALL STREET INTERSECTIONS, AND AT ALL OTHER LOCATIONS WHERE THE GRADE OF A DRIVEWAY OR OTHER FACILITY TAKES PRECEDENCE OVER THE GRADE OF THE PROPOSED OF THE PROPOSED SIDEWALKS AT ALL STREET.

DETAILS FOR SIDEWALK RAMPS

ACHIEVABLE DUE TO SIDEMALK GRADE, IN RECOGNITION OF THIS, A MINIMUM LIMIT OF 15' FOR A PARALLEL RAMP SHALL BE USED. REMOVAL SHALL NOT BE FURTHER THAN 2' FROM THE PROPOSED RAMP UNLESS DIRECTED BY THE ENGINEER, SAW CUT REQUIRED FOR DUMMY JOINTS SHALL BE INCLUDED IN THE COST OF "CONCRETE

2. CARE SHALL BE TAKEN TO ASSURE UNIFORM GRADE ON THE RAMP, FREE OF SAGS AND ABRUPT GRADE CHANGES. 3. ALL RAMPS SHALL BE CONSTRUCTED OF CLASS "C" CONCRETE IN ACCORDANCE WITH CONNECTICUT STANDARD SPECIFICATIONS ARTICLE M.O.3.01.

OR BITOMINUUS. 13. INSTALL THE EDGE OF THE DETECTABLE WARNING 6' FROM THE EDGE OF ROAD. 14. TO PERMIT WHEELCHAIR WHEELS TO ROLL BETWEEN DOMES, ALIGN DOMES ON A SQUARE GRID IN THE DIRECTION OF PEDESTRIAN TRAVEL.

2' DETECTABLE

DIAGONAL SIDEWALK RAMP

(TYPE 4c)

GUTTER LINE FLUSH WITH ROADWAY PAVEMENT

F6' (MAX.)

-GUTTER

SECTION C-C

48:1

- 0.65° idiN.

F0.2*

DOME SPACING

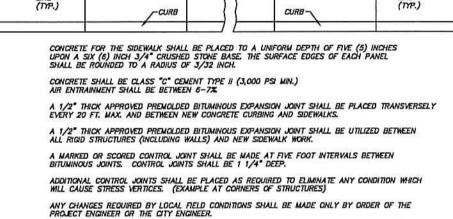
DOME SECTION

ROUND TO

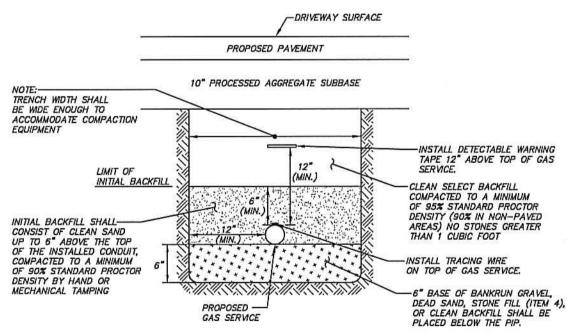
6" REVEAL

CONCRETE CURB

CONCRETE



CONCRETE SIDEWALK WITH CURE



DETAIL FOR GAS SERVICE INSTALLATION

1. THE CONTRACTOR SHALL HAVE ALL MATERIAL SELECTION AND INSTALLATION SPECIFICATIONS APPROVED BY THE GAS COMPANY PRIOR TO INSTALLATION.

2. THIS SECTION IS DESIGNED TO RESIST UPLIFT FLOOD FORCES ASSOCIATED WITH THE MINIMUM ELEVATION STANDARD AS SPECIFIED IN THE ZONING REGULATION.

D'ANDREA SURVEYING & ENGINEERING, PC LAND PLANNERS ENGINEERS SURVEYORS 6 NEIL LANE P.O. ROX 549

MIXED USE DEVELOPMEN

TEL. 637-1779

PREPARED TR BROAD II, LLC **FOR** 0 10-28-22 ZONING SUBMISSION REV. DATE DESCRIPTION 128 BROAD STREET LEONARD C. D'ANDREA, CT PE No. 14865 LOCATION

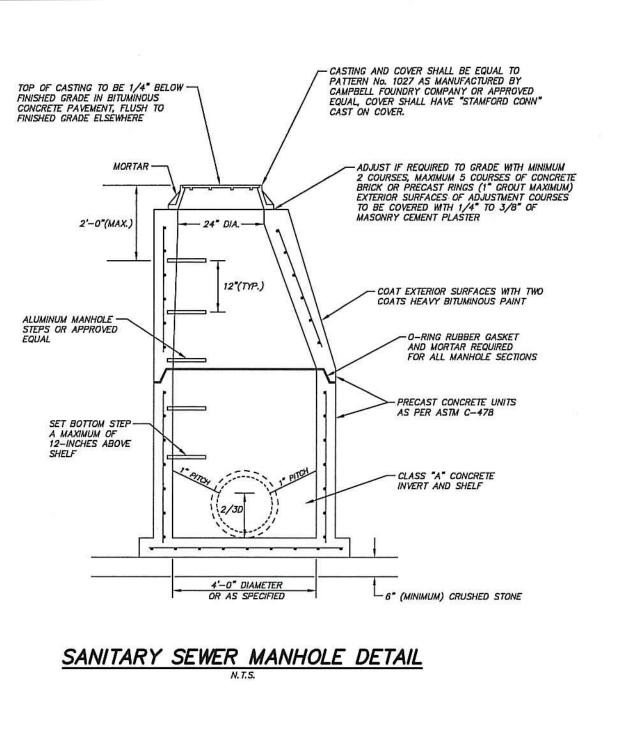
RIVERSIDE, CT 06878

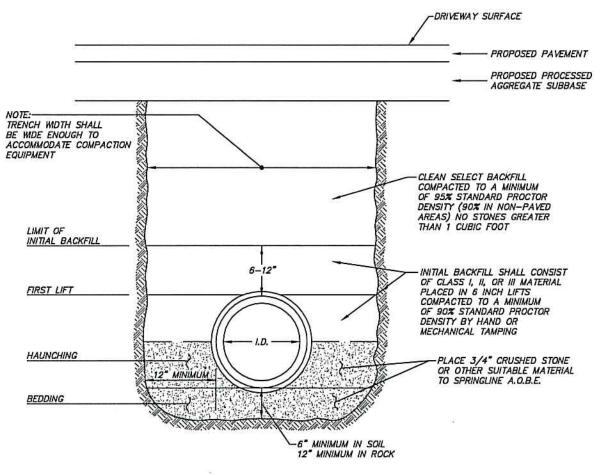
STAMFORD, CONNECTICU 10-28-22 ENGINEER NOTES & DETAILS ONLY COPIES OF THIS PLAN BEARING AN ORIGINAL IMPRINT OF THE ENGINEER'S EMBOSSED SEAL ARE

TRUE, VALID COPIES.

CUT SHEETS FOR APPROVAL. ALL MATERIALS AND PRIOR TO INSTALLATION.

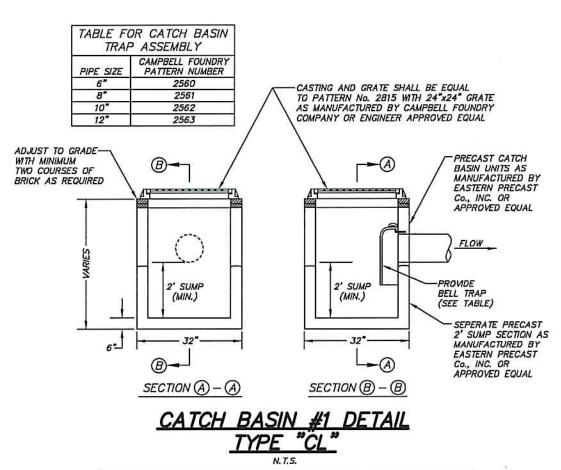
CONTRACTOR SHALL PROVIDE SAMPLES AND/OR CUT SHEETS OF ALL MATERIAL TO BE INSTALLED FOR REVIEW BY THE PROJECT ENGINEER PRIOR TO START OF CONSTRUCTION. CONTRACTOR SHALL ALLOW THREE DAYS FOR PROJECT ENGINEER TO REVIEW MATERIALS AND/OR PRODUCTS MUST BE APPROVED BY THE PROJECT ENGINEE



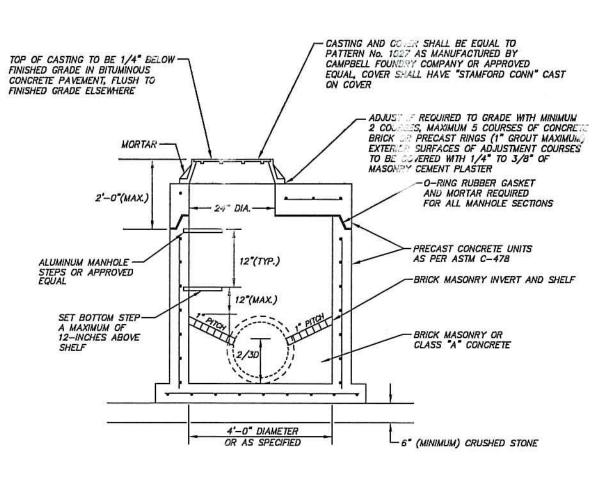


DETAIL FOR PVC SANITARY SEWER AND PVC/RCP STORM DRAIN INSTALLATION

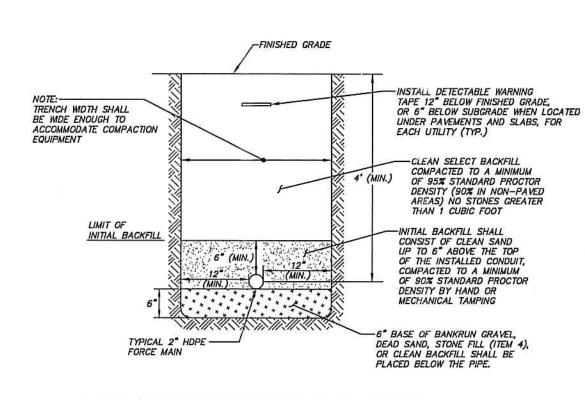
NOTES: 1. REFER TO ASTM D2321 (STANDARD PRACTICE FOR UNDERGROUND INSTALLATION OF THERMOPLASTIC PIPE FOR SEWERS AND OTHER GRAVITY—FLOW APPLICATIONS) FOR TRENCHING SPECIFICATIONS.



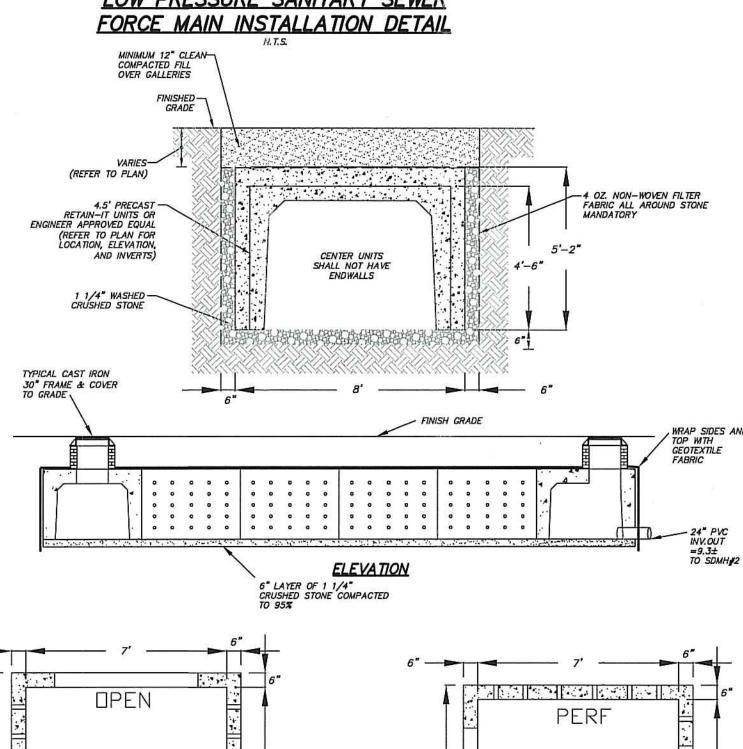
CATCH BASIN SHALL HAVE A MINIMUM SUMP OF 2 FEET AS MEASURED FROM THE LOWEST PIPE INVERT ELEVATION TO THE INTERIOR BOTTOM OF THE STRUCTURE. CONTRACTOR SHALL PURCHASE AND INSTALL A SEPARATE SUMP SECTION. NO OUTLET OR INLET PIPES SHALL PENETRATE THE BOTTOM SUMP SECTION.

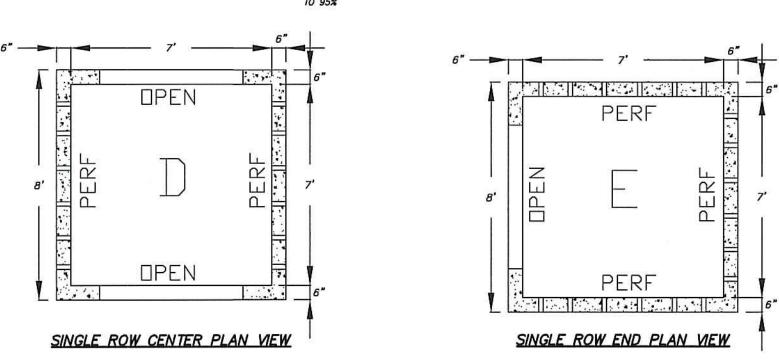


SHALLOW STORM DRAIN MANHOLE DETAIL



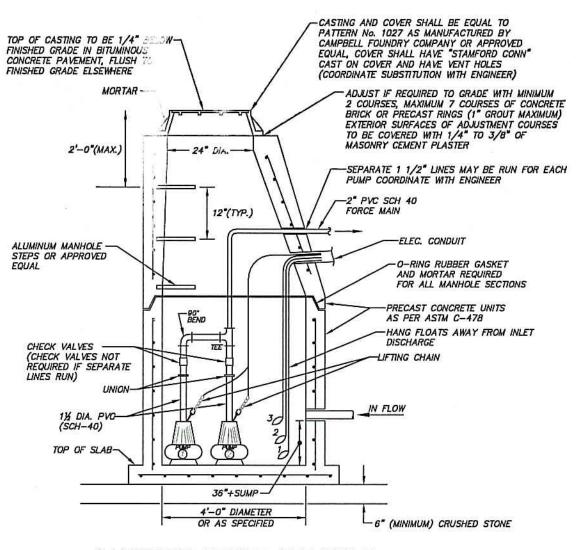
LOW PRESSURE SANITARY SEWER





4.5' PRECAST RETAIN-IT SYSTEM DETAIL

1. THE SOILS BENEATH THE INFILTRATION SYSTEM SHALL BE SCARIFIED OR TILLED



SANITARY SEWER MANHOLE WITH GRINDER PUMPS DETAIL

(FOR DUPLEX GRINDER PUMPS)

OTHERS.

FLOAT ELEV.'S 1. PUMP OFF: (6"± OFF BOTTOM) 2. PUMP ON: (15"± BOTTOM) 3. ALARM AND LAG PUMP ON (WITH SAME FLOAT); (18"± OFF BOTTOM)

1. FURNISH AND INSTALL 2, GOULD'S SEWAGE GRINDER PUMPS WITH GOULD PANEL No. A6—2012 WITH A NEMA—1 ENCLOSURE AND 3 FLOAT CONTROLS POLYURETHANE FOAM FLOAT A2K23W (A2—3)
2. PUMPS AND CONTROLS SHALL BE CONNECTED TO A BACK UP POWER SUPPLY TO RUN DURING POWER FAILURES. LICENCED ELECTRICIAN TO COORDINATE WITH ENGINEER AND PROVIDE WIRING SCHEMATIC AS REQUIRED.

3. CONTRACTOR TO PROVIDE AND INSTALL PIPING, VALVES AND FITTINGS AS REQUIRED.

4. PANEL TO BE INSTALLED PROXIMATE TO OTHER CONTROL PANELS IN BASEMENT, COORDINATE WITH MECHANICAL ENGINEER.
5. ENGINEER TO BE NOTIFIED TO ATTEND START UP TEST WHEN INSTALLATION IS COMPLETE.

DUPLEX PUMP SYSTEM DEPICTED HEREON IS FOR DEMONSTRATION PURPOSES ONLY FLOW CALCULATIONS AND DESIGN OF PUMPS/FLOATS TO BE COMPLETED BY

/ ALTERNATE

POSITION B

6. PUMPS, CONTROLS, AND MANHOLE MAY BE SUPPLIED BY EASTERN PRECAST 1-203-775-0230, ENGINEER MAY APPROVE EQUAL SUBSTITUTIONS. SUBMIT FOR APPROVAL IN WRITING.

- 15'-0" —

PREFERRED

POSITION A

PLAN VIEW

38″——►

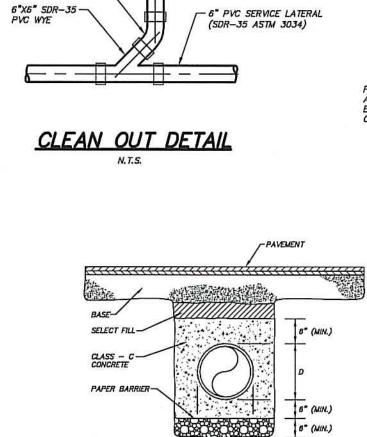
⊢ 20″

─ NOTE 6

SECTION A-A

14'-0" -

NOTE 5 -



- 2'-6" DIA. --

6" PVC RISER PIPE-

6" SDR-35 PVC -45 ELBOW

LENGTH AS REQUIRED (SDR-35 ASTM 3034)

CAST IRON FRAME AND COVER — CAST IRON FRAME AND COVER SHALL BE CAMPBELL FOUNDRY PATTERN No. 4155, OR ENGINEER APPROVED EQUAL, TO BE INSTALLED AT GRADE.

- CLASS "C" CONCRETE COLLAR

- 6" PVC WATER TIGHT PIPE PLUG

CONCRETE CASING DETAIL

See Details and Notes

Alternate – Position C

SECTION B-B

Two 38" openings on

G 44" from inside of

on reverse side.

each end.

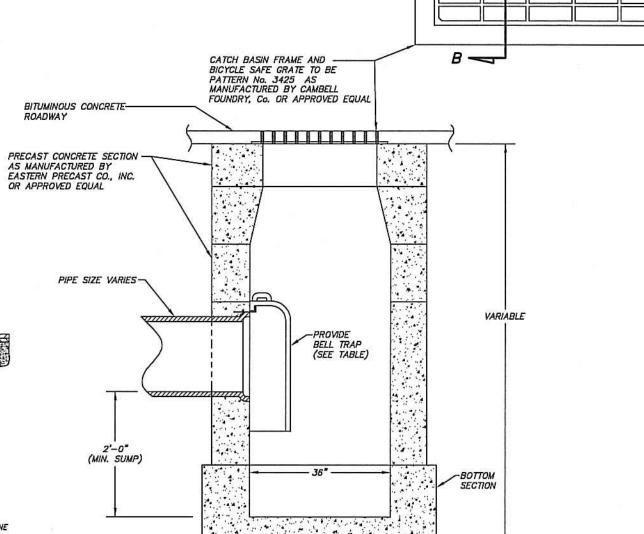


TABLE FOR CATCH BASIN

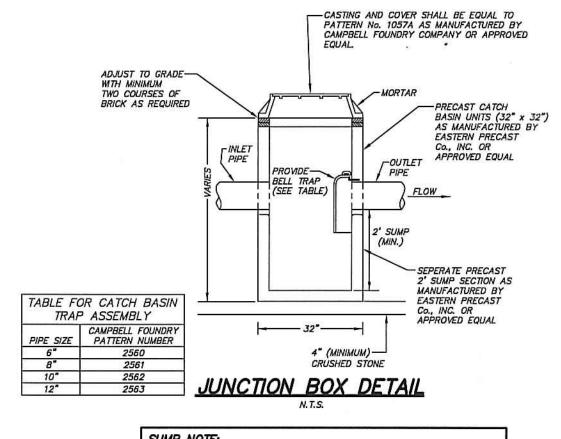
TRAP ASSEMBLY

PIPE SIZE CAMPBELL FOUNDRY
PATTERN NUMBER

CATCH BASIN DETAIL (DOUBLE TYPE "CL") CATCH BASIN SHALL HAVE A MINIMUM SUMP OF 2 FEET

SECTION "B-B"

AS MEASURED FROM THE LOWEST PIPE INVERT ELEVATION TO THE INTERIOR BOTTOM OF THE STRUCTURE. CONTRACTOR SHALL PURCHASE AND INSTALL A SEPARATE SUMP SECTION. NO OUTLET OR INLET PIPES SHALL PENETRATE THE BOTTOM SUMP SECTION.



JUNCTION BOX SHALL HAVE A MINIMUM SUMP OF 2 FEET AS MEASURED FROM THE LOWEST PIPE INVERT ELEVATION TO THE INTERIOR BOTTOM OF THE STRUCTURE. CONTRACTOR SHALL PURCHASE AND INSTALL A SEPARATE SUMP SECTION. NO OUTLET OR INLET PIPES SHALL PENETRATE THE BOTTOM SUMP SECTION.

 Manhole shall be designed for the following loads:
 a. The roof shall be designed for AASHTO HS20-1996 direct wheel load. b. The walls shall be designed for the summation of the following:

 Soil pressure of not less than an equivalent fluid pressure of 33 pcf.
 Hydrostatic pressure of 5 feet measured from the base of the manhole. 3) A surcharge of 2.5 feet of soil weighing 120 pcf. c. The floor shall be designed to resist the hydrostatic pressure resulting from the 5-foot head called for in

 Concrete and concrete design shall be in accordance with ACI 318–1999.
 Concrete shall have a minimum and maximum 28–day strength of 4000 and 5000 psi respectively. 4. Steel reinforcing bars shall conform to ASTM A615-1992 Grade 40 or 60. Welded wire mesh shall conform to ASTM A185-1997 or A497-1999.

5. Pulling eyebolts, with a minimum 8000-pound pulling strength, shall be installed adjacent to window knockouts, at eight places.

6. Zinc alloy inserts $\frac{1}{2}$ inch - 13 x 1 $\frac{1}{2}$ inch shall be installed at 48 places. 7. Openings and knockouts shall be clear of reinforcement.

side of the 38-inch opening.

8. Construction joint shall be sealed with asphalt cement or equivalent. 9. Manufacturer's identification and month/year when manufactured shall be legibly marked in/on concrete in the

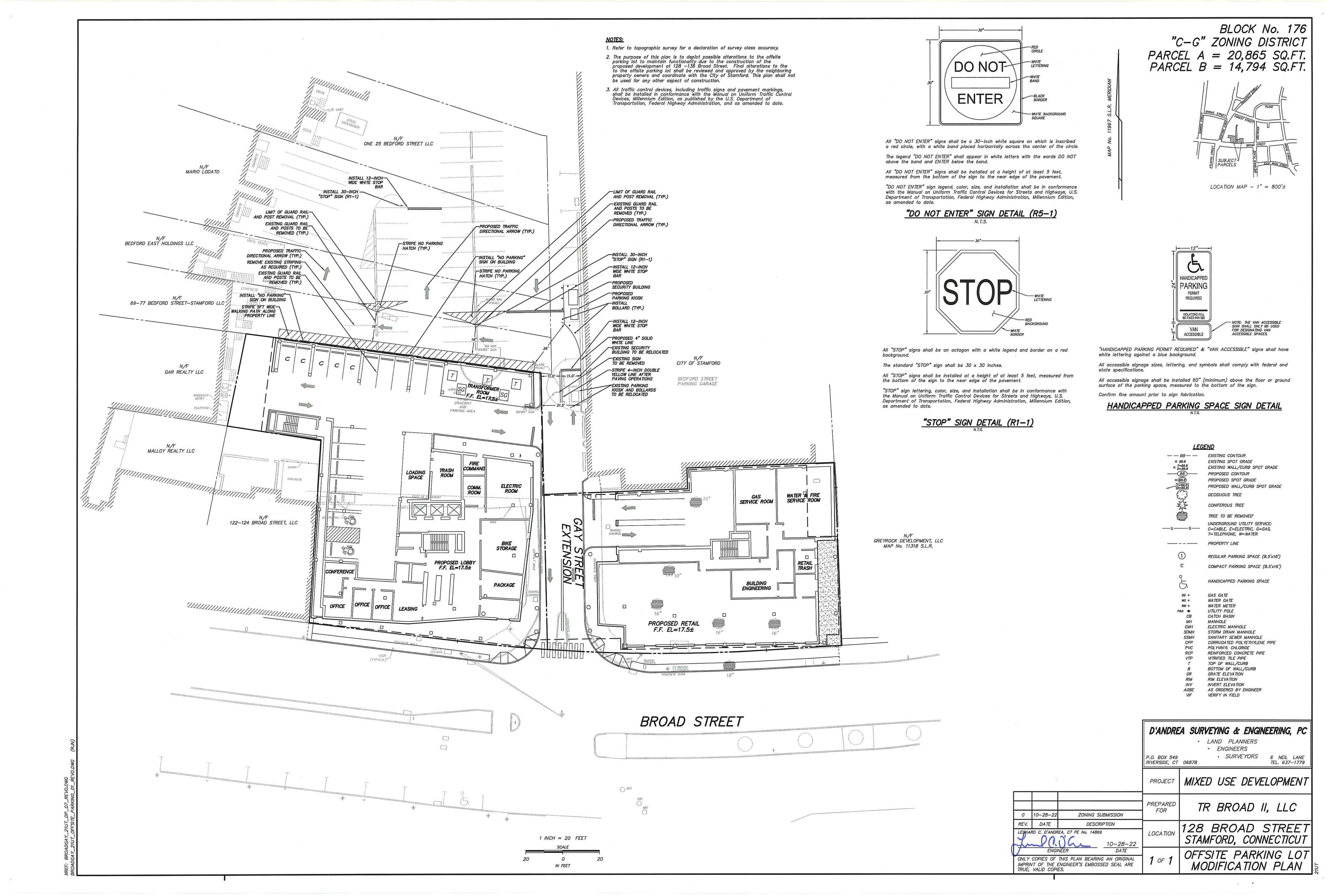
10. This is an oversized manhole only to be used in special cases. A crane will be needed to set both sections of this manhole.

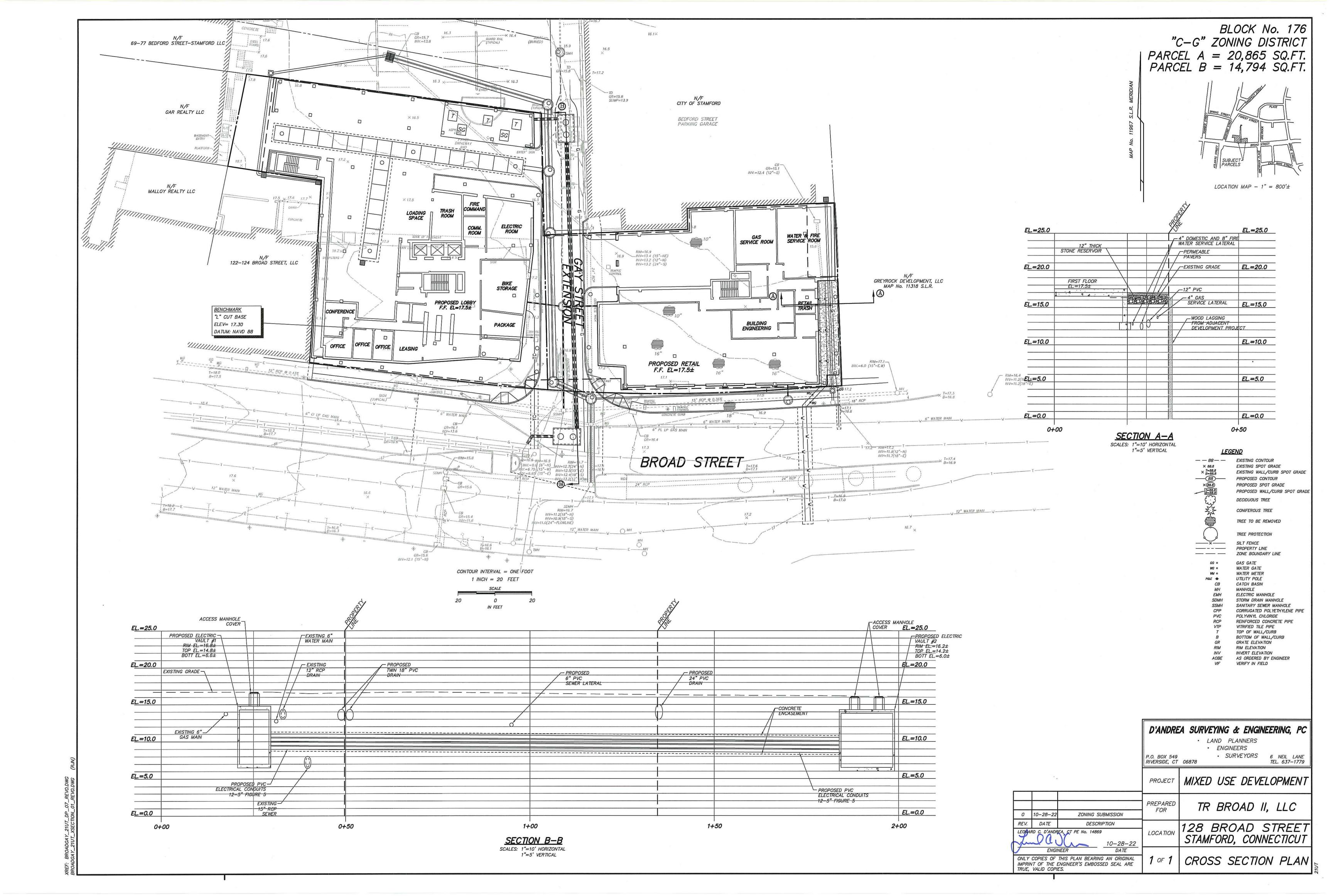
MANHOLE - PRECAST REINFORCED CONCRETE 8'-0" x 14'-0" x 7'-0" INSIDE SPC M-039.02 9 MATERIAL SPECIFICATION EVERSOURCE ENERGY

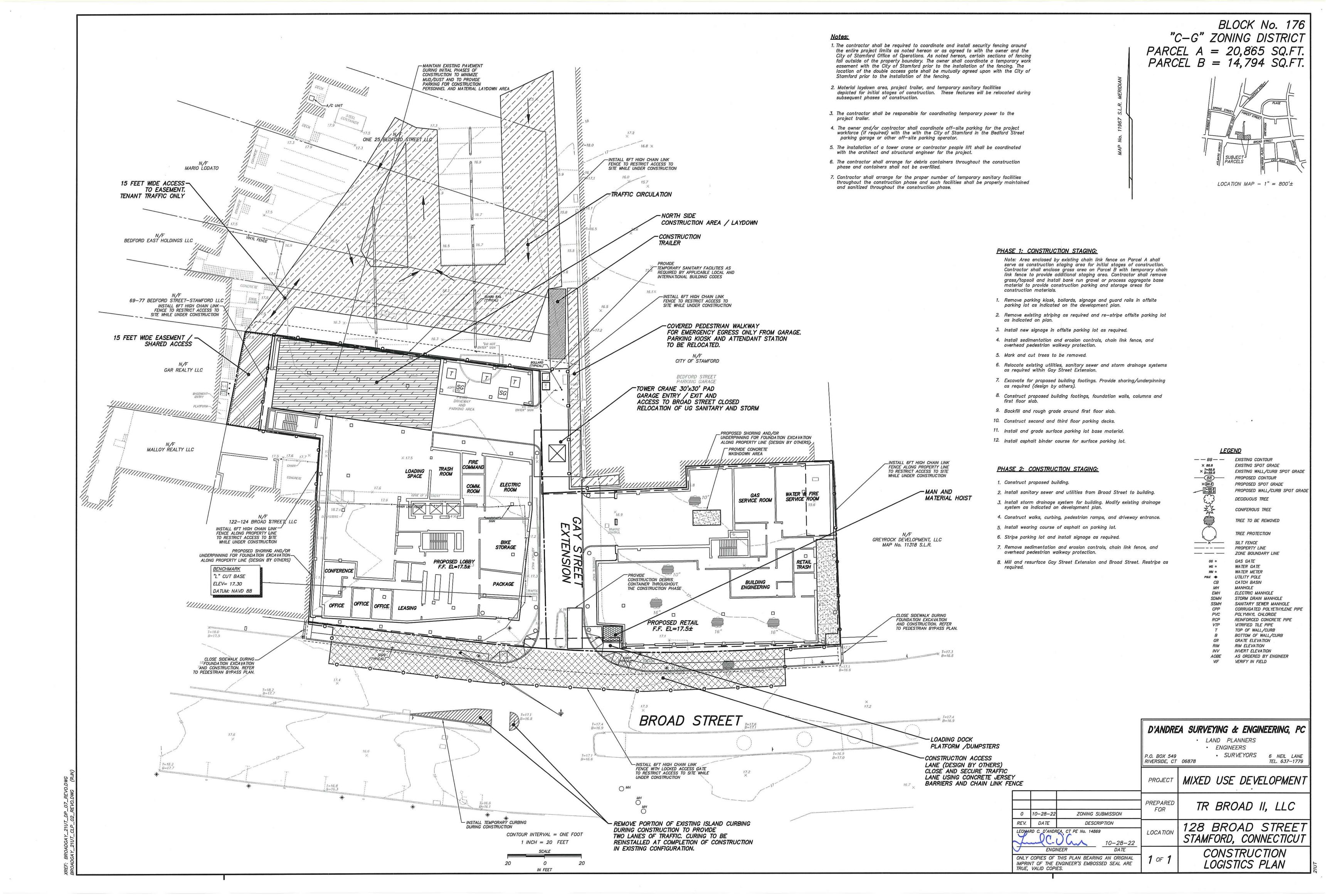
D'ANDREA SURVEYING & ENGINEERING, PC LAND PLANNERS ENGINEERS SURVEYORS P.O. BOX 549 6 NEIL LANE RIVERSIDE, CT 06878 TEL. 637-1779 MIXED USE DEVELOPMENT PROJECT PREPARED TR BROAD II, LLC ZONING SUBMISSION DESCRIPTION

0 10-28-22 REV. DATE 128 BROAD STREET LEONARD, C. D'ANDREA, CT PE No. 14869 LOCATION STAMFORD, CONNECTICUT 10-28-22 ENGINEER

ONLY COPIES OF THIS PLAN BEARING AN ORIGINAL **DETAILS** IMPRINT OF THE ENGINEER'S EMBOSSED SEAL ARE TRUE, VALID COPIES.







AGREEMENT COVENANT

l c	224
AGREEMENT made this day of by hetween TR Broad II LLC of Stamford, CT (hereinaf	
permeenor	
referred to as "Owner") and the CITY OF STAMFORD, 888 Washington Bl	vd.
Stamford CT 06901, a municipal corporation lying within the County	of
Fairfield and State of Connecticut, acting herein by its duly authori	zed
Mayor, Caroline Simmons (hereinafter referred to as the "City"), and	the
ENVIRONMENTAL PROTECTION BOARD OF THE CITY OF STAMFORD, acting herein by	its
duly authorized Chairman, Gary H. Stone (hereinafter referred to as	the
"EPB").	
WITNESSETH:	
WHEREAS, OWNER has commenced the planning and construction	of
a mixed use development	
on a parcel of land owned by them and as more particularly described	on
Schedule "A", attached hereto and made a part hereof (the "Property").	
WHEREAS, certain drainage facilities ("Drainage Facilities	;"),
including but not limited to subsurface retention system as m	nore
particularly described on Schedule "B" attached (the "Construction Plan	ıs")
shall be installed in connection with the aforesaid construction and	in
accordance with the Construction Plans and	
issued therefore, (the "Permit") and;	
WHEREAS, OWNER, the CITY and EPB share a joint concern that	the

Drainage Facilities be maintained in a functioning condition so as to avoid

pollution of surface and groundwaters, flooding and/or improper drainage.

NOW, THEREFORE, in consideration of ten dollars and other good and valuable consideration receipt of which is hereby acknowledged by the OWNER, it is hereby agreed as follows:

- 1) OWNER shall clean the drainage facilities or cause such facilities to be cleaned by periodic removal of accumulated sediment and debris in a good and workman-like manner, at least two (2) times during every twelve (12) month period, which times shall be in the period between April and June and between October and December and more often as the City may determine to be necessary.
- OWNER shall sweep, or cause to be swept, garage facilities, driveways and roadway surfaces located on the Property at least once per calendar quarter.
- 3) OWNER shall utilize only sand or calcium chloride in connection with the de-icing of areas within the Property meaning and intending that road salt (Sodium Chloride) shall not be used for said purpose.
- 4) OWNER shall repair or replace any defects or defective drainage facilities so as to maintain the drainage facilities, at all times, in a fully functional capacity.
- 5) OWNER shall file as-built drainage plans with the EPB immediately upon the completion of work. Said plans shall be prepared by a professional engineer/surveyor registered in the State of Connecticut.

- OWNER grants the CITY and/or EPB, its agents, and employees, the right to enter the Property at all reasonable times upon twenty-four (24) hours notice to the OWNER for the purpose of inspecting the Property to determine if OWNER is complying with the requirements hereunder. A representative of the Owner shall have the right to accompany the City and/or EPB on their inspection of the Property.
- If, after an inspection is made pursuant to Paragraph Six (6) 7) hereof, the CITY and/or EPB determines that the owner has failed to comply with the aforesaid undertakings, then the CITY and/or EPB shall give written notice of said determination to the then OWNER of the Property which notice shall also specify the said Said notice shall be sent by registered or certified failure. mail to the last known address of said Owner. If the Owner disputes the claim, he shall give written notice thereof to City and/or EPB within ten (10) days of receipt of said notice, and the EPB shall hold a hearing as promptly as possible to decide the merits of the disputed claim. If the claim is not disputed within said ten (10) days, the OWNER shall have thirty (30) days from the receipt of said notice to correct said failure, unless it is impossible to cure said defect within said time, in which case, immediately commenced necessary repairs shall be and diligently pursued to completion within a reasonable time.
- 8) If the said failure is not remedied within the time frame herein stated, the CITY and/or EPB may proceed to cure the same and charge the actual cost thereof to the OWNER of the Property.

- 9) OWNER agrees to reimburse the CITY and/or EPB for reasonable legal fees and court costs if it becomes necessary for the CITY and/or EPB to sue for reimbursement of sums expended by the CITY and/or EPB in performance of OWNER'S obligation.
- 10) OWNER agrees and covenants to indemnify and save harmless the CITY and the EPB against any and all claims, suits, actions or judgments arising out of the delay in the performance of any of their obligations pursuant to this Agreement.
- 11) OWNER agrees that this covenant and restriction shall apply to and run with the land. It shall be binding on all future owners, administrators, executors, successors and assigns.
- 12) The OWNER hereby represents to the CITY and EPB that he/she is the owner, in fee simple, of all of the property described in "Schedule A" attached hereto and made a part hereof.
- 13) OWNER agrees that this Agreement and restrictive covenant upon execution of the same, shall be recorded on the land records at the OWNER'S expense at the time that a permit is issued for the Property herein and while the OWNER is in title.
- 14) OWNER agrees not to assert the invalidity of this document.
- 15) OWNER agrees that nothing herein shall be construed to be a limitation upon the right of the EPB to assert and enforce any

rights it may have under federal, state or City statute, ordinance or regulation.

16) This agreement shall be governed by the laws of the State of Connecticut.

IN WITNESS WHEREOF, the said parties hereto have hereunto set their hands and seals, the day and year first above written.

#1	(A. 1)	THE CITY OF STAMFORD
	Printed Name:	BY:
		Caroline Simmons
#2		Its duly authorized Mayor
	Printed Name:	
#1	3	THE ENVIRONMENTAL PROTECTION BOARD
	Printed Name:	BY:
		Gary H. Stone
#2		Its duly authorized Chairman
	Printed Name:	
#1		OWNER
	Printed Name:	BY:
#2		(Owner's Name)
	Printed Name:	

(Acknowledgement on the Following Page)

STATE OF CONNECTICUT }	Date:
Personally appeared Caroline Sim signer and sealer of the foregoing In be her free act and deed and the free	mons, Mayor of the City of Stamford, strument, and acknowledged the same to act and deed of said City, before me.
	Commissioner of the Superior Court or Notary Public
STATE OF CONNECTICUT} } ss: STAMFORD COUNTY OF FAIRFIELD }	Date:
Protection Board of the City of Stamfo	tone, Chairman of the Environmental ord, signer and sealer of the foregoing to be his free act and deed and the before me.
**	Commissioner of the Superior Court or Notary Public
STATE OF CONNECTICUT } } ss: STAMFORD COUNTY OF FAIRFIELD }	Date:
	and sealer of the foregoing instrument, see act and deed, before me.
	Commissioner of the Superior Court or Notary Public

SCHEDULE "A"

PARCEL A:

ALL THAT CERTAIN piece, parcel or tract of land, with the buildings and improvements thereon, situated in the City of Stamford, County of Fairfield and State of Connecticut, and known as 128 Broad Street, which is more particularly bounded and described as follows:

NORTHERLY: One Hundred Sixty-one (161) feet, more or less, by land now or formerly of The Estate of Mary M. Scofield, dec'd.

EASTERLY: One Hundred Forty-eight (148) feet, more or less, by a driveway, now or formerly known as Gay Street Extension;

SOUTHERLY: One Hundred Thirty (130) feet by Broad Street;

WESTERLY: Ninety-eight (98) feet, more or less, by land now or formerly of Charles M. Lounsbury, dec'd. et al, and now or formerly of George Dimenstein:

SOUTHERLY AGAIN: Fifty-one (51) feet, more or less, by land now or formerly of the Estate of Charles Lounsbury, dec'd, et al and now or formerly of George Dimensiein; and

WESTERLY AGAIN: Fifty and 05/100 (50.5) feet by land now or formerly of Merwin Realty Co., and now or formerly of Floyd B. Bertrom, et al.

SAID PREMISES are known and designated as "Parcet 'C', 7.883+/- Sq. Ft." and "Parcet 'D', 12,982+/- Sq. Ft." as shown on a certain map entitled, "Map Prepared for Thomas K. Standish. Stamford, Connecticut, Scale 1" = 20', Aug. 22, 1988", certified "Substantially Correct" by William W. Seymour, Conn. L.S. Reg. No. 11352 for William W. Seymour and Associates, P.C., Land Surveyors, Darien, Conn., which map is on file in the Office of the Town Clerk of the City of Stamford as Map No. 11192, reference thereto being had.

PARCEL B:

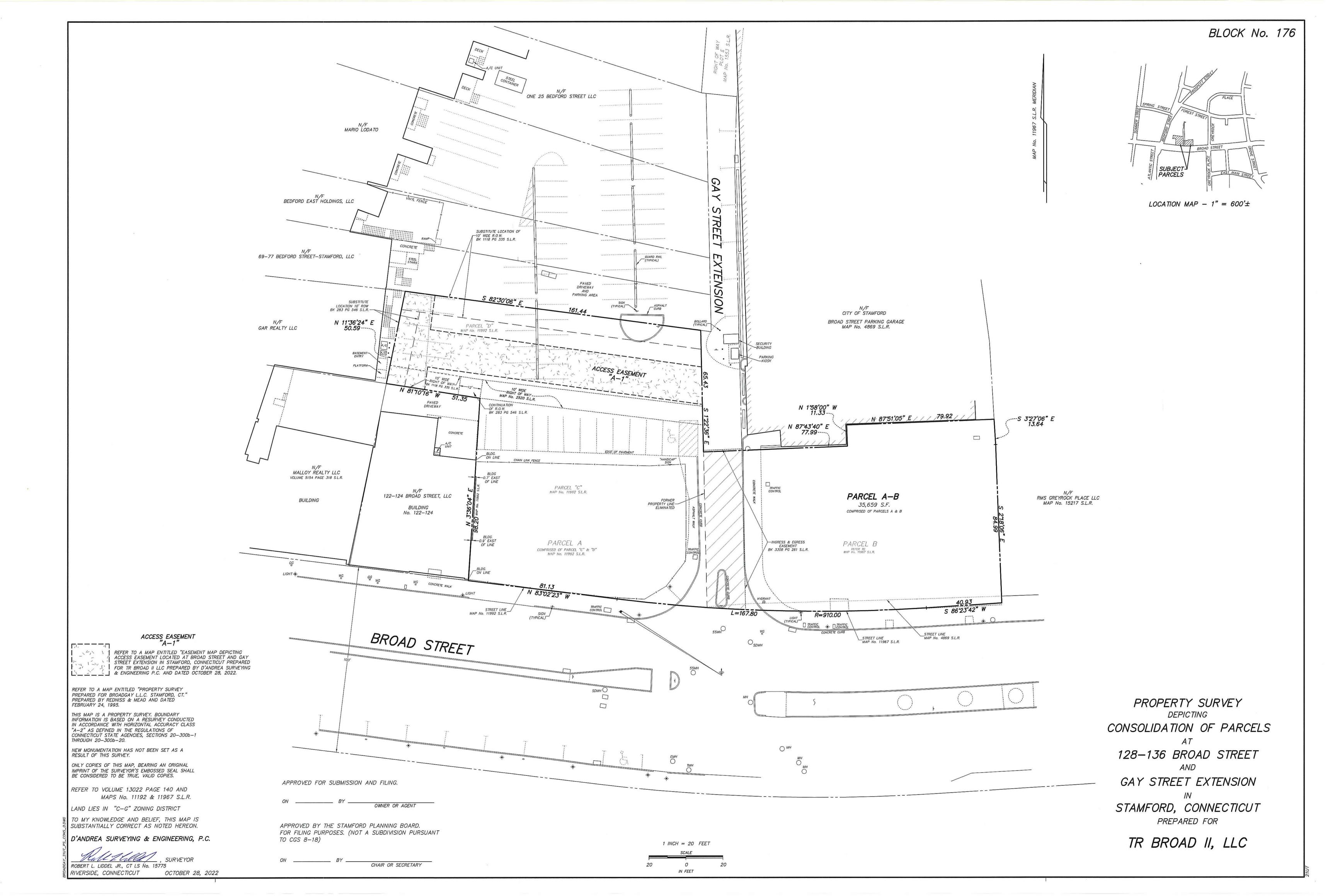
ALL THAT CERTAIN piece, parcel or tract of land, located in the City of Stamford, County of Fairfield and State of Connecticut, located at the northeast corner of Broad Street including the southerly terminus of Gay Street Extension, and bounded and described as follows:

BEGINNING at a point on the new northerly street line of Broad Street as it now exists where said northerly street line intersects the westerly property line of land of United Broad Street Associates, said point being further located 3.65 feet southerly of the southwesterly corner of said land of United Broad Street Associates as shown and delineated on Map No. 11318 of the Stamford Land Records. Thence westerly along said northerly street line of Broad Street, the following courses and distances: S. 86° 23' 42" W. a distance of 40.93 feet, thence continuing on a curve to the right, thence continuing on a curve to the right, the radius of which is 910.00 feet a distance of 118.869 feet to land of Anthony R. Lorenzo, Trustee. Thence northerly along land of said Anthony R. Lorenzo, Trustee N. 1° 22' 36" W. a distance of \$3.437 feet to a point, thence casterly, northerly and again easterly through in part across Gey Street Extension and land of the City of Stamford. the following courses and distances: N. 87° 43' 40" E. a distance of 77.992 feet, N. 1° 58' 00" W. a distance of 11.33 feet and N. 87" 51" 05" E. a distance of 79.917 feet to land of United Broad Street Associates. Thence southerly along land of said United Broad Street Associates the following courses and distances: S. 3° 27' 06" E. a distance of 13.64 feet and S. 2º 18' 06" E. a distance of 84.99 feet to the point or place of beginning,

SAID PREMISES are shown and defineated on a certain map entitled, "Map Showing a Portion of Property of the City of Stamford, Stamford, Connecticut,", certified by Paul R.-Manula, Land Surveyor, on December 22, 1987, which map is on file in the Stamford Town Clerk's Office as Map No. 11967, reference thereto being had.

THE above-described property contains 14,794 square feet and lies in Block 176 of the Stamford Land Records.

Properties are known as 136 Broad Street, Stamford, Connecticut & 0 Broad Street (Account #004-0515), Stamford, Connecticut



Sanitary Sewer Flow Calculations

Name:

TR Broad II, LLC

Address:

128 Broad Street Stamford, Connecticut

Date:

October 28, 2022

Summary

The following calculations were performed to determine if the existing sanitary sewer main, which extends along the frontage of the proposed development, has sufficient capacity to handle contributing flows from the proposed building. The sanitary sewer connections from the proposed building to the existing sanitary sewer main are depicted on Sheet 2 of 6 of the Final Site Plan Review Set, as prepared by D'Andrea Surveying & Engineering, PC.

The existing sanitary sewer main receiving contributing flows from the proposed building is a 15-inch RCP that directs flow to the east along the northern edge of the Broad Street Right-of-Way towards Greyrock Place.

Proposed Building Daily Residential Sewer Discharge Volume:

		0.1
Proposed Number of Studio Units	=	31
Proposed Number of One Bedroom Units	=	87
Proposed Number of Two Bedroom Units	=	69
Proposed Number of Three Redroom Units	=	9

Sewer Discharge Per Capita Per Day = 75 gallons

Studio Units

$$V_{1BR} = 31 \text{ units } \times \frac{1 \text{ bedroom}}{1 \text{ unit}} \times \frac{1 \text{ persons}}{1 \text{ bedroom}} \times 75 \text{ gpcd} = 2,325 \text{ gpd}$$

One Bedroom Units

$$V_{1BR} = 87 \text{ units } \times \frac{1 \text{ bedroom}}{1 \text{ unit}} \times \frac{2 \text{ persons}}{1 \text{ bedroom}} \times 75 \text{ gpcd} = 13,050 \text{ gpd}$$

Two Bedroom Units

$$V_{2BR} = 69 \text{ units } \times \frac{2 \text{ bedroom}}{1 \text{ unit}} \times \frac{2 \text{ persons}}{1 \text{ bedroom}} \times 75 \text{ gpcd} = 20,700 \text{ gpd}$$

Three Bedroom Units

$$V_{3BR} = 9 \ units \times \frac{3 \ bedroom}{1 \ unit} \times \frac{2 \ persons}{1 \ bedroom} \times 75 \ gpcd = 4,050 \ gpd$$

□ Proposed Building Retail Sewer Discharge Volume:

Eastern Retail: 4,284 sq.ft. (Approximately)

Assume this space will be used for a restaurant and/or food establishment.

Assume restaurant has 150 seats and serves breakfast, lunch and dinner.

Sewer Discharge Per Seat Per Day (Restaurant with Public Toilet) = 45 gallons

$$V_{Western\,Re\,tail} = 150 seats \times \frac{45\ GPD}{1\ seat} = 6,750\ gpd$$

□ Proposed Building Total Combined Daily Discharge Volume:

$$V_{Total} = 2,325 + 13,050 + 20,700 + 4,050 + 6,750 = 46,875 Gallons$$

Total Combined Daily Discharge Volume < 50,000 gpd, therefore only a local discharge permit is required.

Proposed Building Peak Daily Discharge Rate:

Peak Daily Discharge Rate

$$q_{peak} = V_{Total} \times Peak \ Factor = 46,875 \times 6.0 = 281,250 gpd$$

= 260 gpm (18 hour period)

Maximum Capacity of Existing 15" RCP Sewer Main in Broad Street

=	Pipe Capacity			
=	Manning's Roughness Coefficient	=	0.013	(RCP)
=	Pipe Slope	=	0.004	ft/ft
=	Pipe Diameter	=	15	in
=	Pipe Area	=	1.227	\mathbf{ft}^2
=	Wetted Perimeter	=	3.927	ft
=	Hydraulic Radius	=	0.3125	ft
	= = =	 Pipe Capacity Manning's Roughness Coefficient Pipe Slope Pipe Diameter Pipe Area Wetted Perimeter Hydraulic Radius 	 Manning's Roughness Coefficient Pipe Slope Pipe Diameter Pipe Area Wetted Perimeter 	= Manning's Roughness Coefficient = 0.013 = Pipe Slope = 0.004 = Pipe Diameter = 15 = Pipe Area = 1.227 = Wetted Perimeter = 3.927

$$Q = \frac{1.49}{n} A R_H^{\frac{2}{3}} S^{\frac{1}{2}} = \frac{1.49}{0.013} (1.227) (0.3125)^{\frac{2}{3}} (0.004)^{\frac{1}{2}} = 4.10 \ cfs$$
$$= 1.840 \ \text{gpm}$$

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□ Existing Peak Daily Flow Rate (Per Field Observations)

An inspection of the existing sanitary sewer manhole approximately 30 feet to the east of 136 Broad Street has revealed a high water mark stain/scum line contained within the flow line trough of the manhole. Therefore, an assumption has been made that under "high flow conditions", flow in the sewer main is approximately 8" above the invert of the 15" sewer main. Therefore, the peak flow rate under "high flow conditions" is approximately 2.3 cfs or 1,032 gpm.

Conclusion Summary

Proposed Total Combined Daily Discharge Volume	=	46,875	gal
Existing Daily Peak Flow Rate	=	1,032	gpm
Proposed Increase in Daily Peak Flow Rate	=	260	gpm
Proposed Daily Peak Flow Rate	=	1,292	gpm
Capacity of Existing 15-inch RCP Sewer	=	1,840	gpm

The proposed total combined daily discharge volume from the proposed development is estimated to be approximately 46,875 gallons and will therefore require a local discharge permit from the WPCA. The addition of the calculated peak discharge from the project site, 260 gpm, plus the approximate existing "high flow condition" flow rate, 1,032 gpm, equals 1,292 gpm, which is still less than the maximum flow capacity of the sewer pipe, 1,840 gpm, by approximately 30 percent. Therefore, the existing sanitary sewer main has sufficient capacity to handle the increase in the daily peak flow rate from the proposed building.

Leonard C. D'Andrea, PE CT License No. 14869





